

Name: _____ (please print)

Signature: _____

ECE 3455
Exam 1
October 9, 2010

Exam duration: 90 minutes

- You may have one 8 ½ x 11 in. "crib" sheet, written on both sides, during the quiz. You may have any calculator you choose, but no computers. No other notes or materials will be allowed.
- Show all work necessary to complete the problem on these pages. A solution without the work shown will receive no credit.
- Show units in intermediate and final results, and in figures.
- If your work is sloppy or difficult to follow, points will be subtracted.

This exam has 9 pages, including the cover sheet. Raise your hand if you are missing a page.

1 _____ /25

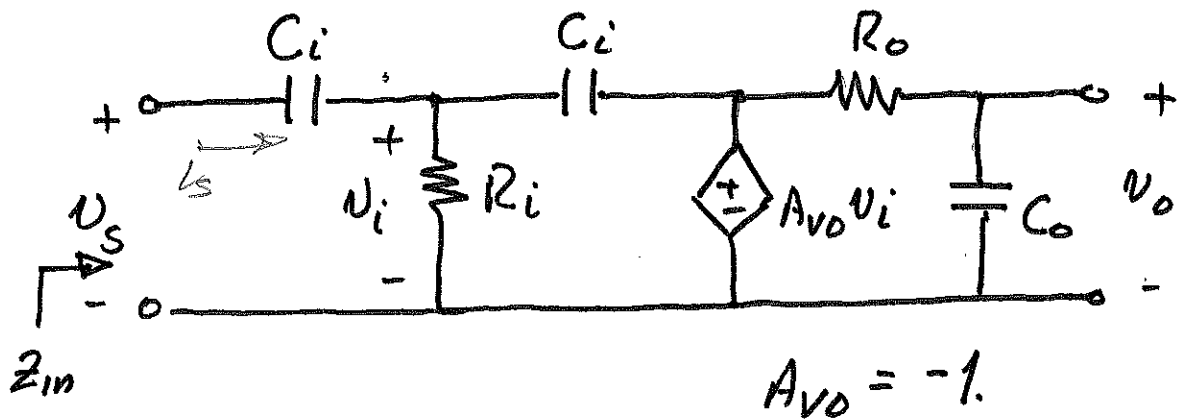
2 _____ /25

3 _____ /25

4 _____ /25

Total _____ /100

1. (25 points) Find the input impedance, Z_{in} , of the circuit below.



$$\frac{\bar{V}_i}{R_i} + \frac{\bar{V}_i - \bar{V}_s}{j\omega C_i} + \frac{\bar{V}_i - A_{vo}\bar{V}_i}{j\omega C_i} = 0$$

$$\Rightarrow \bar{V}_i \left(\frac{1}{R_i} + j\omega C_i + 2j\omega C_i \right) = \bar{V}_s \cdot j\omega C_i$$

$$\therefore \frac{\bar{V}_s}{\bar{V}_i} = \frac{1 + 3j\omega C_i R_i}{j\omega C_i R_i}$$

$$\bar{I}_i = (\bar{V}_s - \bar{V}_i) j\omega C_i = \bar{V}_s \left(1 - \frac{\bar{V}_i}{\bar{V}_s} \right) j\omega C_i$$

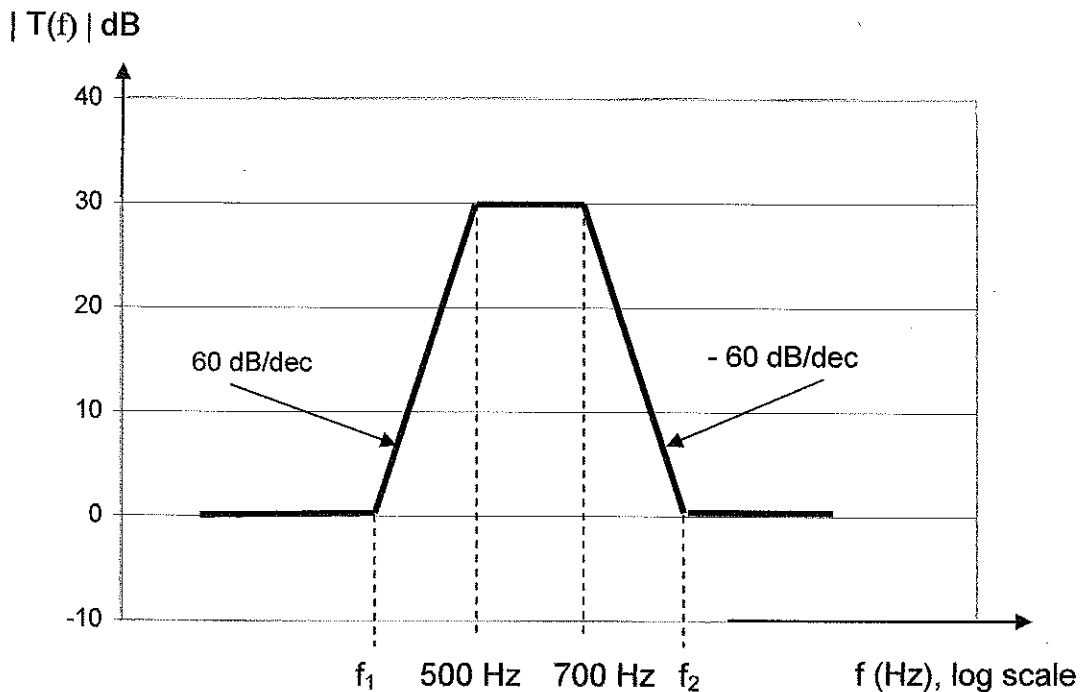
$$= \bar{V}_s \left(1 - \frac{j\omega C_i R_i}{1 + 3j\omega C_i R_i} \right) j\omega C_i$$

$$= \bar{V}_s \left(\frac{1 + 2j\omega C_i R_i}{1 + 3j\omega C_i R_i} \right) j\omega C_i$$

$$\text{Finally } Z_{in} = \frac{\bar{V}_s}{\bar{I}_i} = \frac{1}{j\omega C_i} \frac{1 + 3j\omega C_i R_i}{1 + 2j\omega C_i R_i}$$

2. (25 points) The figure below shows the straight-line approximation to the magnitude Bode plot for a certain filter. As the figure shows, the gain between 500 Hz and 700 Hz is 30 dB, and drops off on either side at 60 dB/dec. The gain levels off at 0 dB at frequencies f_1 and f_2 . There are no poles or zeros outside the region shown in the plot. Note that the plot is merely a sketch: it is NOT drawn to scale, and should not be used for quantitative calculations.

- It is known that the transfer function $T(f)$ is multiplied by a constant that is real and negative. Find the transfer function.
- What is the phase of the transfer function as f approaches infinity?



The slopes are 60 dB/dec and run for 30 dB, which means that f_1 and 500 Hz are separated by $\frac{1}{2}$ dec, as are 700 Hz and f_2 .

So... $\frac{500 \text{ Hz}}{f_1} = 10^{0.5}$

$$\frac{f_2}{700 \text{ Hz}} = 10^{0.5}$$

$$\Rightarrow f_1 \approx 160 \text{ Hz}$$

$$f_2 \approx 2200 \text{ Hz}$$

+5

Poles & Zeros:

+4
 z_1 at 160 Hz P_1 at 500 Hz
 z_2 at 2200 Hz P_2 at 700 Hz

} 3 times each!
(± 60 dB/dec)

$$T(f) = K \frac{(1 + jf/160)^3 (1 + jf/2200)^3}{(1 + jf/500)^3 (1 + jf/700)^3}$$

We need K :

+4 For $f \rightarrow 0$, $T(f) \rightarrow K$, and $|T(f)| \rightarrow 0$ dB
 $\Rightarrow 1$ V/V

So $K = -1$. (negative since we are told this!)

+10

$$T(f) = -1 \cdot \frac{(1 + jf/160)^3 (1 + jf/2200)^3}{(1 + jf/500)^3 (1 + jf/700)^3}$$

+2
ii) For f large, $T(f) \rightarrow -1 \Rightarrow \angle T(f) \rightarrow 180^\circ$

If we had evaluated $|T(f)|$ at, say, 600 Hz, we would find

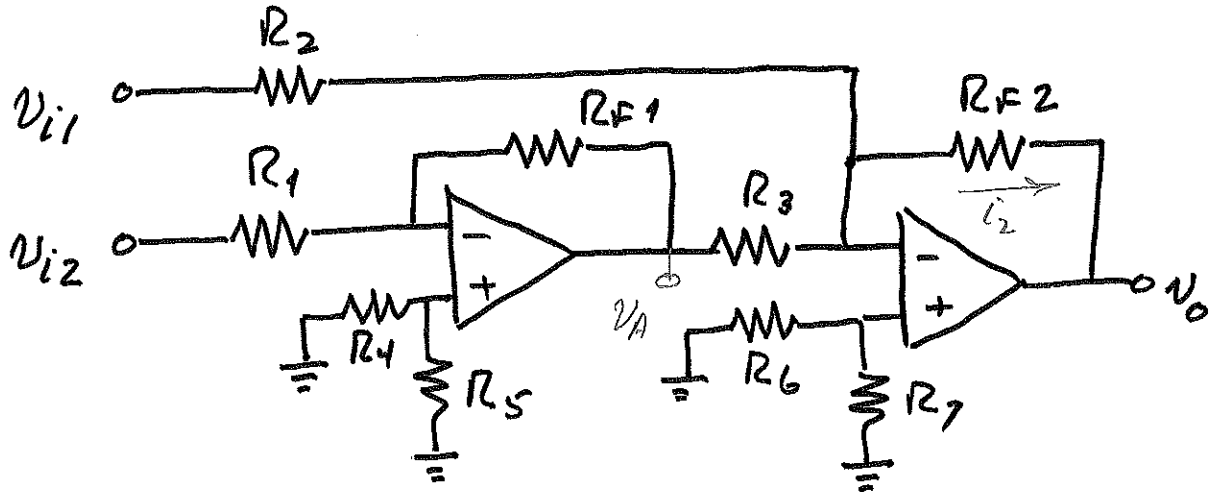
$$|T(f)| = |K| \cdot \left| \frac{(1 + j600/160)^3 (1 + j600/2200)^3}{(1 + j600/500)^3 (1 + j600/700)^3} \right| = |K| \times 2.48 = 10^{30/20}$$

$$\Rightarrow |K| = 4.23$$

Why the discrepancy? Because the break points are so close together that the actual function $|T(f)|$ does not reach 30 dB at 600 Hz: It is about 17.5 dB there. No credit was subtracted if K was found this way.

$$A_d (v_{i2} - v_{i1})$$

3. (25 points) If the resistances in the circuit below are chosen appropriately, the circuit is a differential amplifier, i.e., $v_o = A_d(v_{i1} - v_{i2})$. Choose resistances so that the differential gain A_d is 10, and the input resistance seen by v_{i1} and v_{i2} are each 5 k Ω . Assume the op amps are ideal.



$$v_A = -\frac{R_{F1}}{R_1} v_{i2}$$

$$i_2 = \frac{v_A}{R_3} + \frac{v_{i1}}{R_2}$$

$$R_1 = R_2 = 5 \text{ k}\Omega$$

$$R_{F1} = R_3 = 10 \text{ k}\Omega$$

$$R_{F2} = 50 \text{ k}\Omega$$

$$R_{4,5,6,7} = \text{anything}$$

$$\therefore v_o = -\frac{R_{F2}}{R_3} v_A - v_{i1} \frac{R_{F2}}{R_2}$$

$$= \frac{R_{F2} R_{F1}}{R_1 R_3} v_{i2} - \frac{R_{F2}}{R_2} v_{i1}$$

For $R_i = 5 \text{ k}\Omega$ for each input, we need

$$R \equiv R_2 = R_1 = 5 \text{ k}\Omega.$$

For $v_o = A_d (v_{i2} - v_{i1})$ we need

$$\frac{R_{F2} R_{F1}}{R R_3} = \frac{R_{F2}}{R} \Rightarrow \frac{R_{F1}}{R_3} = 1$$

$$\text{Choose } R_{F1} = R_3 = 10 \text{ k}\Omega \Rightarrow R_{F2} = 50 \text{ k}\Omega$$

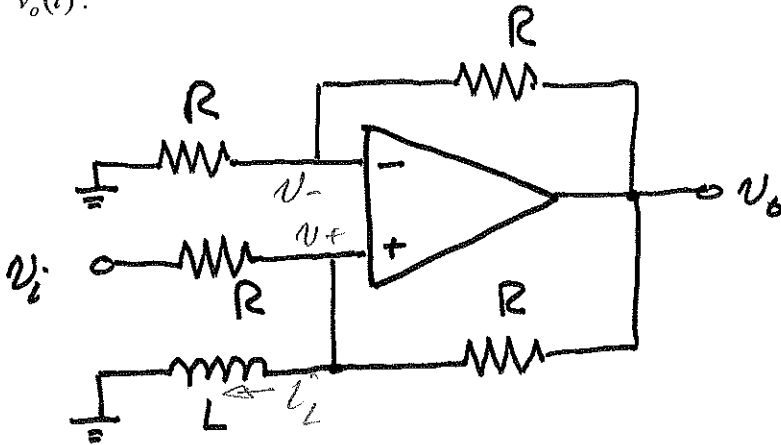
$$R_4, R_5, R_6, R_7 \text{ have no effect} \rightarrow 10 \text{ k}\Omega$$

4. (25 points) For the circuit below, assume the op amp is ideal.

i) Find $v_o(t)$ as a function of $v_i(t)$ for arbitrary $v_i(t)$.

ii) Find the transfer function $T(\omega) = \frac{\bar{V}_o}{\bar{V}_i}$.

iii) Show that if $v_i(t) = V_m \cos(\omega t)$, your answers to part i) and part ii) predict the same thing for $v_o(t)$.



i)

$$v_- = v_+ = \frac{1}{2} v_o \quad \frac{1}{2} \frac{v_o - v_i}{R} + \frac{1}{2} \frac{v_o - v_o}{R} + \frac{1}{L} \int \frac{1}{2} v_o dt + i_L(0) = 0$$

$$\Rightarrow -\frac{v_i}{R} + \frac{1}{L} \int \frac{1}{2} v_o dt + i_L'(0) = 0$$

$$-\frac{1}{R} \frac{dv_i}{dt} + \frac{1}{2L} v_o = 0$$

$$\Rightarrow v_o = \frac{2L}{R} \frac{dv_i}{dt}$$

ii)

$$\frac{1}{2} \frac{\bar{V}_o - \bar{V}_i}{R} + \frac{1}{2} \frac{\bar{V}_o - \bar{V}_o}{R} + \frac{1}{j\omega L} \bar{V}_o = 0$$

$$\Rightarrow \bar{V}_o = \frac{2j\omega L}{R} \bar{V}_i$$

$$\frac{\bar{V}_o}{\bar{V}_i} = \frac{2j\omega L}{R}$$

Room for extra work

iii)

$$V_i = V_m \cos \omega t$$

$$\frac{dV_i}{dt} = -\omega V_m \sin \omega t$$

$$V_o = -\frac{2L\omega}{R} V_m \sin \omega t$$

$$\bar{V}_i = V_m \angle 0^\circ$$

$$\bar{V}_o = \frac{2j\omega L}{R} V_m \angle 0^\circ$$

$$= \frac{2\omega L}{R} V_m \angle 90^\circ$$

$$\Rightarrow V_o = \frac{2L\omega}{R} V_m \cos(\omega t + 90^\circ)$$

$$V_o = -\frac{2L\omega}{R} V_m \sin(\omega t)$$

P.E.D.