

# ECE 5317-6351

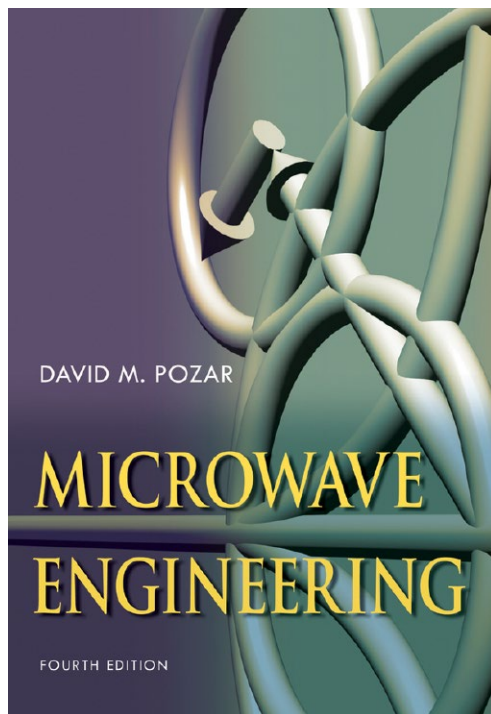
# Microwave Engineering

**Fall 2019**

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Dept. of ECE

## Notes 17

## S-Parameter Measurements



# *S*-Parameter Measurements

*S*-parameters are typically measured, at microwave frequencies, with a network analyzer (NA).

These instruments have found wide, almost universal, application since the mid to late 1970's.

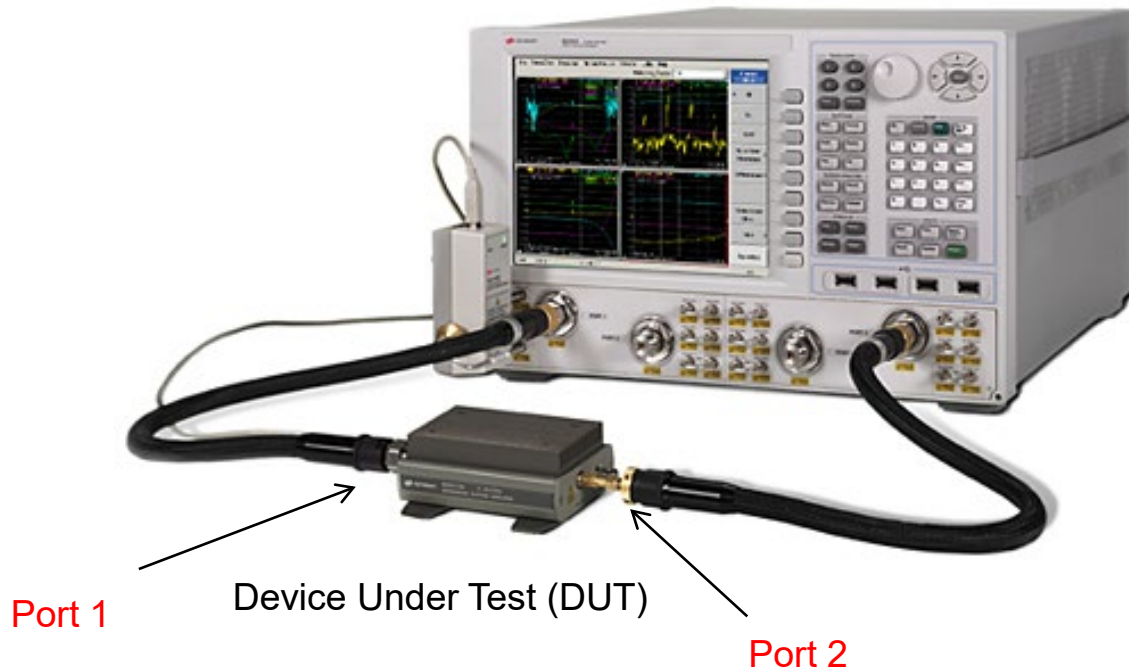
- ❖ Vector\* network analyzer: Magnitudes and phases of the *S* parameters are measured.
- ❖ Scalar network analyzer: Only the magnitudes of the *S*-parameters are measured.

Most NA's measure 2-port parameters. Some measure 4 and 6 ports.

\* The *S* parameters are really complex numbers, not vectors, but this is the customary name. There is an analogy between complex numbers and 2D vectors.

# $S$ -Parameter Measurements (cont.)

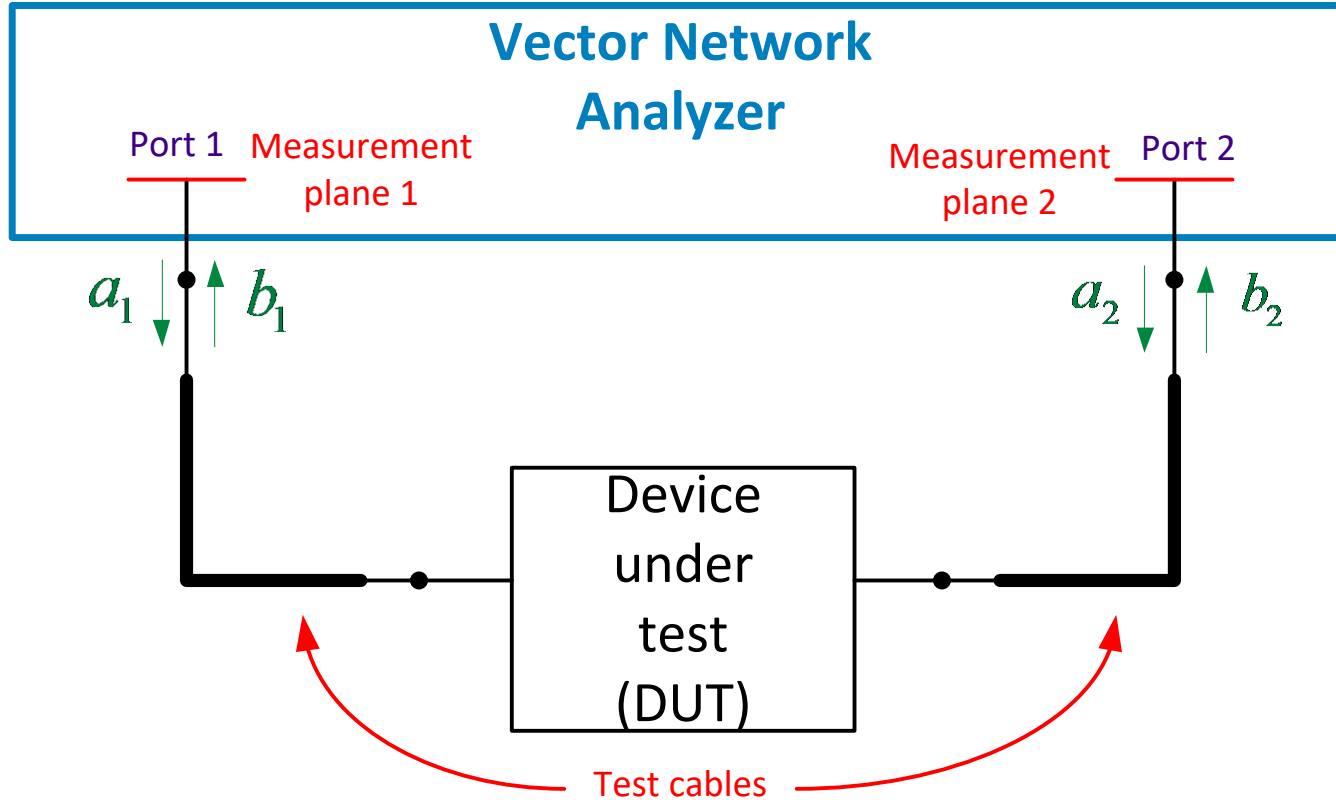
A Vector Network Analyzer (VNA) is usually used to measure  $S$  parameters.



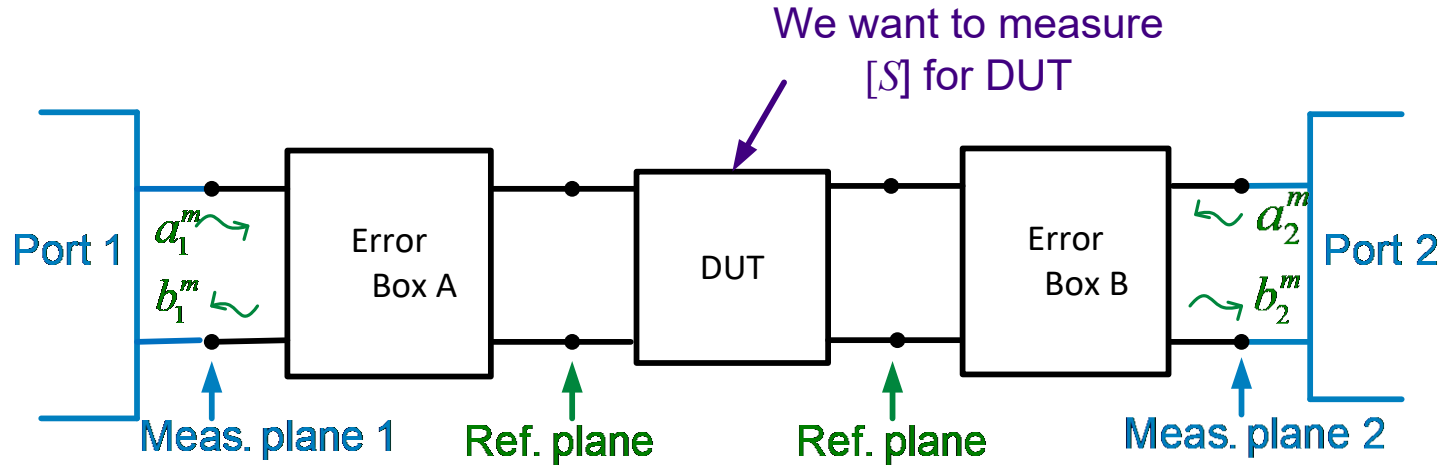
**Note:**

If there are more than 2 ports, we measure different pairs of ports separately with a 2-port VNA.

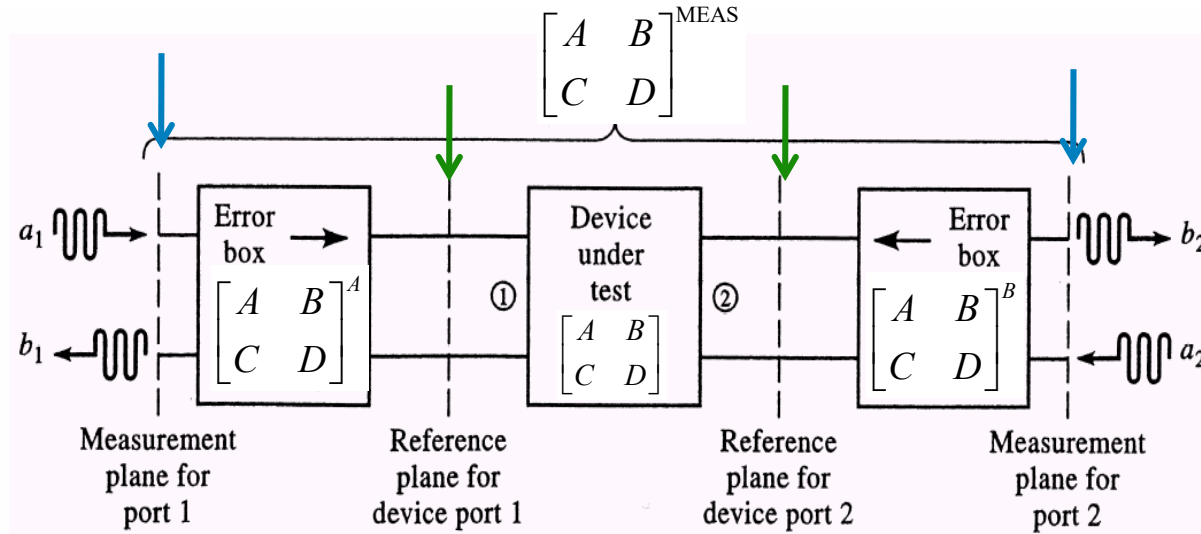
# S-Parameter Measurements (cont.)



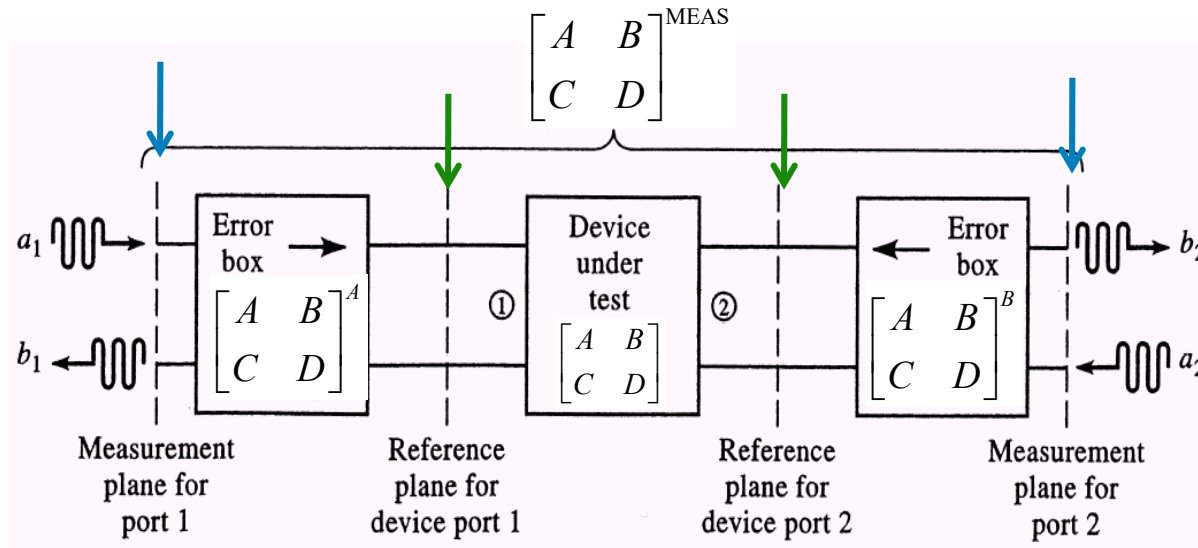
# S-Parameter Measurements (cont.)



Error boxes contain effects of test cables, connectors, couplers,...



# S-Parameter Measurements (cont.)



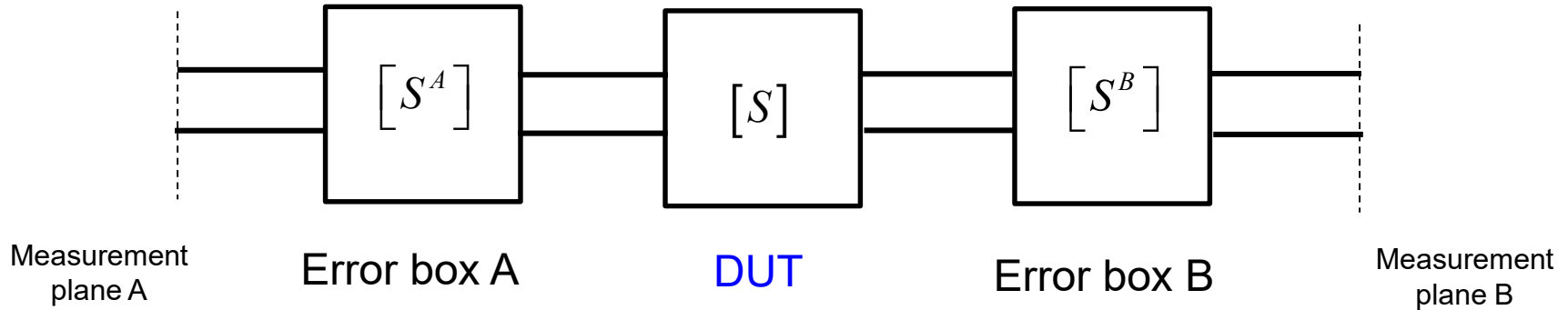
$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}^{\text{MEAS}} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}^A \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} A & B \\ C & D \end{bmatrix}^B$$

Embedded inside measured ABCD matrix

De-embedded

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \left( \begin{bmatrix} A & B \\ C & D \end{bmatrix}^A \right)^{-1} \begin{bmatrix} A & B \\ C & D \end{bmatrix}^{\text{MEAS}} \left( \begin{bmatrix} A & B \\ C & D \end{bmatrix}^B \right)^{-1}$$

# S-Parameter Measurements (cont.)



Assume error boxes are reciprocal (symmetric matrices)

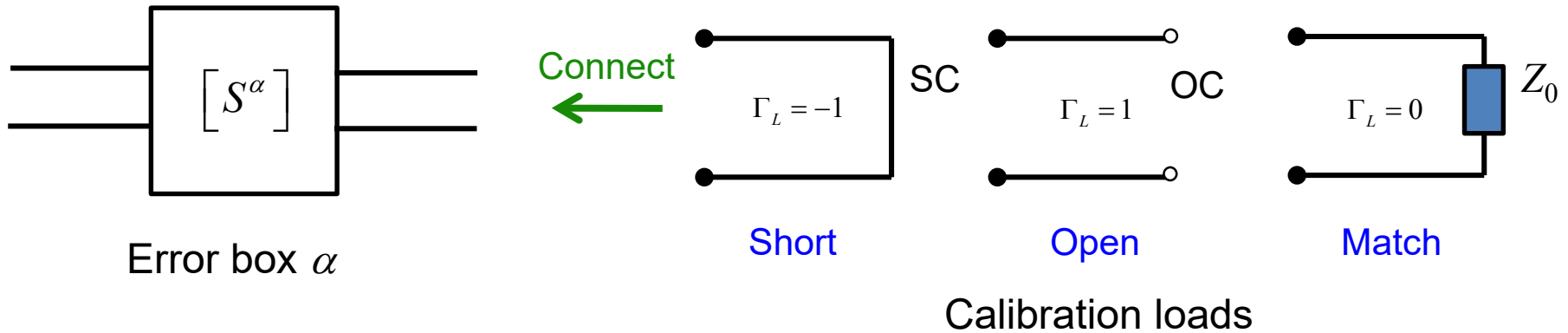
We need to "calibrate" to find  $[S^A]$  and  $[S^B]$ .

If  $[S^A]$  and  $[S^B]$  are known  $\Rightarrow$  we can extract  $[S]$  from measurements.

This is called "de-embedding".

# Calibration

## “Short, open, match” calibration procedure



These loads are connected to the end of the cable from the VNA.

$$S_{11_{SC}}^m = S_{11}^\alpha - \frac{(S_{21}^\alpha)^2}{1 + S_{22}^\alpha}$$

$$S_{11_{OC}}^m = S_{11}^\alpha + \frac{(S_{21}^\alpha)^2}{1 - S_{22}^\alpha}$$

$$S_{11_{match}}^m = S_{11}^\alpha$$

3 measurements:

$$(S_{11_{SC}}^m, S_{11_{OC}}^m, S_{11_{match}}^m)$$

3 unknowns:

$$(S_{11}^\alpha, S_{21}^\alpha, S_{22}^\alpha)$$

Recall from Notes 16:

$$\Gamma_{in} = S_{11} + \frac{S_{21}S_{12}\Gamma_L}{1 - \Gamma_L S_{22}}$$



# Calibration (cont.)

## “Thru-Reflect-Line (TRL)” calibration procedure

This is an improved calibration method that involves three types of connections:

- 1) The “thru” connection, in which port 1 is directly connected to port 2.
- 2) The “reflect” connection, in which a load with an (ideally) large (but not necessarily precisely known) reflection coefficient is connected.
- 3) The “line” connection, in which a length of matched transmission line (with an unknown length) is connected between ports 1 and 2.

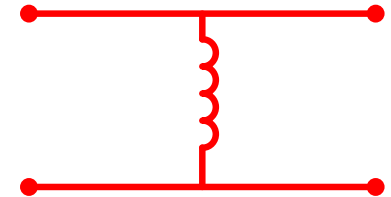
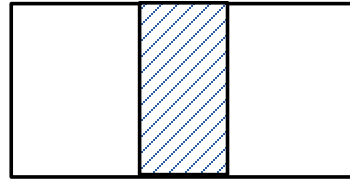
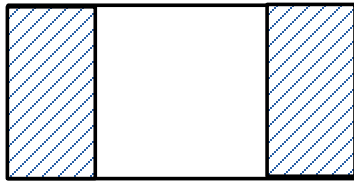
The advantage of the TRL calibration is that it does not require precise short, open, and matched loads.

This method is discussed in the Pozar book (pp. 193-196).

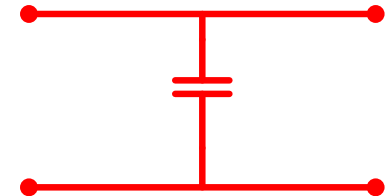
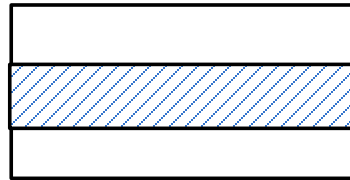
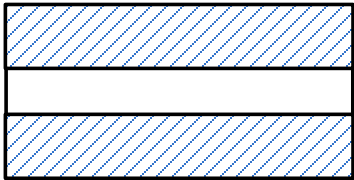
# Discontinuities

- ❖ In microwave engineering, discontinuities are often represented by pi or tee networks.
- ❖ Sometimes the pi or tee network reduces to a single series or shunt element.
- ❖ For waveguide systems, the TEN is used to represent the waveguide.

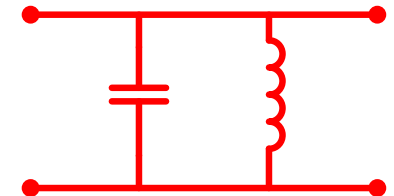
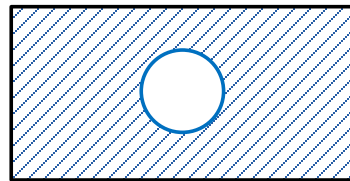
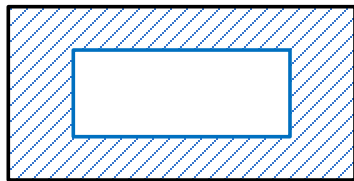
# Discontinuities: Rectangular Waveguide



Inductive iris or strip

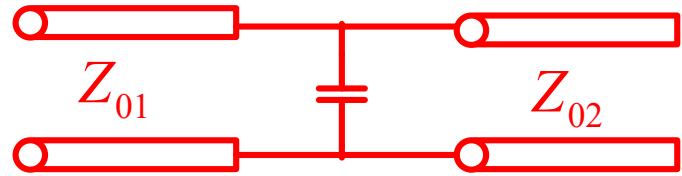
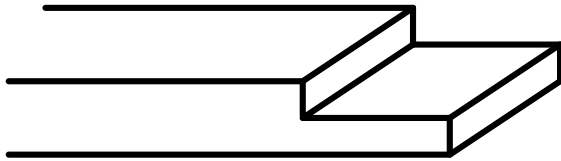


Capacitive iris or strip

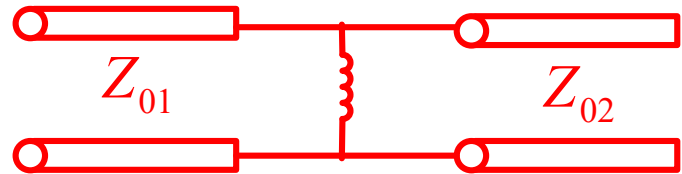
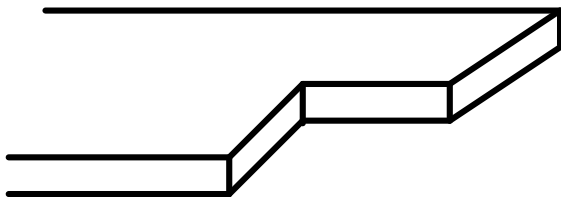


Resonant iris

# Discontinuities: RWG (cont.)

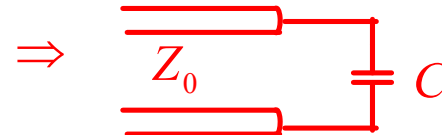
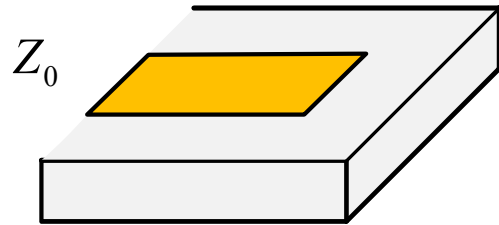


E plane step

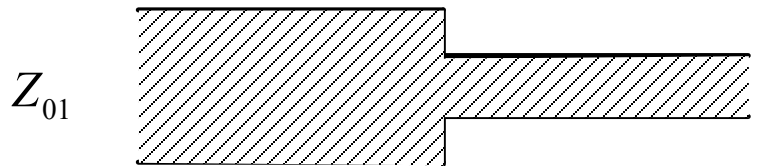
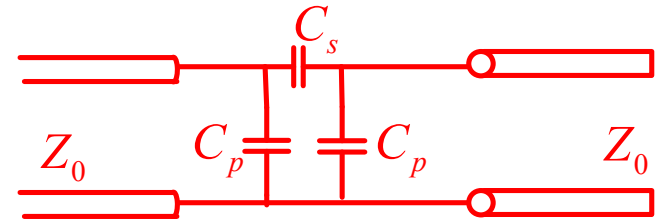


H plane step

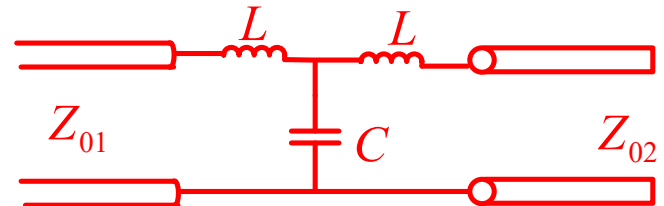
# Discontinuities: Microstrip



$Z_0 \Rightarrow$



$Z_{02} \Rightarrow$

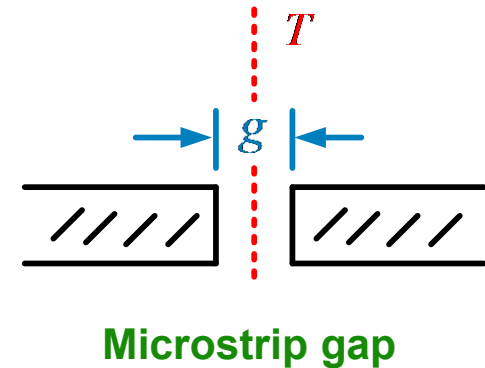
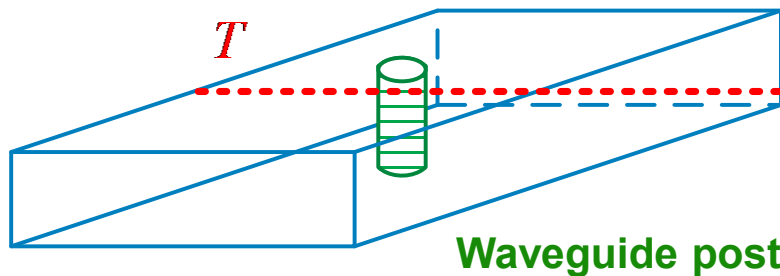


**Note:**  
For a good equivalent circuit,  
the element values are fairly stable over a wide range of frequencies.

# Z-Parameter Extraction

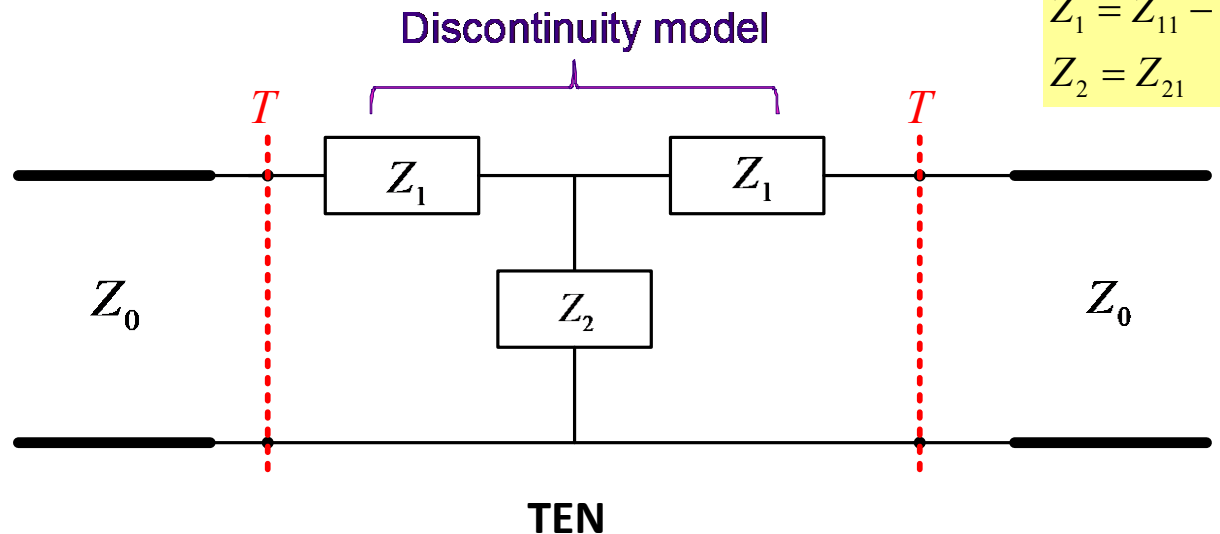
Assume a reciprocal and symmetrical waveguide or transmission-line discontinuity.

## Examples

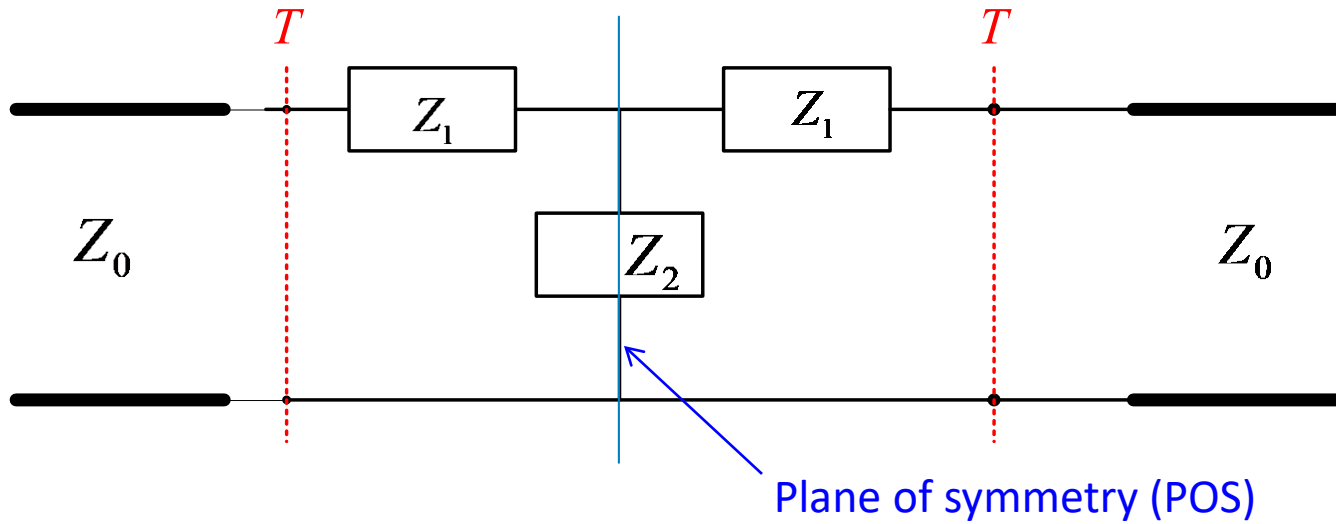


We want to find  $Z_1$  and  $Z_2$  to model the discontinuity.

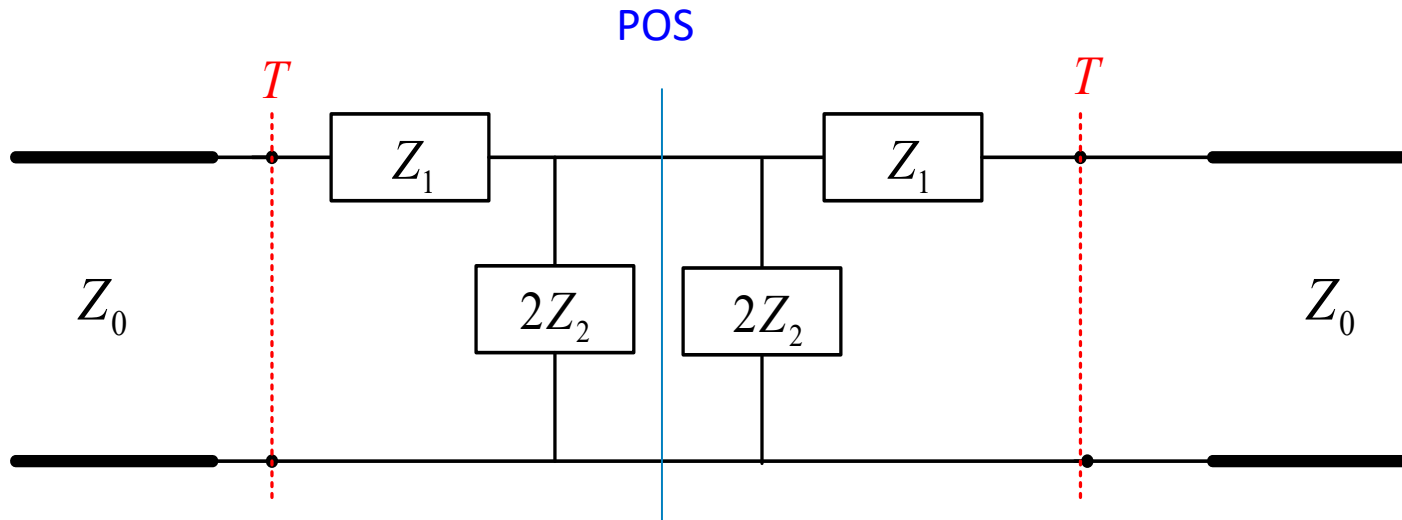
**Note:**  
We could also use a pi network if we wish.



# Z-Parameter Extraction (cont.)

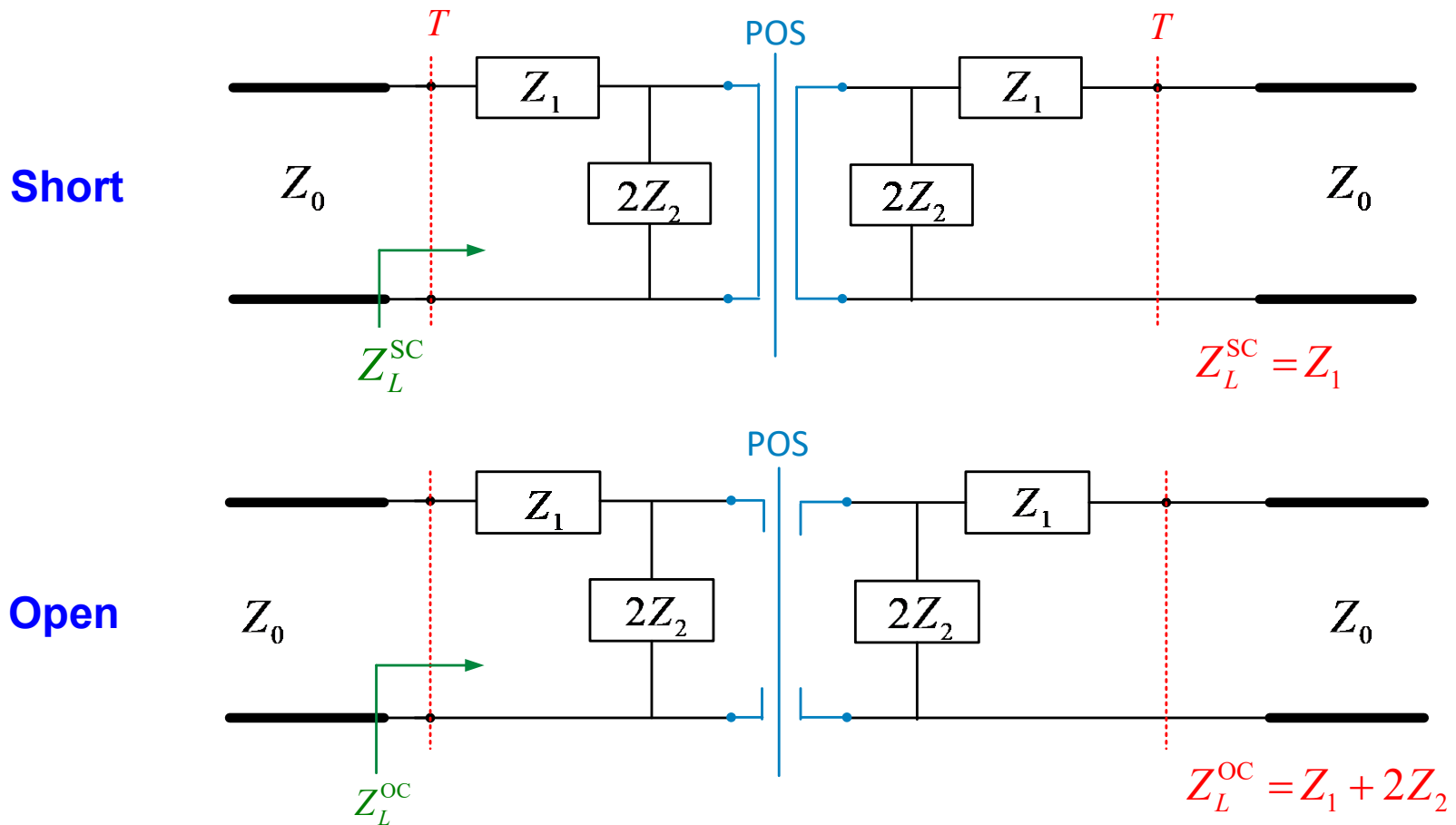


The  $Z_2$  element is split in two:



# Z-Parameter Extraction (cont.)

Assume that we place a short or an open along the plane of symmetry.

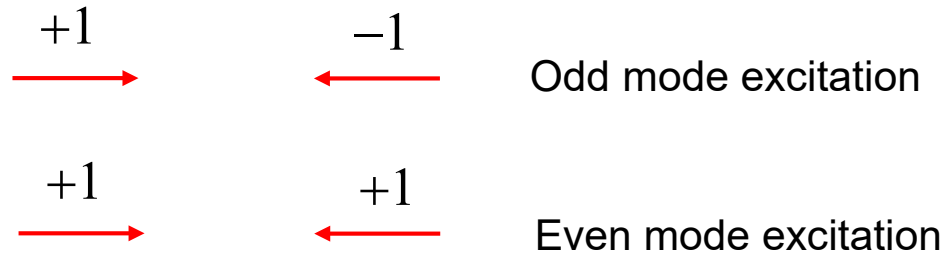
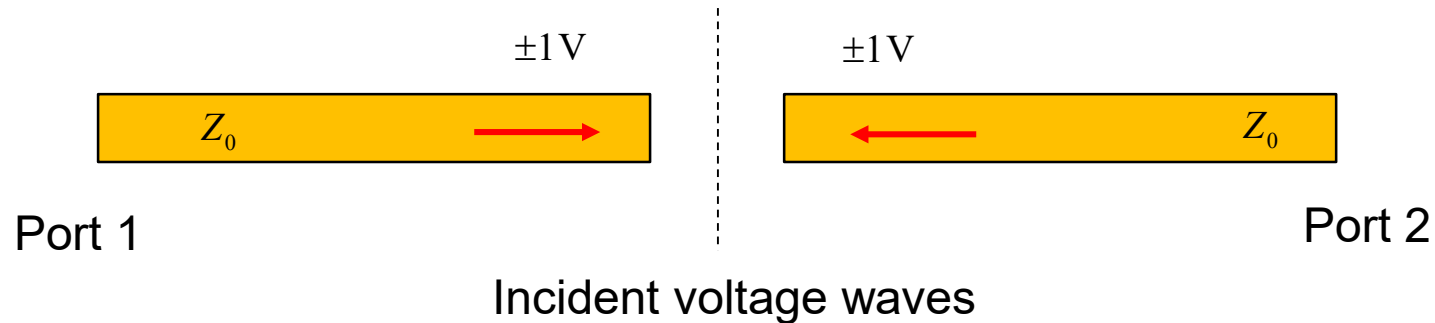


$$Z_1 = Z_L^{\text{SC}}, \quad Z_2 = \frac{1}{2}(Z_L^{\text{OC}} - Z_L^{\text{SC}})$$



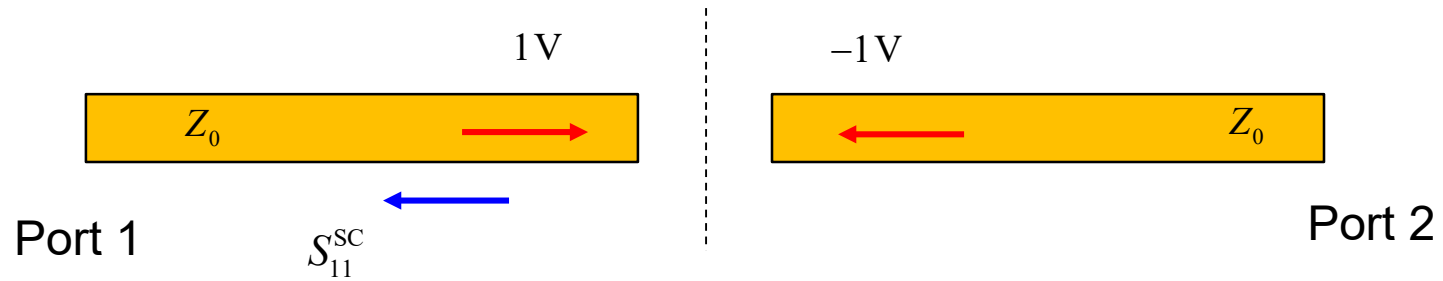
# Z-Parameter Extraction (cont.)

The short or open can be realized by using odd-mode or even-mode excitation.



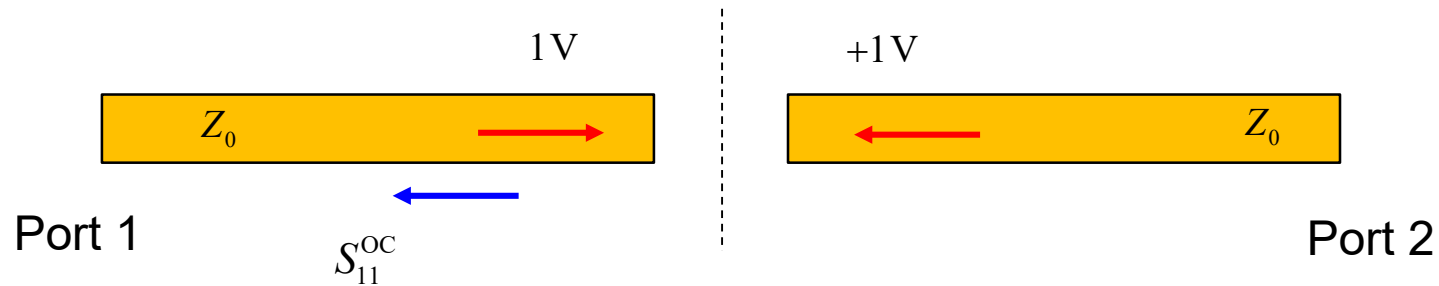
Even/odd-mode analysis is very useful in analyzing devices (e.g., using HFSS).

# Z-Parameter Extraction (cont.)



Odd mode voltage waves

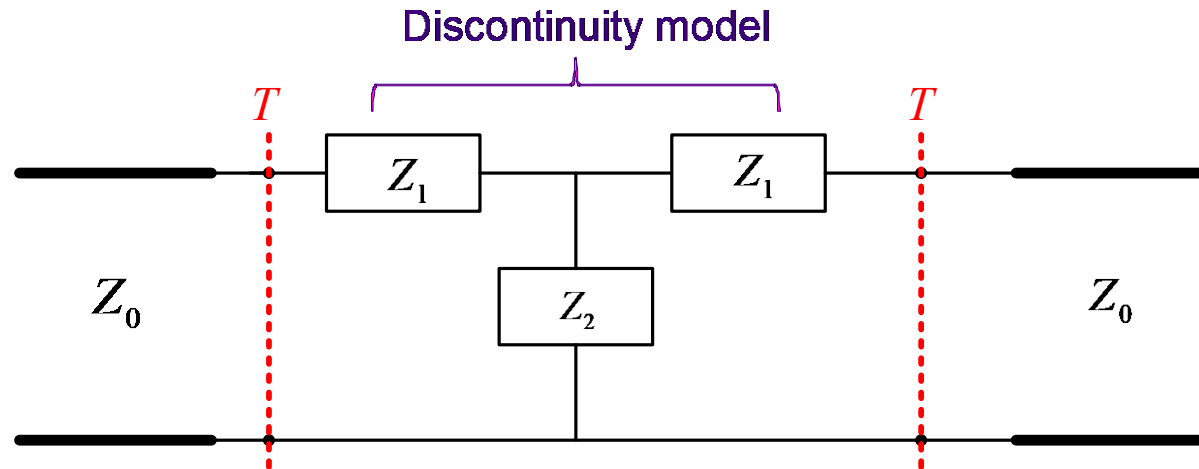
$$Z_L^{SC} = Z_0 \left( \frac{1 + S_{11}^{SC}}{1 - S_{11}^{SC}} \right)$$



Even mode voltage waves

$$Z_L^{OC} = Z_0 \left( \frac{1 + S_{11}^{OC}}{1 - S_{11}^{OC}} \right)$$

# Z-Parameter Extraction (cont.)



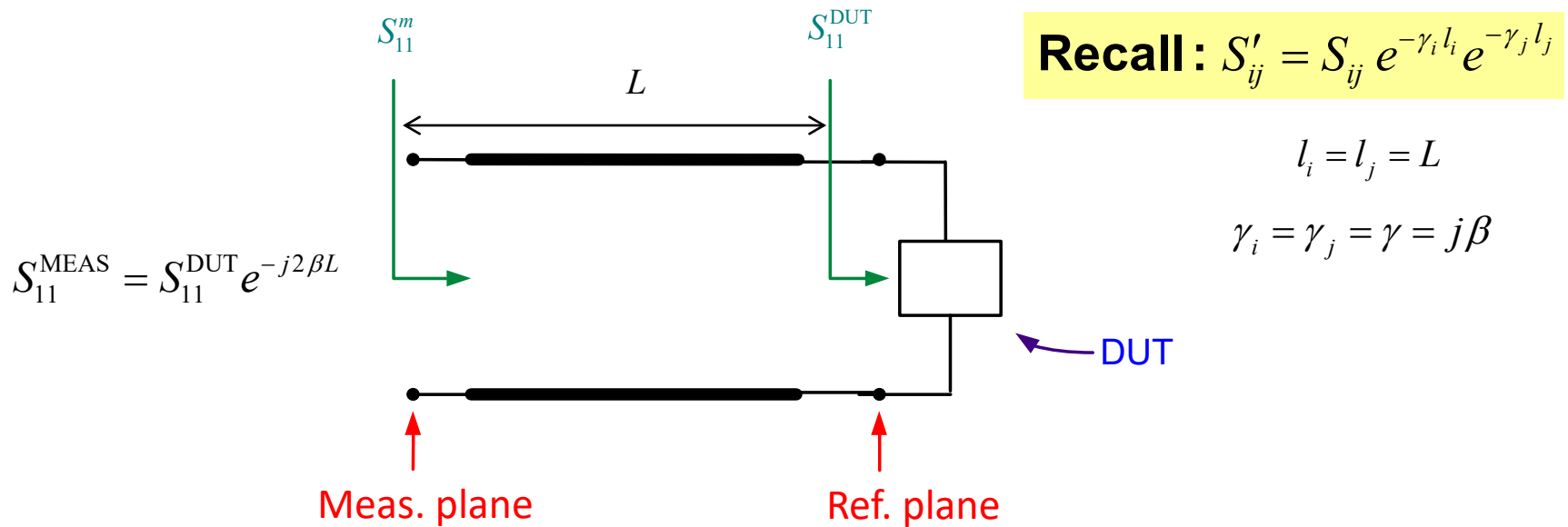
Hence we have:

$$Z_1 = Z_0 \left( \frac{1 + S_{11}^{\text{SC}}}{1 - S_{11}^{\text{SC}}} \right)$$

$$Z_2 = \frac{1}{2} \left( Z_0 \left( \frac{1 + S_{11}^{\text{OC}}}{1 - S_{11}^{\text{OC}}} \right) - Z_0 \left( \frac{1 + S_{11}^{\text{SC}}}{1 - S_{11}^{\text{SC}}} \right) \right)$$

# De-embedding of a Line Length

We wish to know the reflection coefficient of a 1-port device under test (DUT), but the DUT is not assessable directly – it has an extra length of transmission line connected to it (whose length may not be known).



Replace DUT with short circuit ( $S_{11}^{\text{DUT}} \rightarrow -1$ )  $\Rightarrow S_{11}^{\text{MEAS, SC}} = -e^{-j2\beta L} = -1 / e^{+j2\beta L}$

$$S_{11}^{\text{DUT}} = S_{11}^{\text{MEAS, DUT}} e^{+j2\beta L} \quad \Rightarrow \quad S_{11}^{\text{DUT}} = S_{11}^{\text{MEAS, DUT}} \left( \frac{-1}{S_{11}^{\text{MEAS, SC}}} \right)$$