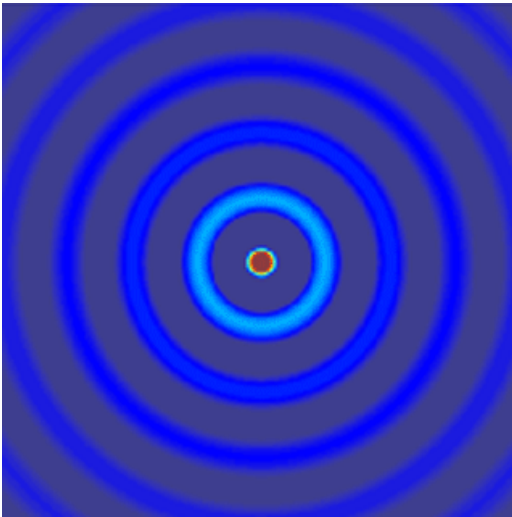


ECE 6341

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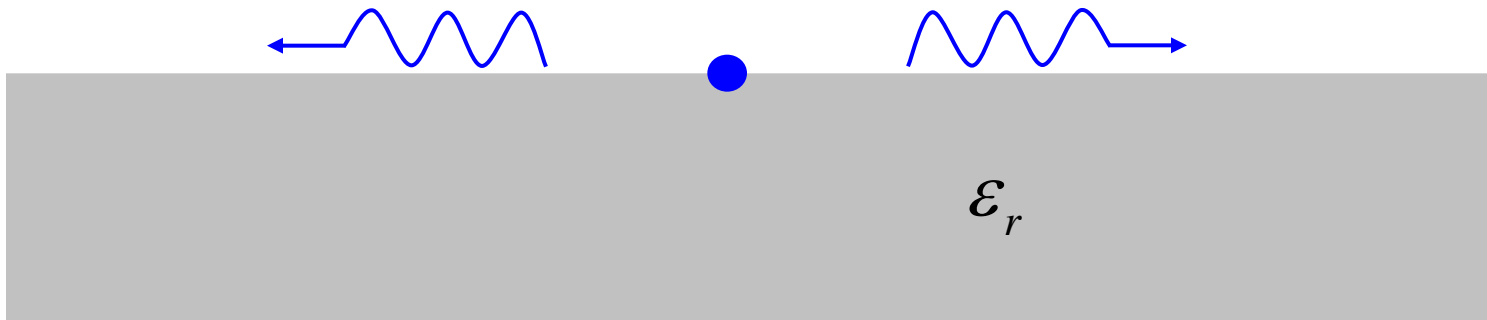
Notes 35

Higher-order Steepest-Descent Method

$$I(\Omega) = \int_c f(z) e^{\Omega g(z)} dz$$

Assume $f(z_0) = 0$

This important special case arises when asymptotically evaluating the field along an interface (discussed later in the notes).



Higher-order SDM (cont.)

$$I(\Omega) = \int_C f(z) e^{\Omega g(z)} dz$$

$$I(\Omega) = e^{\Omega g(z_0)} \int_{SDP} f(z) e^{-\Omega[g(z_0) - g(z)]} dz$$

Along SDP: $s^2 \equiv g(z_0) - g(z)$ (real)

Note: The variable s is taken as positive after we leave the saddle point, and negative before we enter the saddle point.

Hence
$$I(\Omega) = e^{\Omega g(z_0)} \int_{-\infty}^{+\infty} f(z(s)) \left(\frac{dz}{ds} \right) e^{-\Omega s^2} ds$$

Higher-order SDM (cont.)

$$I(\Omega) = e^{\Omega g(z_0)} \int_{-\infty}^{+\infty} f(z(s)) \left(\frac{dz}{ds} \right) e^{-\Omega s^2} ds$$

Define $h(s) \equiv f(z(s)) \frac{dz}{ds}$

Then $I(\Omega) = e^{\Omega g(z_0)} \int_{-\infty}^{+\infty} h(s) e^{-\Omega s^2} ds$

Assume $h(s) \sim \cancel{h(0)} + h'(0)s + \frac{1}{2}h''(0)s^2$

$f(z_0) = 0$

Higher-order SDM (cont.)

Note: $\int_{-\infty}^{+\infty} s e^{-\Omega s^2} ds = 0$ (s is odd)

Hence $I(\Omega) \sim \frac{1}{2} h''(0) e^{\Omega g(z_0)} I_s$

where $I_s \equiv \int_{-\infty}^{+\infty} s^2 e^{-\Omega s^2} ds = 2 \int_0^{\infty} s^2 e^{-\Omega s^2} ds$

Use $t = \Omega s^2$
 $dt = 2\Omega s ds$

Higher-order SDM (cont.)

$$I_s = 2 \int_0^{\infty} s^2 e^{-\Omega s^2} ds$$

$$t = \Omega s^2$$

$$dt = 2\Omega s ds$$

$$I_s = 2 \int_0^{\infty} \left(\frac{t}{\Omega} \right) e^{-t} \left(\frac{1}{2\Omega \sqrt{\frac{t}{\Omega}}} \right) dt$$

$$= \frac{1}{\Omega^{3/2}} \int_0^{\infty} t^{1/2} e^{-t} dt$$

$$= \frac{1}{\Omega^{3/2}} \Gamma\left(\frac{3}{2}\right) = \frac{1}{\Omega^{3/2}} \frac{1}{2} \Gamma\left(\frac{1}{2}\right)$$

$$= \frac{1}{\Omega^{3/2}} \left(\frac{\sqrt{\pi}}{2} \right)$$

Recall:

$$\Gamma(x) = \int_0^{\infty} t^{x-1} e^{-t} dt$$

$$\begin{aligned} \Gamma(x) &= (x-1)! = (x-1)(x-2)! \\ &= (x-1)\Gamma(x-1) \end{aligned}$$

$$\Gamma(1/2) = \sqrt{\pi}$$

Higher-order SDM (cont.)

Hence

$$I(\Omega) \sim \frac{1}{4} h''(0) e^{\Omega g(z_0)} \sqrt{\pi} \left(\frac{1}{\Omega^{3/2}} \right)$$

Note: The leading term of the expansion now behaves as $1 / \Omega^{3/2}$.

We now we need to calculate $h''(0)$

Higher-order SDM (cont.)

$$h(s) = f(z(s))z'(s)$$

$$h'(s) = f'(z(s))(z'(s))^2 + f(z(s))z''(s)$$

$$h''(s) = f''(z(s))(z'(s))^3 + f'(z(s))(2)(z'(s))z''(s) \\ + f'(z(s))z'(s)z''(s) + f(z(s))z'''(s)$$

$$h''(0) = f''(z_0)(z'(0))^3 + 3f'(z_0)(z'(0))z''(0) + \cancel{f(z_0)z'''(0)}$$

Higher-order SDM (cont.)

Hence

$$h''(0) = f''(z_0)(z'(0))^3 + 3f'(z_0)z'(0)z''(0)$$

We next take two derivatives with respect to s
in order to calculate $z'(0)$, $z''(0)$

$$s^2 \equiv g(z_0) - g(z)$$

$$(1st) \quad 2s = -g'(z)z'(s)$$

$$(2nd) \quad 2 = -g''(z)(z'(s))^2 - g'(z)z''(s)$$

Higher-order SDM (cont.)

From (2nd): $2 = -g''(z_0)(z'(0))^2 - g'(z_0)z''(0)$

We then have

$$z'(0) = \left(\frac{-2}{g''(z_0)} \right)^{1/2}$$

or

$$z'(0) = \sqrt{\frac{2}{|g''(z_0)|}} e^{j\theta_{SDP}}$$

$$\theta_{SDP} = -\frac{\alpha}{2} \pm \frac{\pi}{2}$$

$$\alpha = \arg(g''(z_0))$$

Higher-order SDM (cont.)

$$(2\text{nd}) \quad 2 = -g''(z)(z'(s))^2 - g'(z)z''(s)$$

Take one more derivative to calculate z''' :

$$\begin{aligned} 0 &= -g'''(z)(z'(s))^3 - 2g''(z)(z'(s))z''(s) - g''(z)z'(s)z''(s) - g'(z)z'''(s) \\ &= -g'''(z)(z'(s))^3 - 3g''(z)(z'(s))z''(s) - g'(z)z'''(s) \quad (3\text{rd}) \end{aligned}$$

$$0 = -g'''(z_0)(z'(0))^3 - 3g''(z_0)(z'(0))z''(0) - \cancel{g'(z_0)z'''(0)}$$

or

$$0 = -g'''(z_0)(z'(0))^2 - 3g''(z_0)z''(0)$$

Higher-order SDM (cont.)

Hence,

$$z''(0) = -\frac{1}{3} \frac{g'''(z_0)(z'(0))^2}{g''(z_0)}$$

where

$$z'(0) = \left(\frac{-2}{g''(z_0)} \right)^{1/2}$$

Therefore,

$$z''(0) = \frac{2}{3} \frac{g'''(z_0)}{(g''(z_0))^2}$$

Higher-order SDM (cont.)

We then have

$$h''(0) = f''(z_0) \left(\frac{2}{|g''(z_0)|} \right)^{3/2} e^{j3\theta_{SDP}} \\ + 3f'(z_0) \sqrt{\frac{2}{|g''(z_0)|}} e^{j\theta_{SDP}} \left(\frac{2}{3} \frac{g'''(z_0)}{(g''(z_0))^2} \right)$$

Higher-order SDM (cont.)

Summary

$$I(\Omega) = \int_C f(z) e^{\Omega g(z)} dz \quad f(z_0) = 0$$

$$I(\Omega) \sim \frac{1}{4} h''(0) e^{\Omega g(z_0)} \sqrt{\pi} \left(\frac{1}{\Omega^{3/2}} \right)$$

$$h''(0) = f''(z_0) \left(\frac{2}{|g''(z_0)|} \right)^{3/2} e^{j3\theta_{SDP}}$$

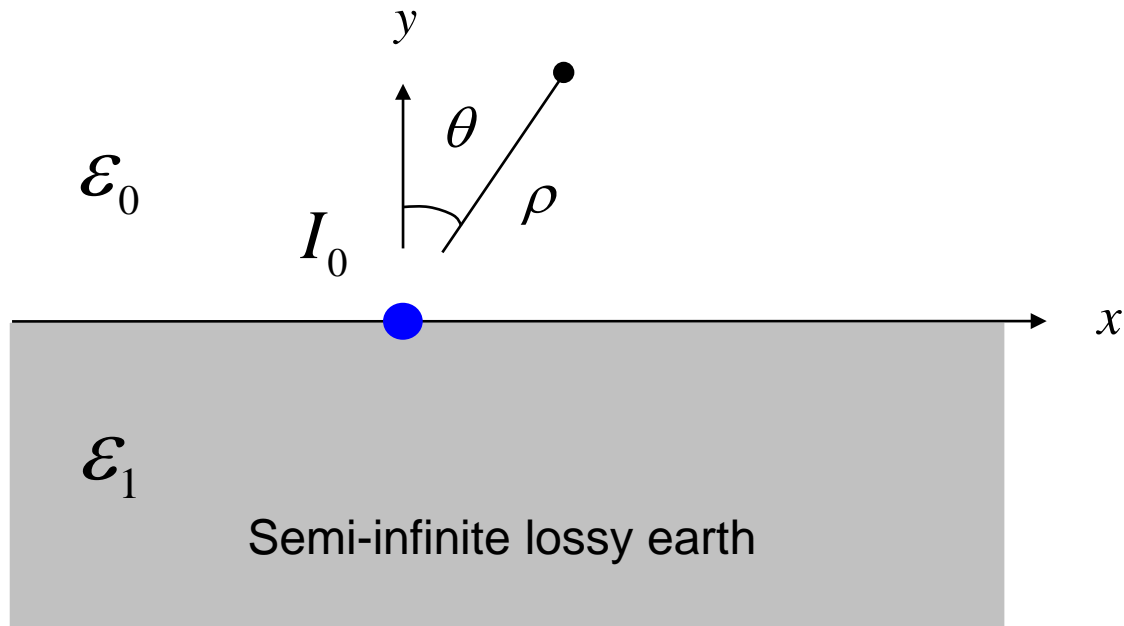
$$+ 3f'(z_0) \sqrt{\frac{2}{|g''(z_0)|}} e^{j\theta_{SDP}} \left(\frac{2}{3} \frac{g'''(z_0)}{(g''(z_0))^2} \right)$$

$$\theta_{SDP} = -\frac{\alpha}{2} \pm \frac{\pi}{2}$$

$$\alpha = \arg(g''(z_0))$$

Example

A line source is located on the interface.



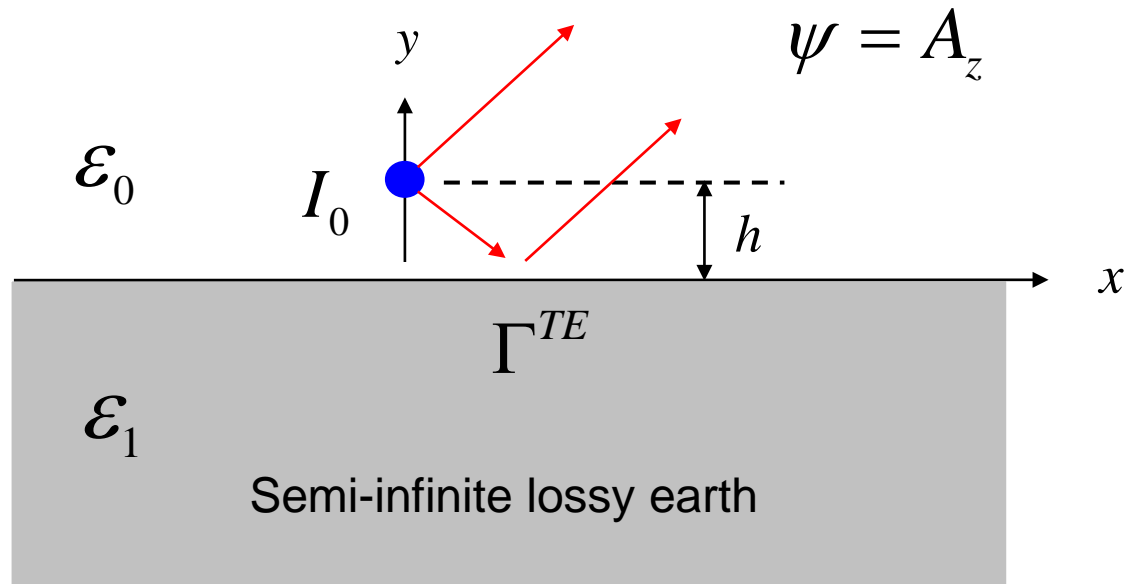
Example

Consider first the line source at a height h above the interface.

The field is TM_z and also TE_y .

$$\underline{E} = \hat{z}E_z$$

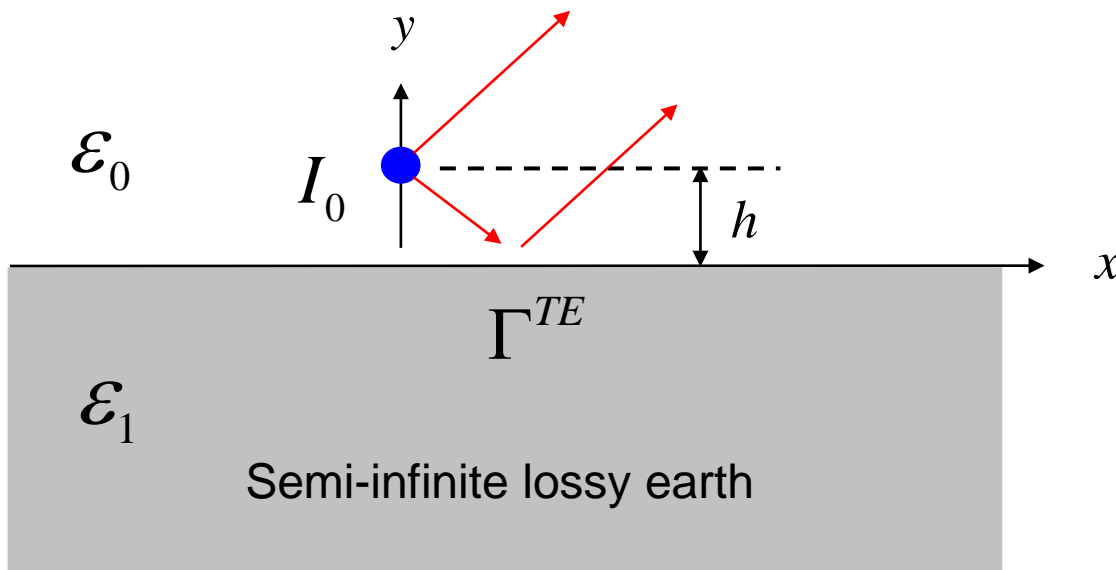
$$\underline{E} = -j\omega\underline{A} - \nabla\Phi$$



Example

$$\psi = \frac{\mu_0 I_0}{4\pi j} \int_{-\infty}^{+\infty} \left[\frac{1}{k_{y0}} e^{-jk_{y0}|y-h|} + \frac{1}{k_{y0}} e^{-jk_{y0}h} \Gamma^{TE} e^{-jk_{y0}y} \right] e^{-jk_x x} dk_x$$

$$\Gamma^{TE} = \frac{Z_1^{TE} - Z_0^{TE}}{Z_1^{TE} + Z_0^{TE}}$$



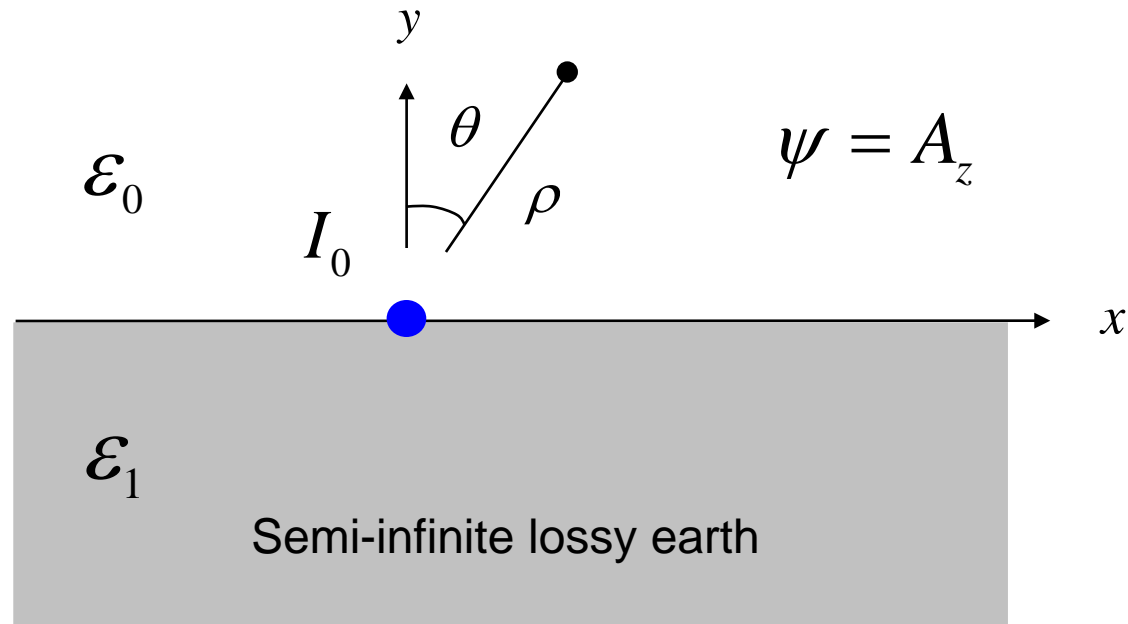
TE_y:

$$Z_0^{TE} = \frac{\omega\mu_0}{k_{y0}}$$

$$Z_1^{TE} = \frac{\omega\mu_0}{k_{y1}}$$

Example

The line source is now at the interface ($h = 0$).



$$\psi = \frac{\mu_0 I_0}{4\pi j} \int_{-\infty}^{+\infty} \frac{1}{k_{y0}} \left[1 + \left(\frac{Z_1^{TE} - Z_0^{TE}}{Z_1^{TE} + Z_0^{TE}} \right) \right] e^{-jk_{y0}y} e^{-jk_x x} dk_x$$

$$k_{y0} = (k_0^2 - k_x^2)^{1/2}$$

Example (cont.)

Simplifying,

$$1 + \frac{Z_1^{TE} - Z_0^{TE}}{Z_1^{TE} + Z_0^{TE}} = \frac{2Z_1^{TE}}{Z_0^{TE} + Z_1^{TE}}$$

$$Z_0^{TE} = \frac{\omega\mu_0}{k_{y0}} \quad k_{y0} = (k_0^2 - k_x^2)^{1/2}$$

$$Z_1^{TE} = \frac{\omega\mu_0}{k_{y1}} \quad k_{y1} = (k_1^2 - k_x^2)^{1/2}$$

Example (cont.)

Hence, we have

$$\frac{2Z_1^{TE}}{Z_0^{TE} + Z_1^{TE}} = \frac{2\left(\frac{1}{k_{y1}}\right)}{\frac{1}{k_{y0}} + \frac{1}{k_{y1}}} = \frac{2k_{y0}}{k_{y0} + k_{y1}}$$

Therefore,

$$\psi = \frac{\mu_0 I_0}{2\pi j} \int_{-\infty}^{+\infty} \left(\frac{1}{k_{y0} + k_{y1}} \right) e^{-jk_{y0}y} e^{-jk_x x} dk_x$$

Now use:

$$\begin{aligned} k_x &= k_0 \sin \zeta & x &= \rho \sin \theta \\ dk_x &= k_0 \cos \zeta d\zeta & y &= \rho \cos \theta \\ k_{y0} &= k_0 \cos \zeta \end{aligned}$$

Example (cont.)

$$\psi = \frac{\mu_0 I_0}{2\pi j} \int_C \left(\frac{k_0 \cos \zeta}{k_0 \cos \zeta + (k_1^2 - k_0^2 \sin^2 \zeta)^{1/2}} \right) e^{-j(k_0 \rho) \cos(\zeta - \theta)} d\zeta$$

or

$$\psi = \frac{\mu_0 I_0}{2\pi j} \int_C \left(\frac{\cos \zeta}{\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2}} \right) e^{-j(k_0 \rho) \cos(\zeta - \theta)} d\zeta$$

$$n_1 \equiv k_1 / k_0 = \sqrt{\epsilon_r \mu_r}$$

Note:

For a lossless earth

$$k_{y1} = (k_1^2 - k_0^2 \sin^2 \zeta)^{1/2} = \begin{cases} k_0 \sqrt{k_1^2 - k_0^2 \sin^2 \zeta}, & k_0 \sin \zeta < k_1 \\ -jk_0 \sqrt{k_0^2 \sin^2 \zeta - k_1^2}, & k_0 \sin \zeta > k_1 \end{cases}$$

Example (cont.)

We then identify (ignoring the constant in front of the integral):

$$\Omega = k\rho$$

$$g(\zeta) = -j \cos(\zeta - \theta)$$

$$f(\zeta) = \frac{\cos \zeta}{\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2}}$$

Saddle point: $\zeta_0 = \theta$

Notes:

There are branch points in the complex ζ plane arising from k_{y1} , but we are ignoring these for a lossy earth (n_1 is complex).

There are no branch points in the ζ plane arising from k_{y0} , since the steepest-descent transformation has removed them.

$$k_{y0} = (k^2 - k_x^2)^{1/2} = k_0 \cos \zeta$$

Example (cont.)

$$f(\zeta) = \frac{\cos \zeta}{\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2}}$$

Fields on the interface:

$$\text{As } \theta \rightarrow 90^\circ, \zeta_0 \rightarrow 90^\circ$$

Hence $f(\zeta_0) = 0$ (unless $n_1 = 1$)

We need the higher-order steepest-descent method when we evaluate the fields along the interface.

Example (cont.)

Far-field (antenna) radiation pattern: $0 \leq \theta < \pi / 2$

$$\Omega = k\rho$$

$$\zeta_0 = \theta$$

$$f(\zeta_0) = \frac{\cos \theta}{\cos \theta + (n_1^2 - \sin^2 \theta)^{1/2}}$$

$$g(\zeta_0) = -j$$

$$g''(\zeta_0) = j$$

$$f(\zeta_0) = f(\theta) \neq 0$$

The usual steepest-descent method applies:

$$I(\Omega) \sim f(\zeta_0) e^{\Omega g(\zeta_0)} \sqrt{\frac{\pi}{\Omega}} \sqrt{\frac{2}{|g''(\zeta_0)|}} e^{j\theta_{SDP}}$$

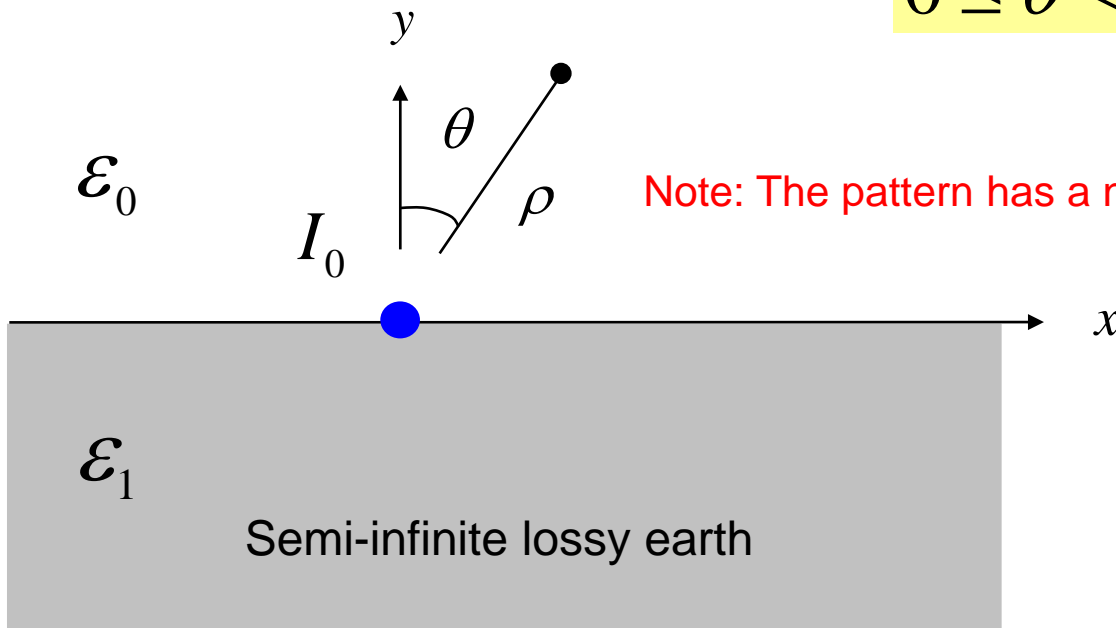
$$\psi \sim \frac{\mu_0 I_0}{2\pi j} \left(\frac{\cos \theta}{\cos \theta + (n_1^2 - \sin^2 \theta)^{1/2}} \right) e^{-j(k_0 \rho)} \sqrt{\frac{\pi}{k_0 \rho}} \sqrt{\frac{2}{|j|}} e^{j\pi/4}$$

Example (cont.)

Final far-field radiation pattern:

$$E_z \sim -j\omega \left(\frac{\mu_0 I_0}{2\pi j} \right) \left(\frac{\cos \theta}{\cos \theta + (n_1^2 - \sin^2 \theta)^{1/2}} \right) e^{-j(k_0 \rho)} \sqrt{\frac{2\pi}{k_0 \rho}} e^{j\pi/4}$$

$$0 \leq \theta < \pi / 2$$



Note: The pattern has a null as we approach the horizon.

Example (cont.)

Interface field: $\theta = \pi / 2$

$$\psi = \frac{\mu_0 I_0}{2\pi j} \int_C \left(\frac{\cos \zeta}{\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2}} \right) e^{-j(k_0 \rho) \cos(\zeta - \theta)} d\zeta$$

Recall

$$\psi = \frac{\mu_0 I_0}{2\pi j} I(\Omega)$$

$$f(\zeta_0) = f(\theta) = f\left(\frac{\pi}{2}\right) = 0$$

From the higher-order steepest-descent method, we have:

$$I(\Omega) \sim \frac{1}{4} h''(0) e^{\Omega g(z_0)} \sqrt{\pi} \left(\frac{1}{\Omega^{3/2}} \right)$$

Example (cont.)

Recall: $\underline{E} = -j\omega\underline{A} - \nabla\Phi$

so $E_z = -j\omega A_z = -j\omega\psi$

We then have

$$E_z \sim -j\omega \left(\frac{\mu_0 I_0}{2\pi j} \right) \left(\frac{1}{4} h''(0) \right) e^{-j(k_0\rho)} \sqrt{\pi} \frac{1}{(k_0\rho)^{3/2}}$$

Example (cont.)

We have

$$h''(0) = f''(\zeta_0) \left(\frac{2}{|g''(\zeta_0)|} \right)^{3/2} e^{j3\theta_{SDP}} \\ + 3f'(\zeta_0) \sqrt{\frac{2}{|g''(\zeta_0)|}} e^{j\theta_{SDP}} \left(\frac{2}{3} \frac{g'''(\zeta_0)}{(g''(\zeta_0))^2} \right)$$

with

$$\zeta_0 = \theta = \pi / 2 \quad \theta_{SDP} = \frac{\pi}{4}$$

$$f(\zeta) = \frac{\cos \zeta}{\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2}}$$

$$g(\zeta) = -j \cos(\zeta - \theta)$$

Example (cont.)

We have

$$g(\zeta) = -j \cos(\zeta - \theta)$$

$$\zeta_0 = \theta = \pi / 2$$

so

$$g(\zeta_0) = -j$$

$$g'(\zeta_0) = 0$$

$$g''(\zeta_0) = j$$

$$g'''(\zeta_0) = 0$$

Example (cont.)

We therefore have

$$h''(0) = f''(\zeta_0) 2^{3/2} e^{j3\pi/4}$$

with

$$f(\zeta) = \frac{\cos \zeta}{\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2}}$$

Example (cont.)

We next calculate the derivatives of the f function:

$$f(\zeta) = \frac{\cos \zeta}{\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2}}$$

$$f'(\zeta) = \frac{-\sin \zeta \left(\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2} \right) + \sin \zeta \cos \zeta \left(1 + (n_1^2 - \sin^2 \zeta)^{-1/2} \cos \zeta \right)}{\left(\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2} \right)^2}$$

$$f''(\zeta) = \frac{D(\zeta)N'(\zeta) - N(\zeta)D'(\zeta)}{D^2(\zeta)}$$

$$N(\zeta) = -\sin \zeta \left(\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2} \right) + \sin \zeta \cos \zeta \left(1 + (n_1^2 - \sin^2 \zeta)^{-1/2} \cos \zeta \right)$$

$$D(\zeta) = \left(\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2} \right)^2$$

Example (cont.)

We then have

$$f''(\zeta) = \frac{D(\zeta)N'(\zeta) - N(\zeta)D'(\zeta)}{D^2(\zeta)}$$

where

$$\begin{aligned} N'(\zeta) = & -\cos \zeta \left(\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2} \right) \\ & - \sin \zeta (-\sin \zeta) \left(1 + (n_1^2 - \sin^2 \zeta)^{-1/2} \cos \zeta \right) \\ & + (\cos \zeta - \sin^2 \zeta) \left(1 + (n_1^2 - \sin^2 \zeta)^{-1/2} \cos \zeta \right) \\ & + (\sin \zeta \cos \zeta) \left[-(n_1^2 - \sin^2 \zeta)^{-1/2} \sin \zeta + \cos \zeta (n_1^2 - \sin^2 \zeta)^{-3/2} \sin \zeta \cos \zeta \right] \end{aligned}$$

$$D'(\zeta) = 2 \left(\cos \zeta + (n_1^2 - \sin^2 \zeta)^{1/2} \right) \left(-\sin \zeta - (n_1^2 - \sin^2 \zeta)^{-1/2} \sin \zeta \cos \zeta \right)$$

Example (cont.)

At the saddle point we have

$$f'(\zeta_0) = -\frac{1}{\sqrt{n_1^2 - 1}}$$

$$N(\zeta_0) = -\sqrt{n_1^2 - 1}$$

$$N'(\zeta_0) = 0$$

$$D(\zeta_0) = n_1^2 - 1$$

$$D'(\zeta_0) = -2\sqrt{n_1^2 - 1}$$

$$f''(\zeta_0) = \frac{-2}{n_1^2 - 1}$$

Example (cont.)

We then have

$$h''(0) = \left(\frac{-2}{n_1^2 - 1} \right) 2^{3/2} e^{j3\pi/4}$$

The field along the interface is then

$$E_z \sim -j\omega \left(\frac{\mu_0 I_0}{2\pi j} \right) \left(\frac{1}{4} \left(\frac{-2}{n_1^2 - 1} \right) 2^{3/2} e^{j3\pi/4} \right) e^{-j(k_0 \rho)} \sqrt{\pi} \frac{1}{(k_0 \rho)^{3/2}}$$

Note: Far away from the source, the wave along the interface of the lossy earth travels with a wavenumber of free space.

Example (cont.)

Summary

The field in space ($\theta < \pi/2$) is

$$E_z \sim -j\omega \left(\frac{\mu_0 I_0}{2\pi j} \right) \left(\frac{\cos \theta}{\cos \theta + (n_1^2 - \sin^2 \theta)^{1/2}} \right) e^{-j(k_0 \rho)} \sqrt{\frac{2\pi}{k_0 \rho}} e^{j\pi/4}$$

The field along the interface ($\theta = \pi/2$) is

$$E_z \sim -j\omega \left(\frac{\mu_0 I_0}{2\pi j} \right) \left(\frac{1}{4} \left(\frac{-2}{n_1^2 - 1} \right) 2^{3/2} e^{j3\pi/4} \right) e^{-j(k_0 \rho)} \sqrt{\pi} \frac{1}{(k_0 \rho)^{3/2}}$$

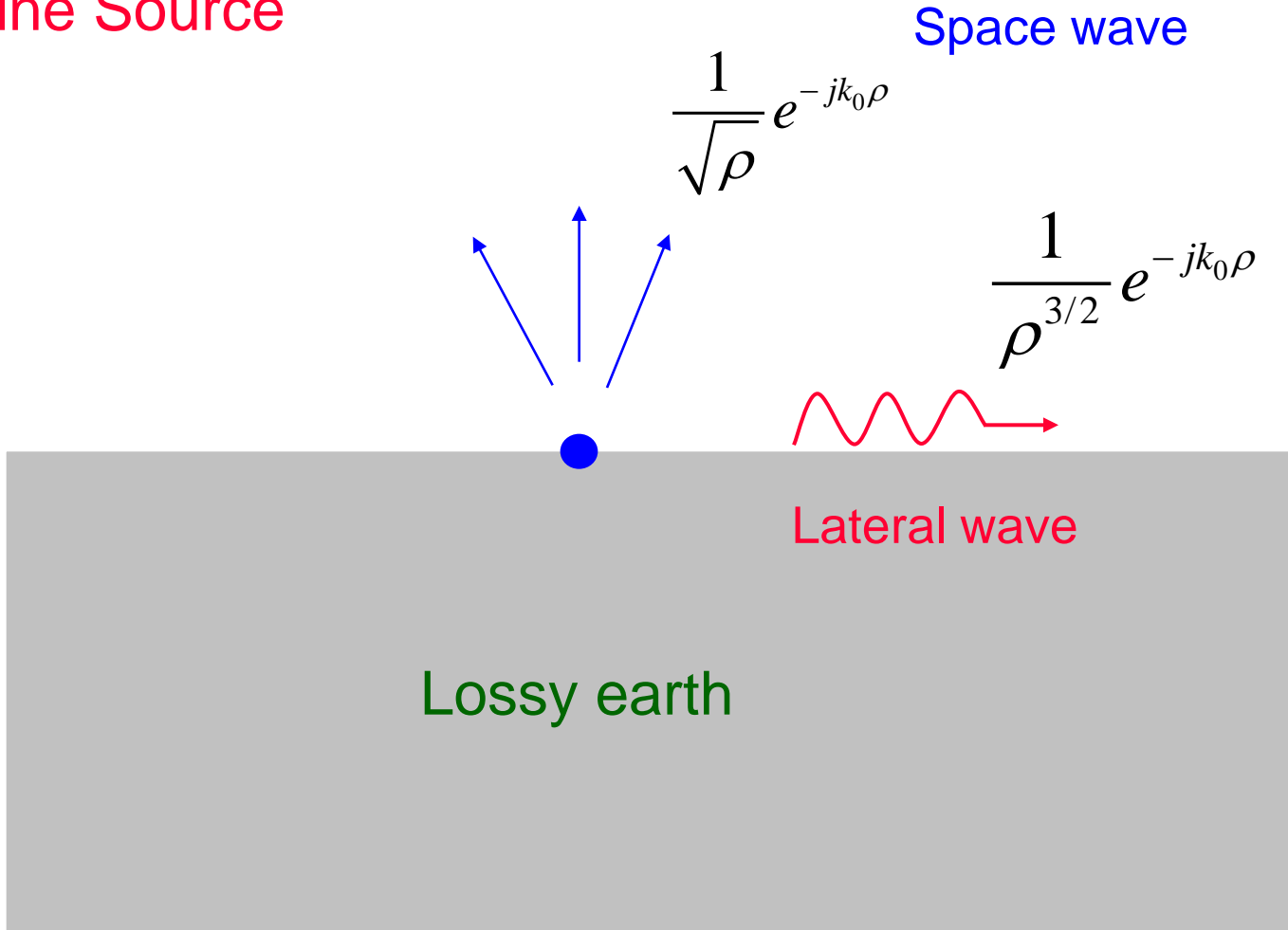
Example (cont.)

Line Source

Space wave

$$\frac{1}{\sqrt{\rho}} e^{-jk_0\rho}$$

$$\frac{1}{\rho^{3/2}} e^{-jk_0\rho}$$



Lossy earth

Lateral wave

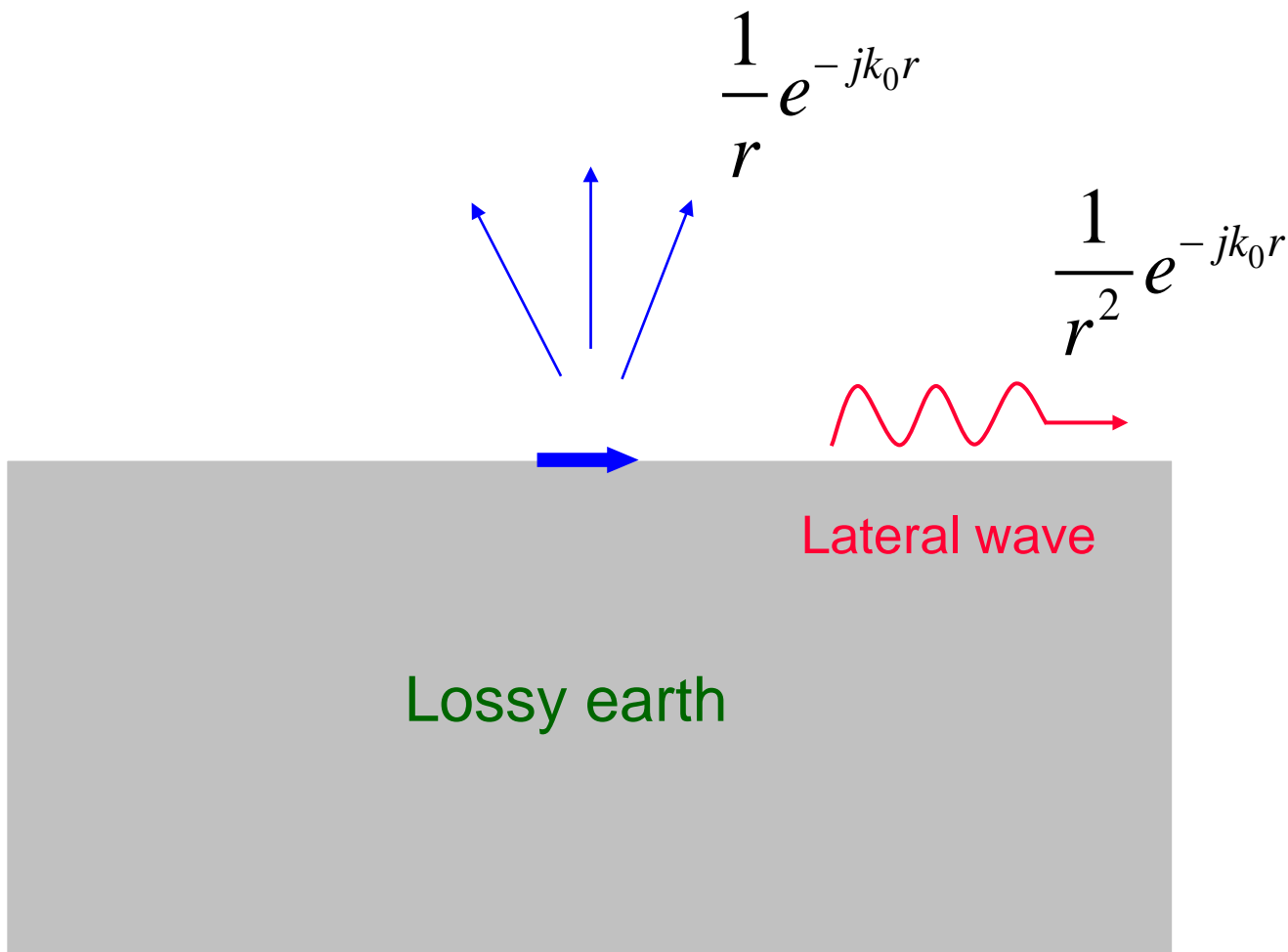
Extension to Dipole

Dipole Source

Space wave

$$\frac{1}{r} e^{-jk_0 r}$$

$$\frac{1}{r^2} e^{-jk_0 r}$$



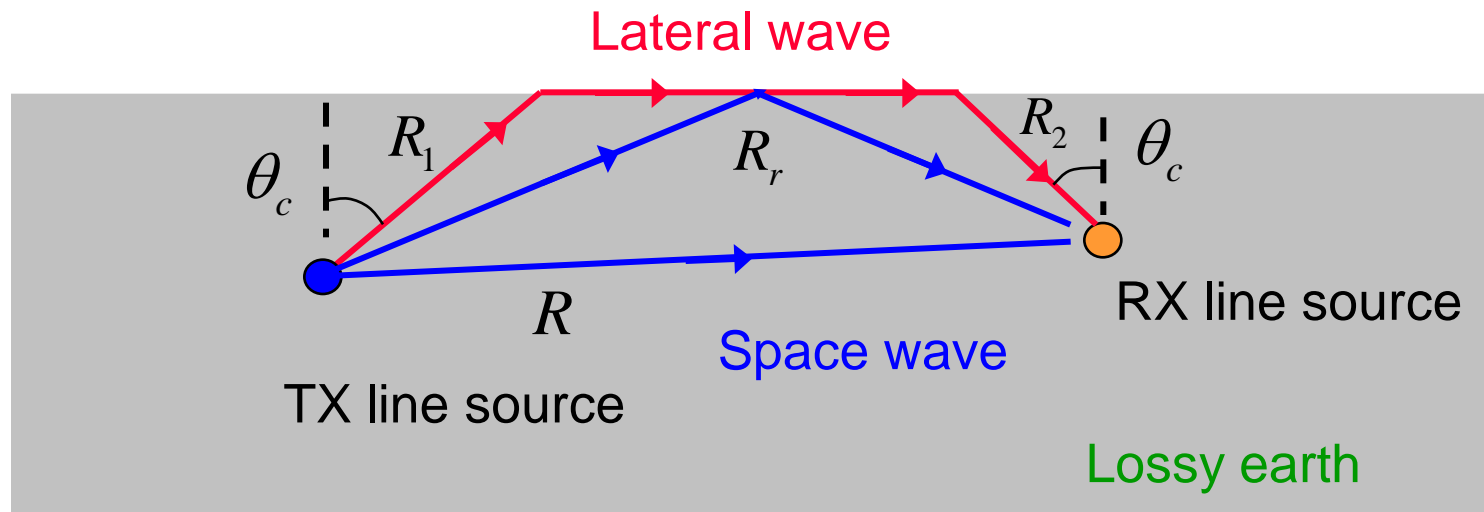
Important Geophysical Problem

The field is asymptotically evaluated for $R \rightarrow \infty$

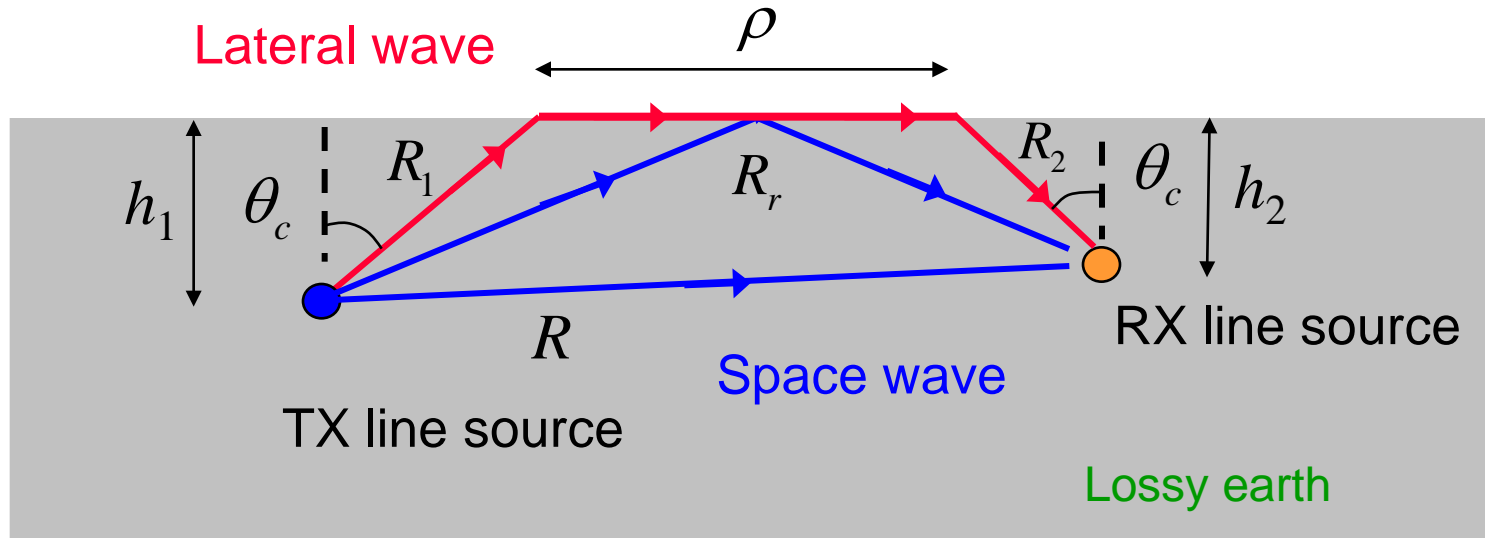
Two types of wave fields are important for large distances:

- Space wave
- Lateral wave

Note: More will be said about these waves in the next chapter on “Radiation Physics of Layered Media.”



Important Geophysical Problem (cont.)



Space wave:
$$\frac{1}{\sqrt{R}} e^{-jk_1 R} + \Gamma_{TE} \frac{1}{\sqrt{R_r}} e^{-jk_1 R_r}$$

Lateral wave:
$$\frac{1}{\rho^{3/2}} e^{-jk_0 \rho} \left[\frac{e^{-jk_1 R_1}}{\sqrt{R_1}} \frac{e^{-jk_1 R_2}}{\sqrt{R_2}} \right]$$

This will be the dominant field for a lossy earth (k_1 is complex).

Note: Amplitude terms have been suppressed here.