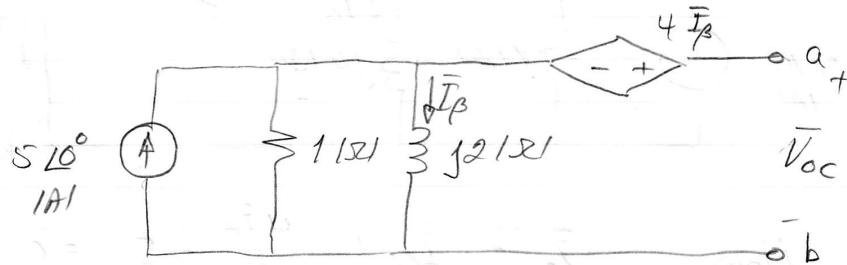


### Example 9.6



Find the Thevenin equivalent at a, b.

Open-Circuit Voltage:

Note there is no current in the source  $4\bar{I}_\beta$ , so we may use the current divider rule to find  $\bar{I}_\beta$ :

$$\bar{I}_\beta = 5\angle 0^\circ \cdot \frac{1}{1+j2} = 1-j2 \text{ A}$$

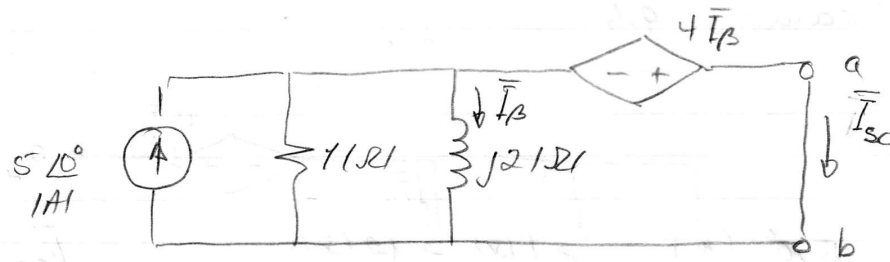
Then

$$\begin{aligned}\bar{V}_{oc} &= 4\bar{I}_\beta + j2\bar{I}_\beta \\ &= (4+j2)(1-j2) = 8-j6\end{aligned}$$

$$\bar{V}_{oc} = \bar{V}_{Th} = 10 \angle -36.9^\circ \text{ V}$$

Short-Circuit Current:

Now there is a current in the  $4\bar{I}_\beta$  source: it is  $\bar{I}_{sc}$ :



Now 
$$\bar{I}_{sc} + \bar{I}_\beta + \frac{4\bar{I}_\beta}{1} - 5 = 0$$

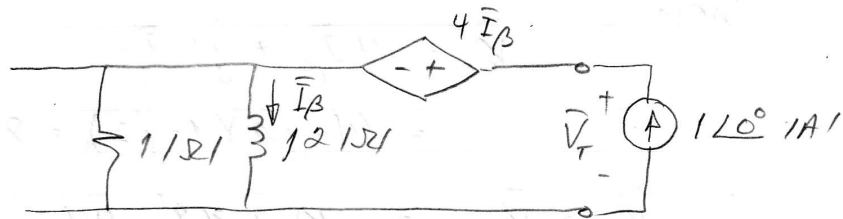
But 
$$-\frac{4\bar{I}_\beta}{j2} = \bar{I}_\beta \Rightarrow \bar{I}_\beta = 0!$$

$$\therefore \bar{I}_{sc} = 5\angle 0^\circ \text{ A}$$

$$\Rightarrow Z_{Th} = \bar{V}_{oc} / \bar{I}_{sc} = 2\angle -36.9^\circ \Omega$$

$$Z_{Th} = 1.6 - j1.2 \Omega$$

Just for practice, we use a test source as well:



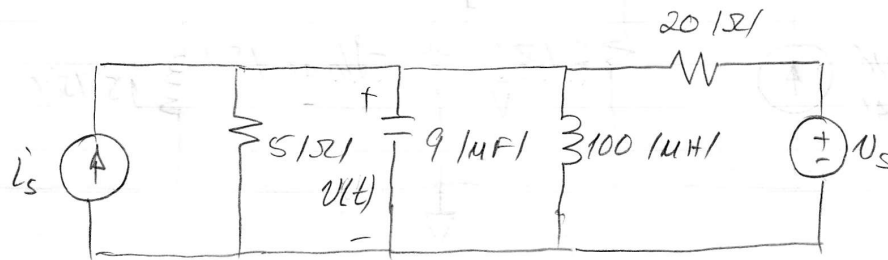
$$\bar{I}_\beta = 1 \cdot \frac{1}{1+j2} = 0.2 - j0.4 \text{ A}$$

$$\bar{V}_T = 4\bar{I}_\beta + j2\bar{I}_\beta = (4+j2)\bar{I}_\beta$$

$$= 1.6 - j1.2 \text{ V}$$

$$\therefore Z_{Th} = \bar{V}_T / \bar{I}_T = 1.6 - j1.2 \Omega \quad \checkmark$$

### Example 9.7



GIVEN:  $i_s = 10 \cos \omega t \text{ A}$

$v_s = 100 \sin \omega t \text{ V}$

$\omega = 50 \times 10^3 \text{ rad/s}$

FIND:  $v(t)$  using the Node-Voltage method.

We must transform to the phasor domain.

Note that  $v_s = 100 \sin(\omega t) \text{ V}$

$= 100 \cos(\omega t - 90^\circ) \text{ V}$

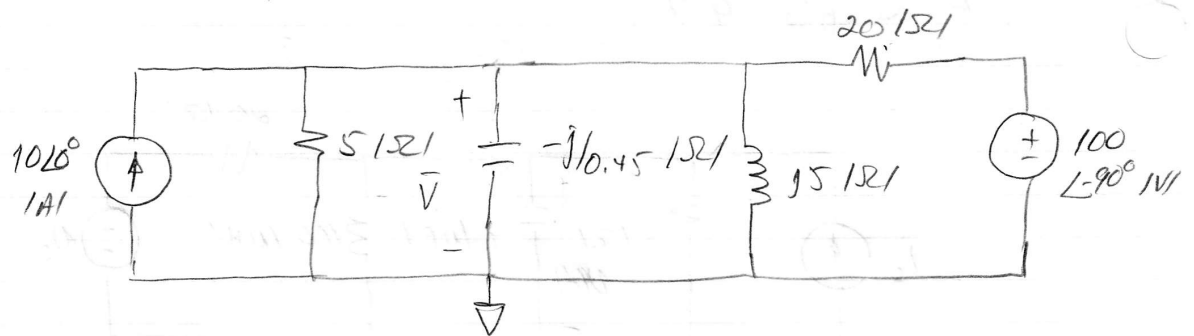
So...  $\bar{I}_s = 10 \angle 0^\circ \text{ A}$

$\bar{V}_s = 100 \angle -90^\circ \text{ V}$

Also:  $j\omega L = j(50 \times 10^3)(100 \times 10^{-6}) = j5 \Omega$

$1/j\omega C = -j/(50 \times 10^3)(9 \times 10^{-6}) = -j/0.45 \Omega$

So in the phasor domain this circuit is:



$$-10 + \frac{\bar{V}}{5} + \frac{\bar{V}}{-j0.45} + \frac{\bar{V}}{j5} + \frac{\bar{V} - 100\angle-90^\circ}{20} = 0$$

$$\bar{V} \left( \frac{1}{5} + \frac{1}{20} + j0.45 - \frac{j}{5} \right) = 10\angle 0^\circ + 5\angle-90^\circ$$

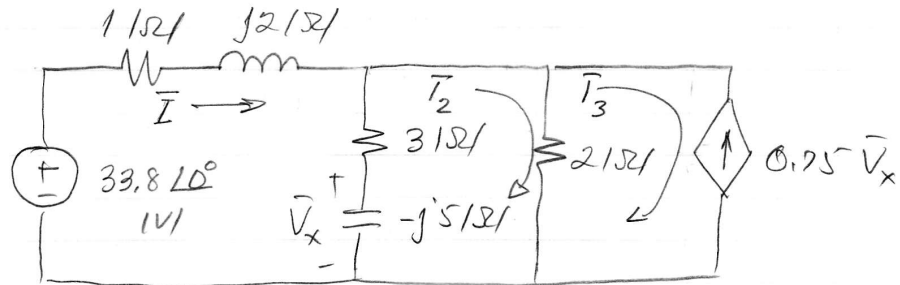
$$\bar{V} = \frac{10 + 5\angle-90^\circ}{0.25 + j0.25} = \frac{10 - j5}{0.25 + j0.25}$$

$$\bar{V} = 10 - j30 \text{ V} = 31.6 \angle -71.6^\circ \text{ V}$$

$$v(t) = 31.6 \cos(\omega t - 71.6^\circ) \text{ V}$$

### Example 9.8

Use the mesh current method to find  $\bar{I}$ .



$$-33.8 + (1+j2)\bar{I} + (3-j5)(\bar{I}-\bar{I}_2) = 0 \quad (1)$$

$$(3-j5)(\bar{I}_2-\bar{I}) + 2(\bar{I}_2-\bar{I}_3) = 0 \quad (2)$$

$$\bar{I}_3 = -0.75\bar{V}_x \quad (3)$$

$$\bar{V}_x = -j5(\bar{I}-\bar{I}_2) \quad (4)$$

$$(3), (4) : \quad \bar{I}_3 = j3.75(\bar{I}-\bar{I}_2)$$

$$(2) : \quad (5-j5)\bar{I}_2 - (3-j5)\bar{I} - j7.5(\bar{I}-\bar{I}_2) = 0$$

$$\Rightarrow (5+j2.5)\bar{I}_2 - (3+j2.5)\bar{I} = 0$$

$$(1) : \quad -(3-j5)\bar{I}_2 + (4-j3)\bar{I} = 33.8$$

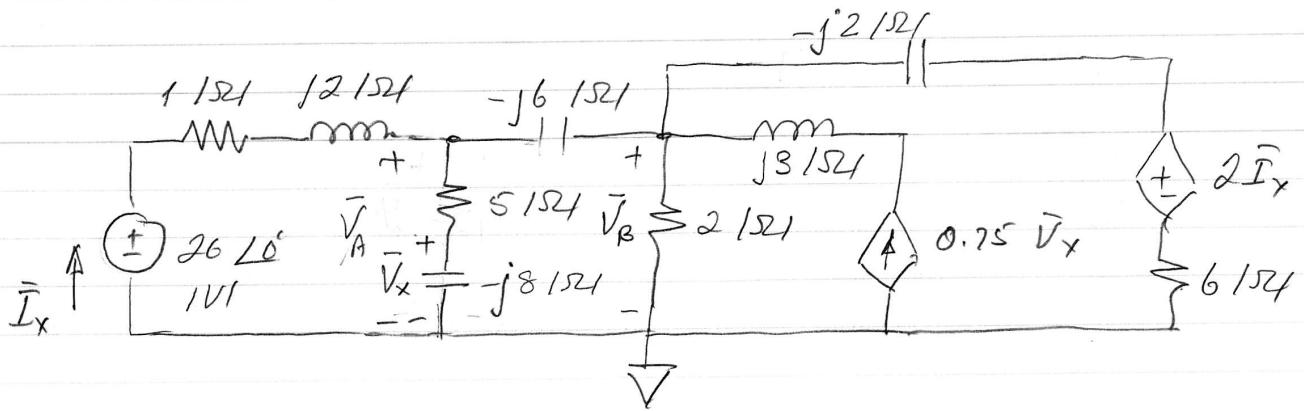
$$\bar{I}_2 = -\bar{I} \frac{(3+j2.5)}{5+j2.5} = (0.68 + j0.16)\bar{I} \quad |A|$$

$$-(3-j5)(0.68+j0.16)\bar{I} + (4-j3)\bar{I} = 33.8$$

$$\bar{I} = \frac{33.8}{-(3-j5)(0.68+j0.16) + (4-j3)}$$

$$\bar{I} = 29.0 + j2 \quad |A| = 29.07 \angle 3.95^\circ \quad |A|$$

### EXAMPLE 9.9



This circuit is already in the phasor domain so no transformation is needed. We write the node voltage equations for  $\bar{V}_A$ ,  $\bar{V}_B$ :

$$\frac{\bar{V}_A}{5-j8} + \frac{\bar{V}_A - 26\angle 0^\circ}{1+j2} + \frac{\bar{V}_A - \bar{V}_B}{-j6} = 0$$

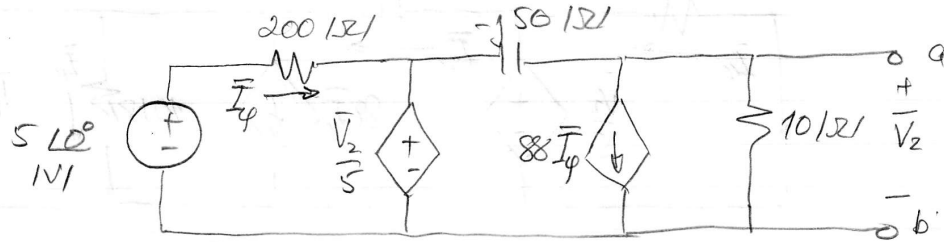
$$\frac{\bar{V}_B}{2} + \frac{\bar{V}_B - \bar{V}_A}{-j6} - 0.75\bar{V}_x + \frac{\bar{V}_B - 2\bar{I}_x}{6-j2} = 0$$

auxiliary:

$$\bar{I}_x = \frac{26\angle 0^\circ - \bar{V}_A}{1+j2}$$

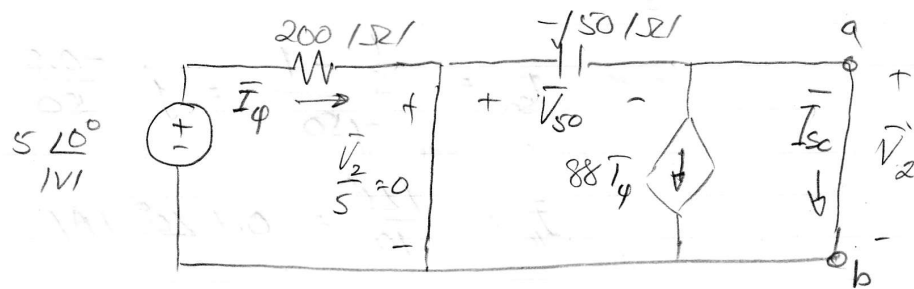
$$\bar{V}_x = \bar{V}_A \cdot \frac{-j8}{5-j8}$$

### EXAMPLE 9.10



Norton Equivalent at a, b:

Find short-circuit current:



If we short-circuit a, b then  $10 \Omega$  has no current in it and  $V_2 = 0$ , so the dependent voltage source is also a short,

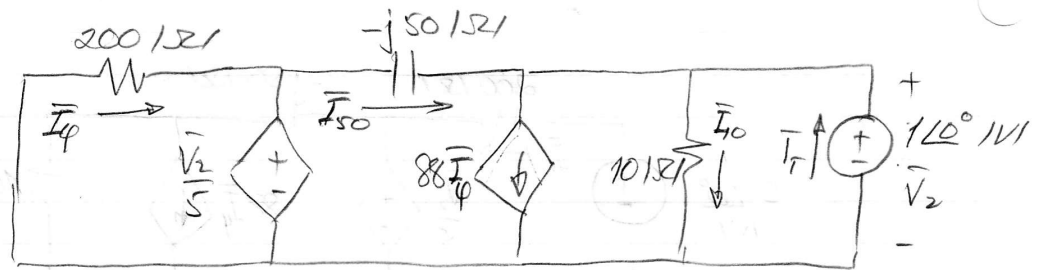
$$\therefore I_\phi = \frac{5 \angle 0^\circ}{200} = 0.025 \angle 0^\circ \text{ A}$$

Also,  $V_{50} = 0$  (KVL through shorts).

$$\therefore I_{sc} = -88 I_\phi = -2.2 \angle 0^\circ \text{ A}$$

Thevenin equivalent impedance:

We will use a test voltage:



$$\bar{V}_2 = 1 \angle 0^\circ \text{ V} \Rightarrow \bar{I}_\phi = \frac{-\bar{V}_2}{1000} = -0.001 \angle 0^\circ \text{ A}$$

$$\text{KVL: } -\frac{\bar{V}_2}{5} + \bar{I}_{50}(-j50) + 1 = 0$$

$$\bar{I}_{50} = \frac{\frac{1}{5} - 1}{-j50} = j \frac{-0.8}{50} = j0.016 \text{ A}$$

$$\bar{I}_{10} = \frac{1 \angle 0^\circ}{10} = 0.1 \angle 0^\circ \text{ A}$$

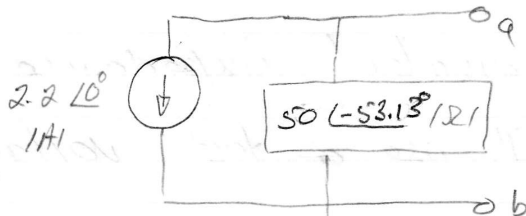
$$\text{KCL: } -\bar{I}_T - \bar{I}_{50} + 88\bar{I}_\phi + \bar{I}_{10} = 0$$

$$\bar{I}_T = -\bar{I}_{50} + 88\bar{I}_\phi + \bar{I}_{10} = 0.012 + j0.016 \text{ A}$$

$$\therefore Z_{Th} = Z_N = \frac{\bar{V}_T}{\bar{I}_T} = \frac{1}{0.012 + j0.016}$$

$$= 50 \angle -53.13^\circ \text{ } [\Omega]$$

$$= 30 - j40 \text{ } [\Omega]$$





(EXAMPLE 9.10 cont)

There is something else we can do here:

The general form of the impedance is

$$Z = R + jX$$

so if  $Z_N = 30 - j40/\Omega$ , we have

$$R = 30 \Omega \quad X = -40/\Omega$$

Now the reactance of a capacitor (the "capacitive reactance") is

$$Z_C = -j/\omega C \Rightarrow X_C = -1/\omega C$$

and the "inductive reactance" is

$$Z_L = j\omega L \Rightarrow X_L = \omega L$$

Since  $X_C$  is negative, we can interpret  $Z_N$  as the impedance of a resistor in series with a capacitance:

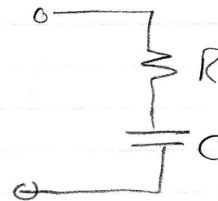
$$Z_N = 30 - j40/\Omega$$

$$X = -4 = -1/\omega C$$

$$\therefore C = 1/\omega \cdot 40$$

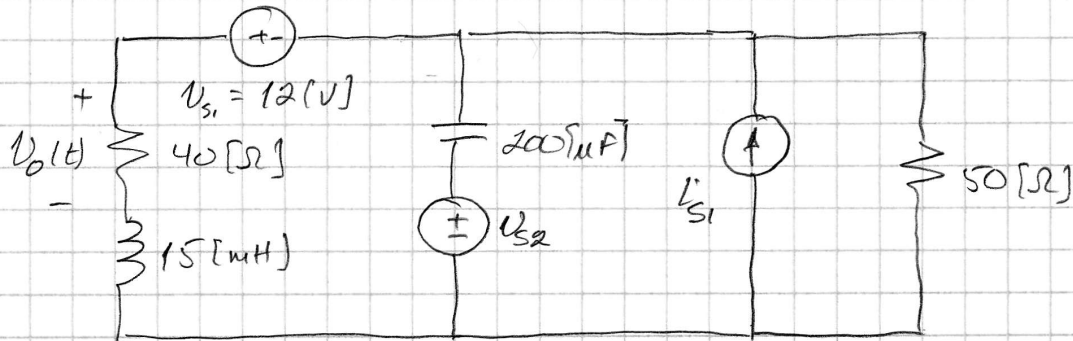
We were not given a frequency here, but say

$$\omega = 10,000 \text{ rad/s} \Rightarrow C = 2.5 \mu\text{F}$$



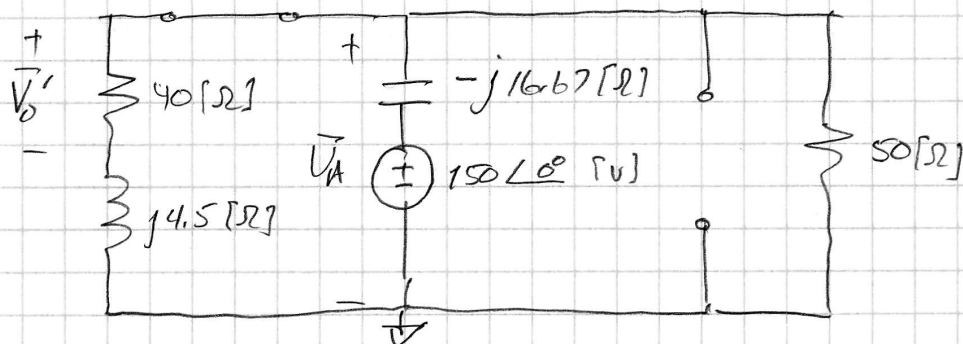
## Problem 9.11

This problem requires superposition to solve, because the sources are at different frequencies.



$$v_{s2} = 150 \cos(300t) \text{ [V]} \quad i_{s1} = 2 \cos(100t) \text{ [A]}$$

consider  $v_{s2}$  first  $\Rightarrow v_{s1} \rightarrow$  short,  $i_{s1} \rightarrow$  open ckt



For  $v_{s1}(t)$ ,  $\omega = 300 \text{ [rad/s]} \Rightarrow L \rightarrow j\omega L = j4.5 \text{ }\Omega$

$$C \rightarrow -j/\omega C = -j16.67 \text{ }\Omega$$

$$\frac{\bar{V}_A - 150}{-j16.67} + \frac{\bar{V}_A}{50} + \frac{\bar{V}_A}{40 + j4.5} = 0$$

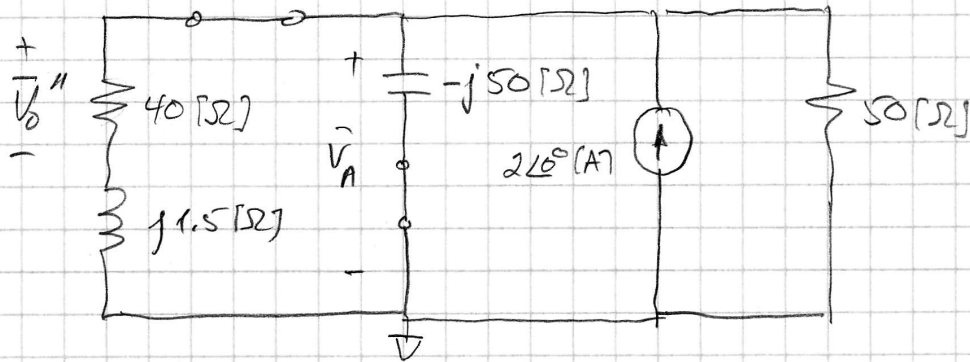
$$\bar{V}_A = 123.96 \angle 38.00^\circ \text{ [V]} \quad \bar{V}_o' = \bar{V}_A \frac{40}{40 + j4.5} = 123.2 \angle 31.58^\circ \text{ [V]}$$

$\rightarrow$

Consider now  $i_{s_1}(t) \Rightarrow \omega = 100 \left[ \frac{\text{rad}}{\text{s}} \right]$  - P9.11 p2 -

$$L \rightarrow j\omega L = j1.5 [\Omega] \quad C \rightarrow -j/\omega C = -j50 [\Omega]$$

$v_{s_2} \rightarrow \text{short}, \quad v_{s_1} \rightarrow \text{short}$

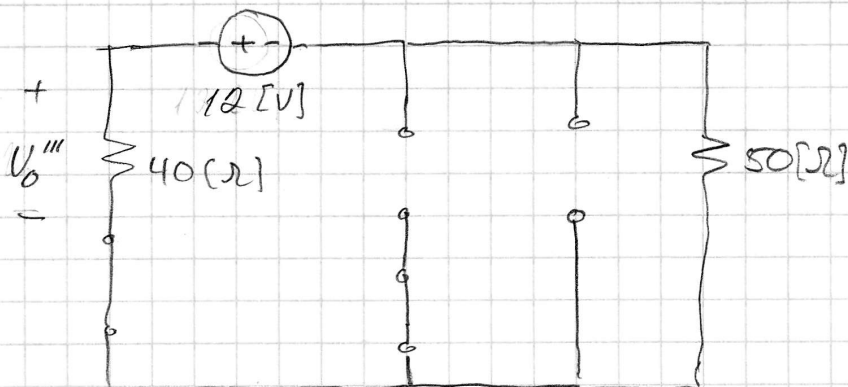


$$\frac{\bar{V}_A}{-j50} + \frac{\bar{V}_A}{40 + j1.5} - 2 + \frac{\bar{V}_A}{50} = 0$$

$$\bar{V}_A = 40.95 \angle -22.98^\circ [\text{V}] \quad \bar{V}_b'' = \bar{V}_A \cdot \frac{40}{40 + j1.5} = 40.92 \angle -25.13^\circ [\text{V}]$$

$v_{s_1}$  is a dc source, for which we take  $\omega = 0$ .  
In that case,  $L \rightarrow \text{short}, \quad C \rightarrow \text{open circuit}$ .

Also,  $v_{s_2} \rightarrow \text{short}, \quad i_{s_1} \rightarrow \text{open}$ .



$\nearrow$

Since there are no reactive components left, we can think of this entirely as a time-domain circuit, but we will continue to phasor notation for consistency.

$$\overline{V}_0''' = 12 \cdot \frac{40}{40+50} = 5.33 \text{ [V]}$$

We now transform back to the time domain, but we have to do it separately for each component of  $V_0$ . Adding phasors does not make sense because they were calculated using different frequencies. So...

$$V_0(t) = 123.2 \cos(300t + 31.58^\circ) \text{ [V]}$$

from  $v_{s2}$   $\nearrow$

$$+ 40.92 \cos(100t - 25.13^\circ) \text{ [V]}$$

from  $i_{s1}$   $\nearrow$   
 $+ 5.33 \text{ [V]}$