

Name: _____ (please print)

Signature: _____

ECE 3455
Exam 1
March 7, 2009

Exam duration: 90 minutes

- You may have one 8 ½ x 11 in. “crib” sheet, written on both sides, during the quiz. You may have any calculator you choose, but no computers. No other notes or materials will be allowed.
- Show all work necessary to complete the problem on these pages. A solution without the work shown will receive no credit.
- Show units in intermediate and final results, and in figures.
- If your work is sloppy or difficult to follow, points will be subtracted.

This exam has 10 pages, including the cover sheet. Raise your hand if you are missing a page.

1 _____ /25

2 _____ /25

3 _____ /25

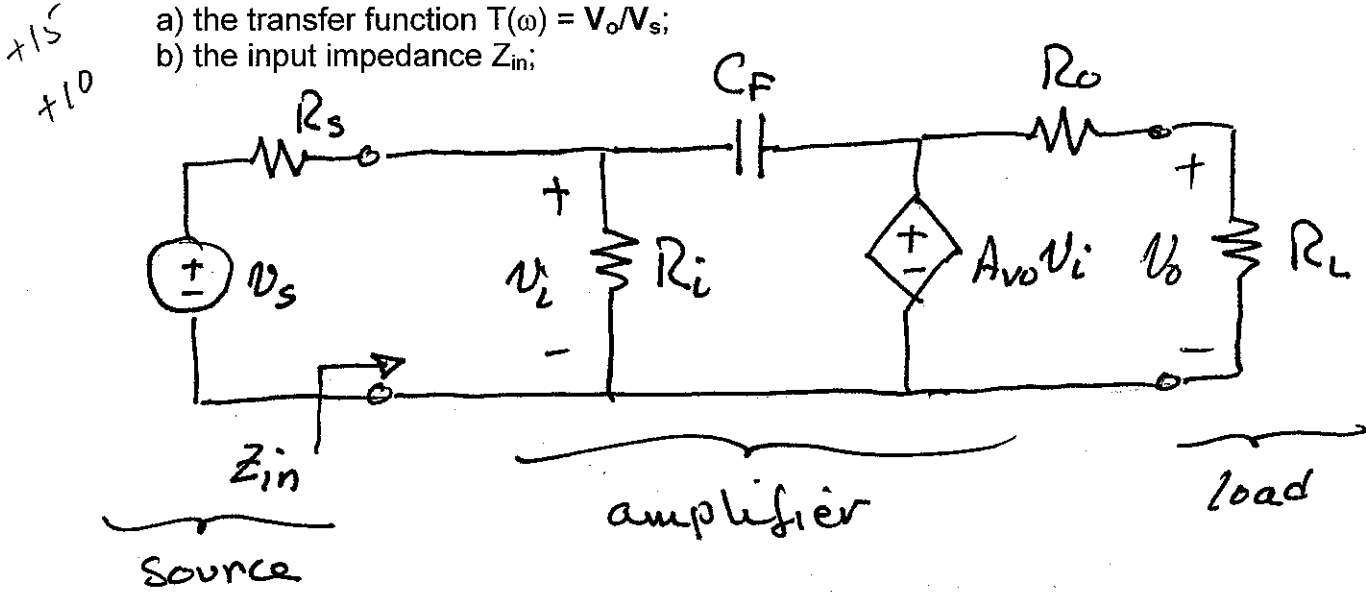
4 _____ /25

Total _____ /100

Room for Extra Work

1. (25 points) For the circuit shown below, find

- a) the transfer function $T(\omega) = V_o/V_s$;
 b) the input impedance Z_{in} ;



a)
$$\bar{V}_o = A_{vo} \bar{V}_i \frac{R_L}{R_L + R_o} \quad \bar{V}_i + \frac{\bar{V}_i - A_{vo} \bar{V}_i}{\frac{1}{j\omega C_F}} + \frac{\bar{V}_i - \bar{V}_s}{R_s} = 0$$

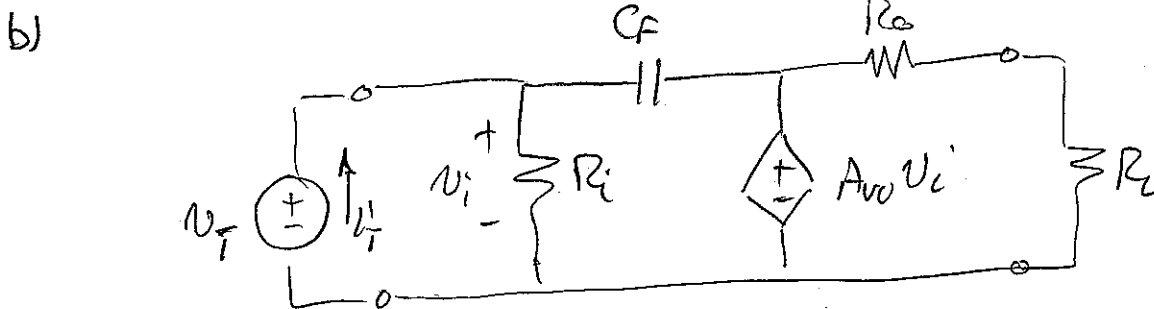
+10

$$\bar{V}_i \left(\frac{1}{R_i} + \frac{1}{R_s} + (1 - A_{vo}) j\omega C_F \right) = \frac{\bar{V}_s}{R_s}$$

+5

$$\bar{V}_i \left(\frac{R_s}{R_i} + 1 + R_s (1 - A_{vo}) j\omega C_F \right) = \bar{V}_s$$

$$\boxed{\frac{\bar{V}_o}{\bar{V}_s} = A_{vo} \frac{R_L}{R_L + R_o} \cdot \frac{1}{\frac{R_s}{R_i} + 1 + j\omega C_F R_s (1 - A_{vo})}}$$



Room for extra work

$$+6 \quad \bar{I}_T = \frac{\bar{V}_i}{R_i} + \frac{\bar{V}_i(1-A_{vo})}{1/j\omega C_F} = \bar{V}_i \left(\frac{1}{R_i} + j\omega C_F(1-A_{vo}) \right)$$

$$\bar{V}_i = \bar{V}_T \Rightarrow \frac{V_T}{I_T} = \frac{1}{\frac{1}{R_i} + j\omega C_F(1-A_{vo})}$$

$$+4 \quad Z_{in} = \frac{R_i}{1 + j\omega C_F R_i (1 - A_{vo})}$$

Any correct algebraic expressions for V_o/\bar{V}_s and Z_{in} that are written in terms of R_L , R_o , C_F , R_i , and A_{vo} are acceptable for full credit.

2. (25 points) The transfer function $T(\omega)$ for a certain amplifier is shown below. It is known that the magnitude of the transfer function at $\omega = 300$ rad/sec is approximately 0 dB.

We are given that $R_1C_1 = 5 \times 10^{-5}$ s; $R_2C_2 = 3.333 \times 10^{-4}$ s; $R_3C_3 = 1.667 \times 10^{-3}$ s; and $R_4C_4 = 10^{-3}$ s. (Note that the value for R_3C_3 is slightly modified from that on the recent quiz.)

$$T(\omega) = K \frac{\left(\frac{1}{R_1C_1} + j\omega\right)(j\omega R_4C_4)^2}{(1 + j\omega R_2C_2)^2 \left(\frac{1}{R_3C_3} + 3j\omega\right)}$$

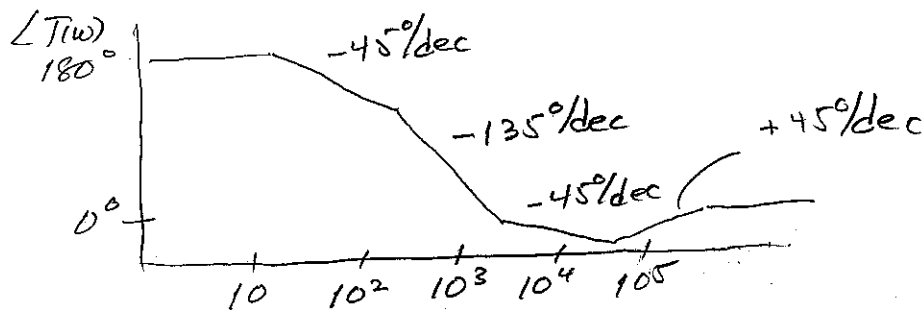
Using the paper provided on the next page, draw the straight-line approximation to the phase Bode plot for this transfer function.

We have zeros at 0 (double) and $\frac{1}{R_4C_4} = 20000$ rad/s
 We have poles at $\frac{1}{3R_3C_3} = 200$ rad/s and
 $\frac{1}{R_2C_2} = 3000$ rad/s (double).

The zeros at 0 have no affect on the slopes of the phase Bode plot.

The phase plot enters at $\angle T(\omega \rightarrow 0) \rightarrow (j\omega R_4C_4)^2 \rightarrow 180^\circ$.

Rough sketch:



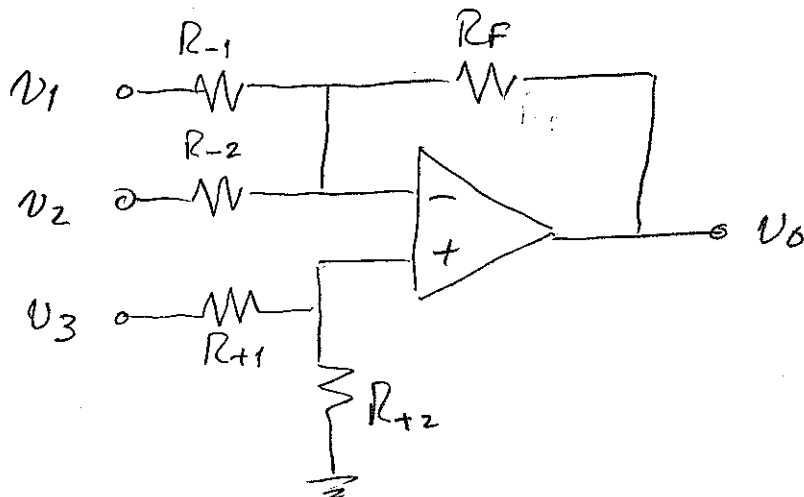
3. (25 points) Use "ideal" op amps to generate a voltage output given by

$$v_o = -0.4v_1 - 0.8v_2 + 0.2v_3$$

where v_1 , v_2 , and v_3 are independent input sources.

For partial credit (10 points), use any number of op amps to generate the required output.

For full credit (25 points), use only one op amp to generate the required output.



+12: basic configuration:

$$R_F/R_{-1} \quad +4$$

$$R_F/R_{-2} \quad +4$$

$$\left. \begin{matrix} R_{+1} \\ R_{+2} \end{matrix} \right\} +5$$

Using superposition, we set $v_2 = v_3 = 0$. Then we have a simple inverting configuration:

$$v_{o1} = -\frac{R_F}{R_{-1}} v_1$$

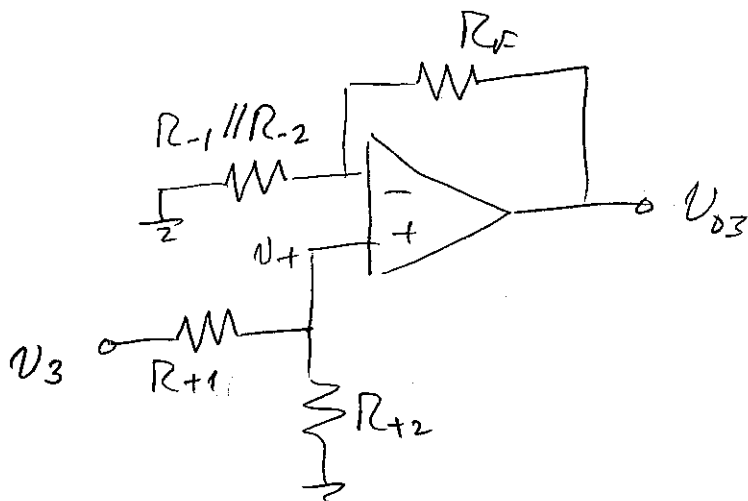
Clearly we will have the same thing for

$v_1 = v_3 = 0$ and

$$v_{o2} = \frac{-R_F}{R_{-2}} v_2$$

Room for extra work

Set $v_1 = v_2 = 0$ and re-draw:



Summary:

$$\begin{aligned} R_{-1} &= 25 \text{ k}\Omega \\ R_{-2} &= 12.5 \text{ k}\Omega \\ R_F &= 10 \text{ k}\Omega \\ R_{t1} &= 10 \text{ k}\Omega \\ R_{t2} &= 1 \text{ k}\Omega \end{aligned}$$

$$v_{o3} = v_+ \left(1 + \frac{R_F}{R_{-1} \parallel R_{-2}} \right) \quad v_+ = v_3 \frac{R_{t2}}{R_{t1} + R_{t2}}$$

$$v_{o3} = v_3 \frac{1}{\frac{R_{t1}}{R_{t2}} + 1} \left(1 + \frac{R_F}{R_{-1} \parallel R_{-2}} \right)$$

Choose $R_F = 10 \text{ k}\Omega$ (arbitrary). Then

$$\frac{R_F}{R_{-1}} = 0.4 \Rightarrow R_{-1} = \frac{R_F}{0.4} = 25 \text{ k}\Omega$$

$$\frac{R_F}{R_{-2}} = 0.8 \Rightarrow R_{-2} = \frac{R_F}{0.8} = 12.5 \text{ k}\Omega$$

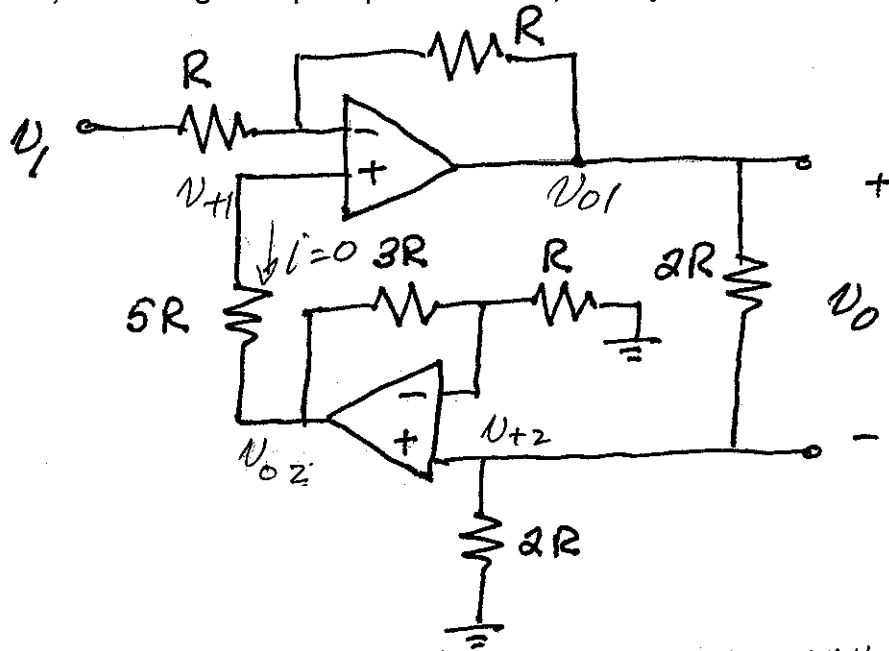
$$\Rightarrow 1 + \frac{R_F}{R_{-1} \parallel R_{-2}} = 1 + \frac{10}{25 \parallel 12.5} = 2.2$$

$$\frac{1}{\frac{R_{t1}}{R_{t2}} + 1} \cdot 2.2 = 0.2 \Rightarrow \frac{R_{t1}}{R_{t2}} = 10$$

choose $R_{t1} = 10 \text{ k}\Omega$

$R_{t2} = 1 \text{ k}\Omega$

4. (25 points) Assuming the op amps are "ideal", find v_o .



NON-INV. analysis + 6

INV analysis + 6

coupling + 13

NON-INV

$$v_{t1} = v_{o2} = v_{t2} \left(1 + \frac{3R}{R}\right) = 4v_{t2}$$

INV

$$v_{o1} - v_{t1} + \frac{v_1 - v_{t1}}{R} \cdot R = 0$$

$$v_{o1} = 2v_{t1} = v_1 = 4v_{t2} - v_1$$

$$v_{t2} = v_{o1} \frac{2R}{2R+2R} = \frac{1}{2} v_{o1}$$

coupling

$$\therefore v_{o1} = 2v_{o1} - v_1 \Rightarrow v_{o1} = \frac{1}{3} v_1$$

$$v_o = \frac{2R}{2R+2R} v_{o1} = \frac{1}{2} v_{o1}$$

$$v_o = \frac{1}{6} v_1$$

Room for extra work