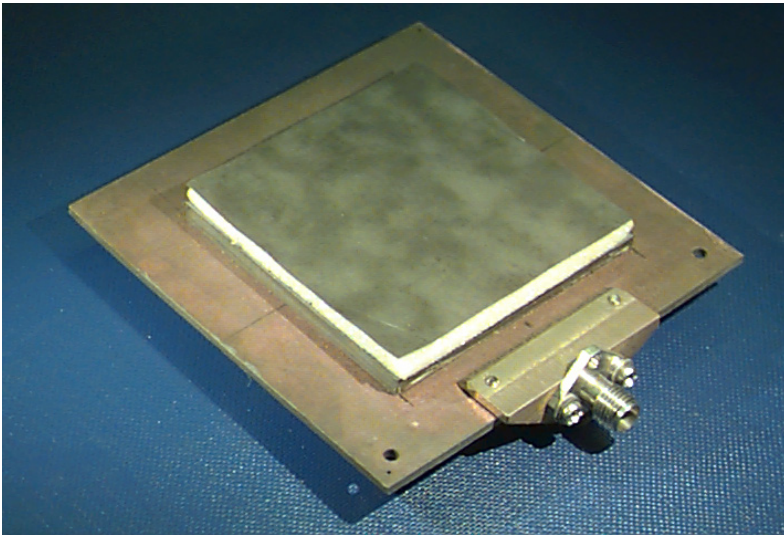


ECE 6345

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ECE Dept.



Notes 32

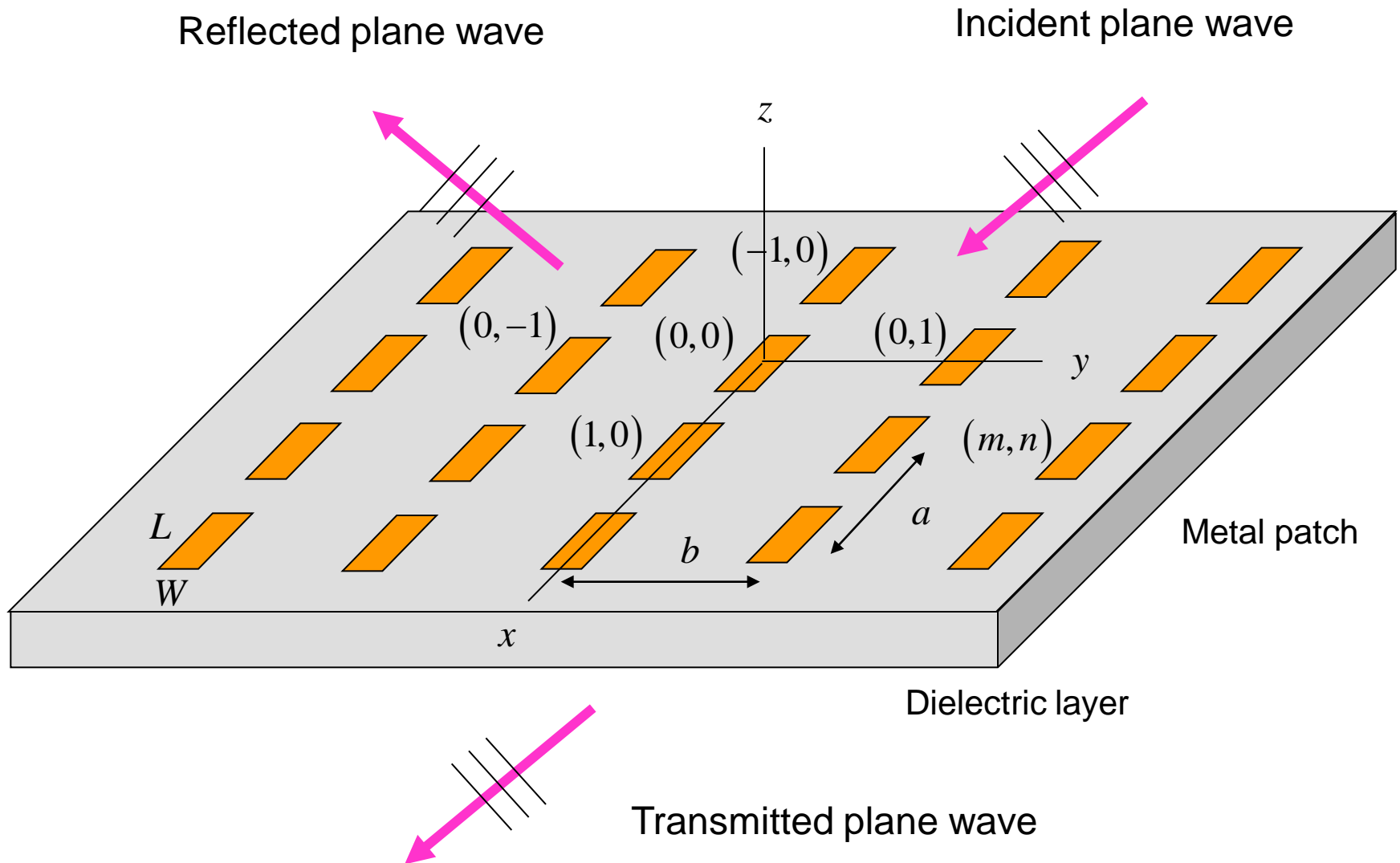
Overview

In this set of notes we extend the spectral-domain method to analyze **infinite periodic structures**.

Two typical examples of infinite periodic problems:

- Scattering from a frequency selective surface (FSS)
- Input impedance of a microstrip phased array

FSS Geometry



FSS Geometry (cont.)

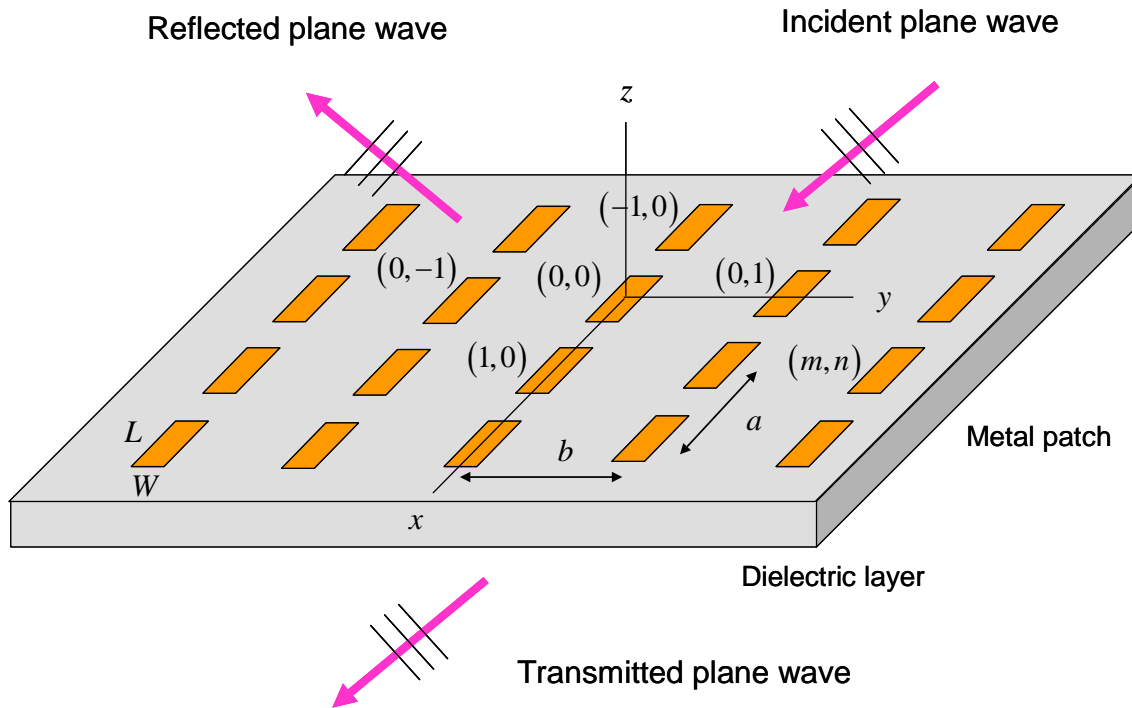
$$\psi^{inc} = A e^{-j(k_{x0}x + k_{y0}y)} e^{+jk_{z0}z}$$

$(\theta_0, \phi_0) =$ arrival angles

$$k_{x0} = -k_0 \sin \theta_0 \cos \phi_0$$

$$k_{y0} = -k_0 \sin \theta_0 \sin \phi_0$$

$$k_{z0} = k_0 \cos \theta_0$$

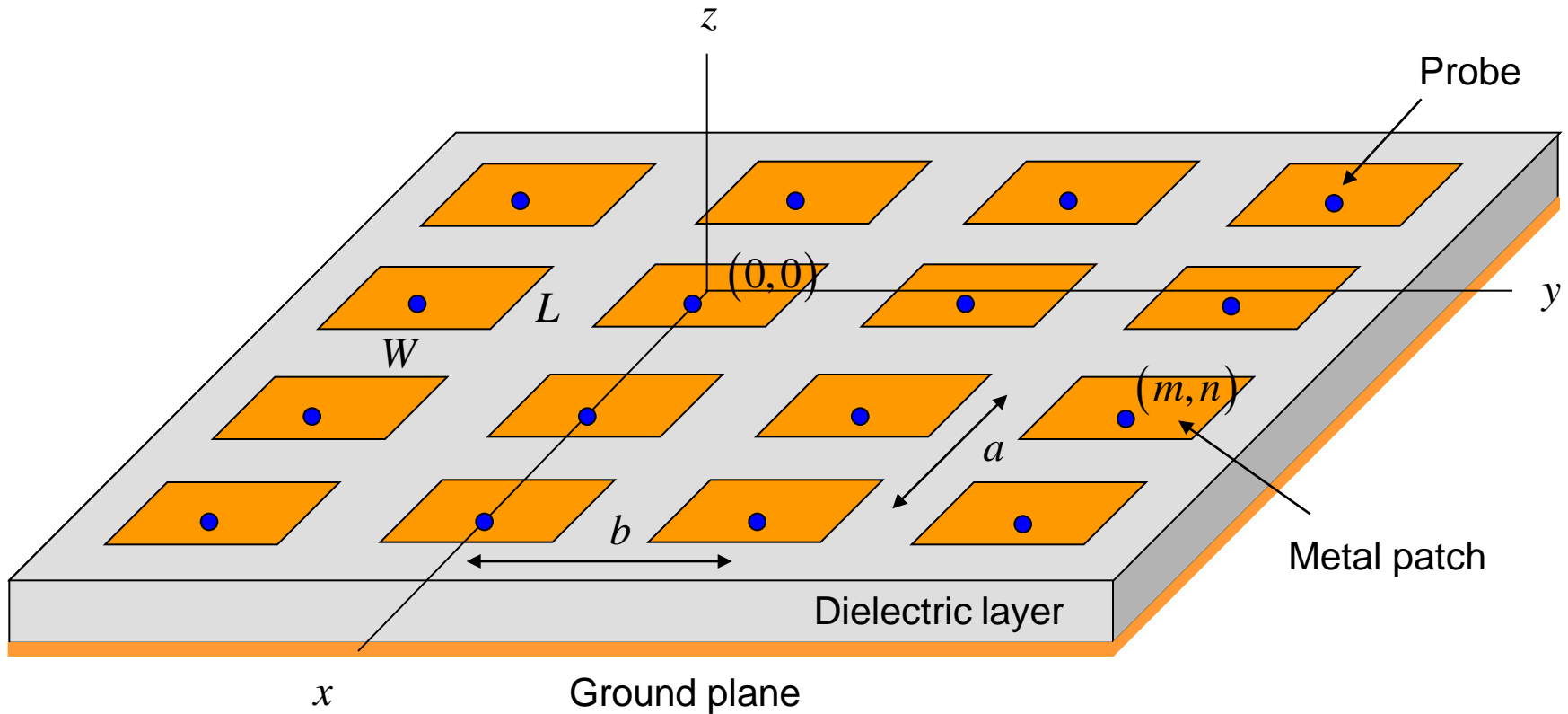


Note:
 ψ denotes any field component of interest.

Note: We are following “plane-wave” convention for k_{x0} and k_{y0} , and “transmission-line” convention for k_{z0} .

Microstrip Phased Array Geometry

Probe current mn :
$$I_{mn} = I_{00} e^{-j(k_{x0}ma + k_{y0}nb)}$$



The wavenumbers k_{x0} and k_{y0} are impressed by the feed network.

Microstrip Phased Array Geometry (cont.)

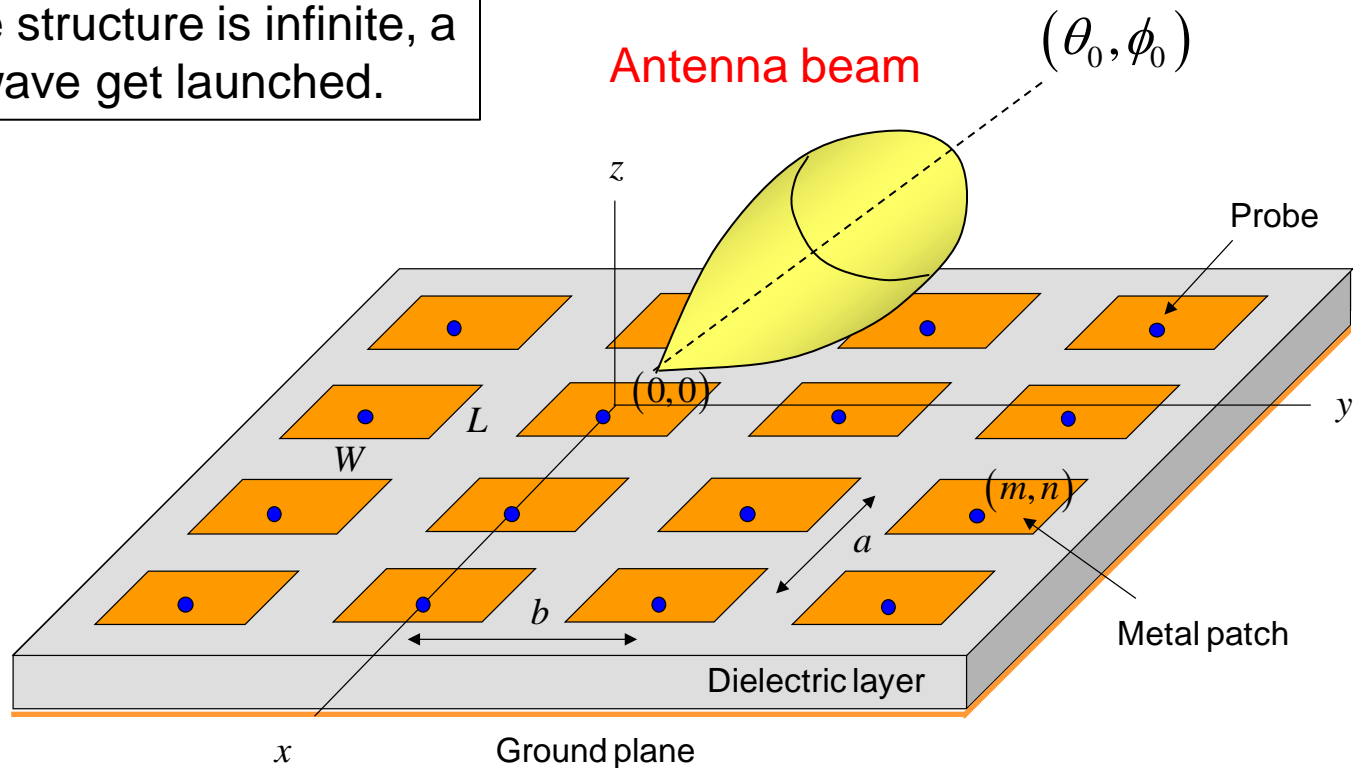
$$I_{mn} = I_{00} e^{-j(k_{x0}ma + k_{y0}nb)}$$

(θ_0, ϕ_0) = radiation angles

$$k_{x0} = k_0 \sin \theta_0 \cos \phi_0$$

$$k_{y0} = k_0 \sin \theta_0 \sin \phi_0$$

Note: If the structure is infinite, a plane wave get launched.

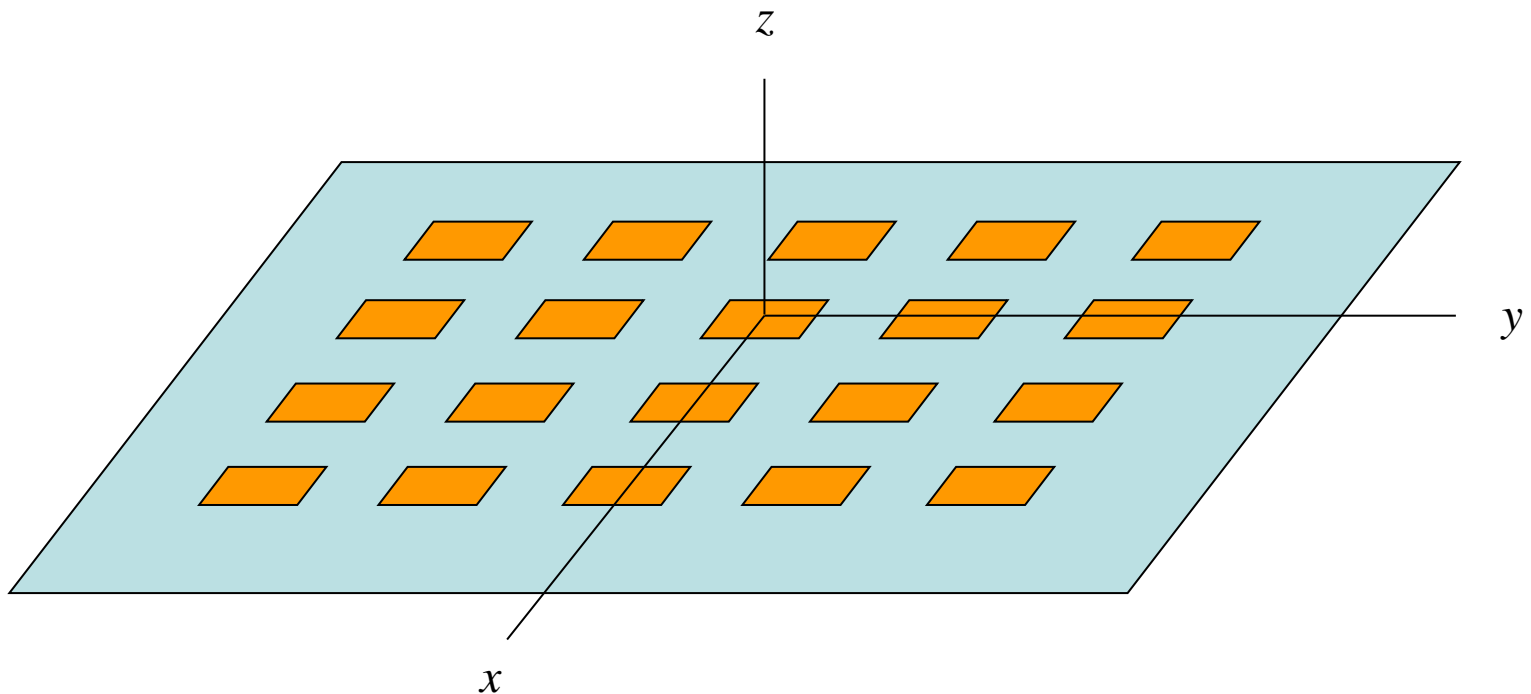


Floquet's Theorem

Fundamental observation:

If the structure is infinite and periodic, and the excitation is periodic except for a phase shift, then all of the currents and radiated fields will also be periodic except for a phase shift.

This is sometimes referred to as “*Floquet's theorem.*”

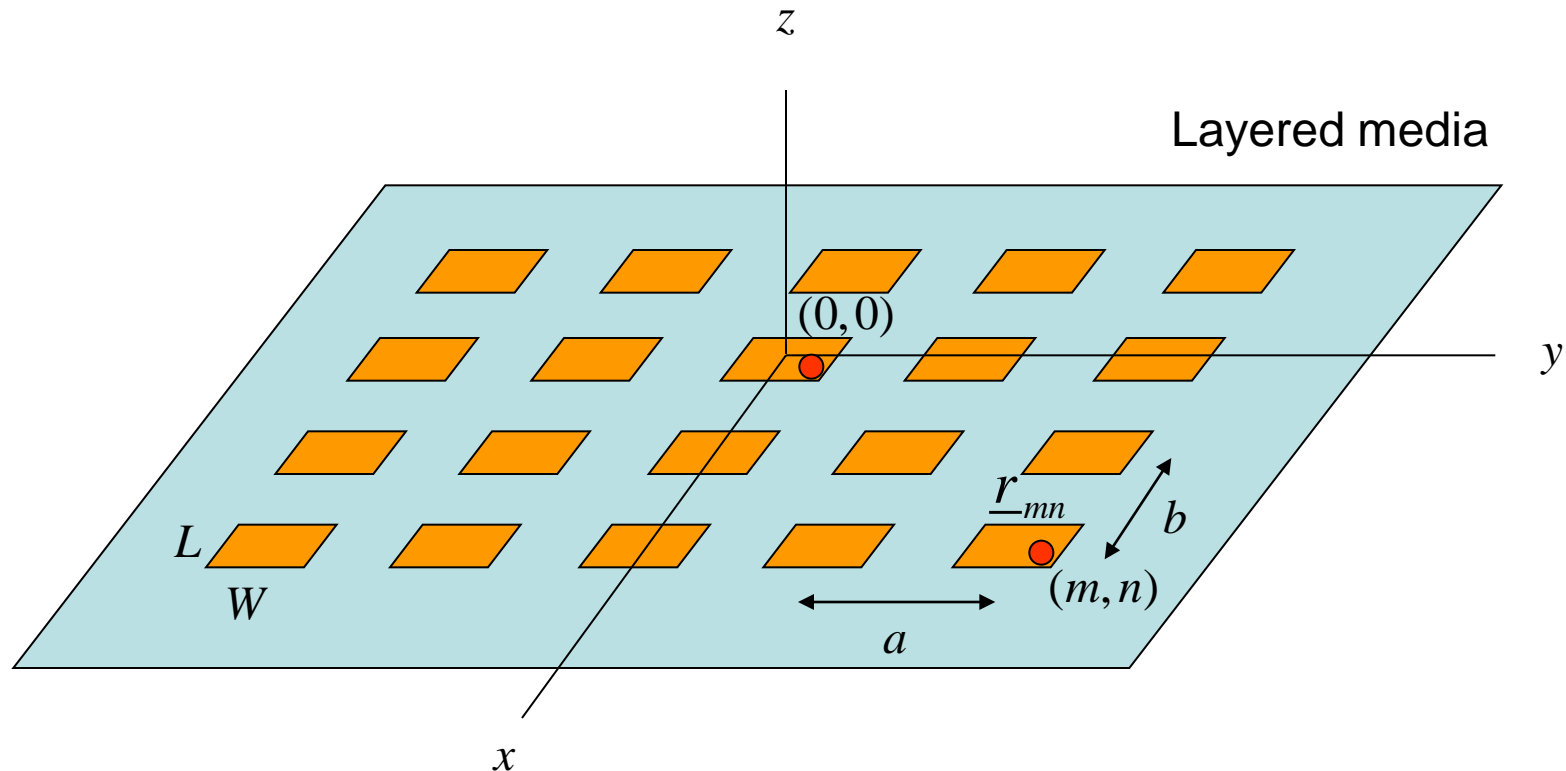


Floquet's Theorem (cont.)

From Floquet's theorem:

$$\underline{J}_s^{mn}(\underline{r}) = \underline{J}_s^{00}(\underline{r} - \underline{r}_{mn}) e^{-jk_{t00} \cdot \underline{r}_{mn}}$$

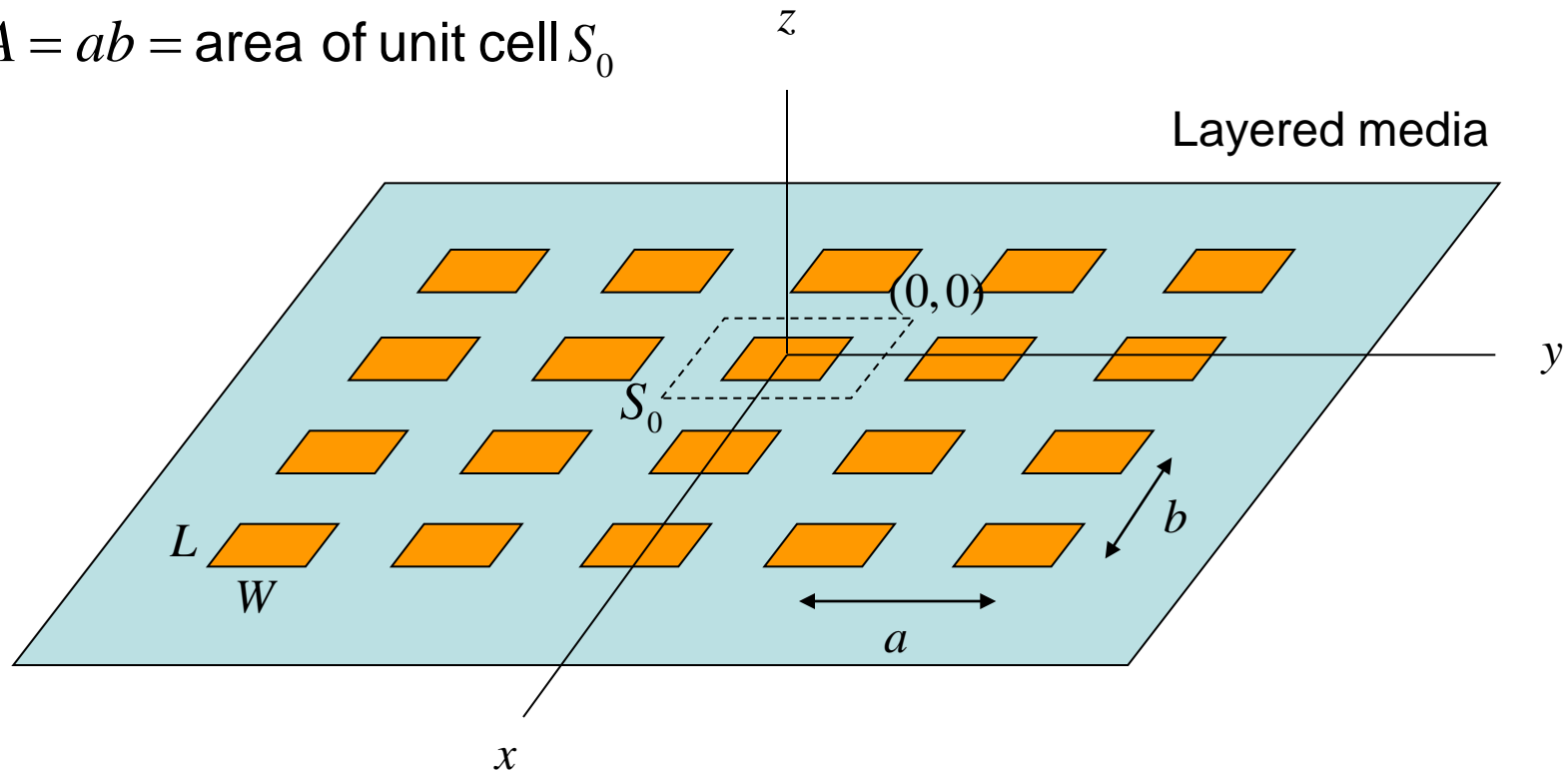
$$\underline{k}_{t00} = \underline{\hat{x}} k_{x0} + \underline{\hat{y}} k_y$$



Floquet's Theorem (cont.)

If we know the current or field at any point within the (0,0) unit cell, we know the current and field everywhere.

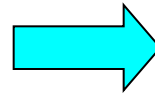
$$A = ab = \text{area of unit cell } S_0$$



Floquet Waves

Let ψ denote any component of the surface current or the field
(at a fixed value of z).

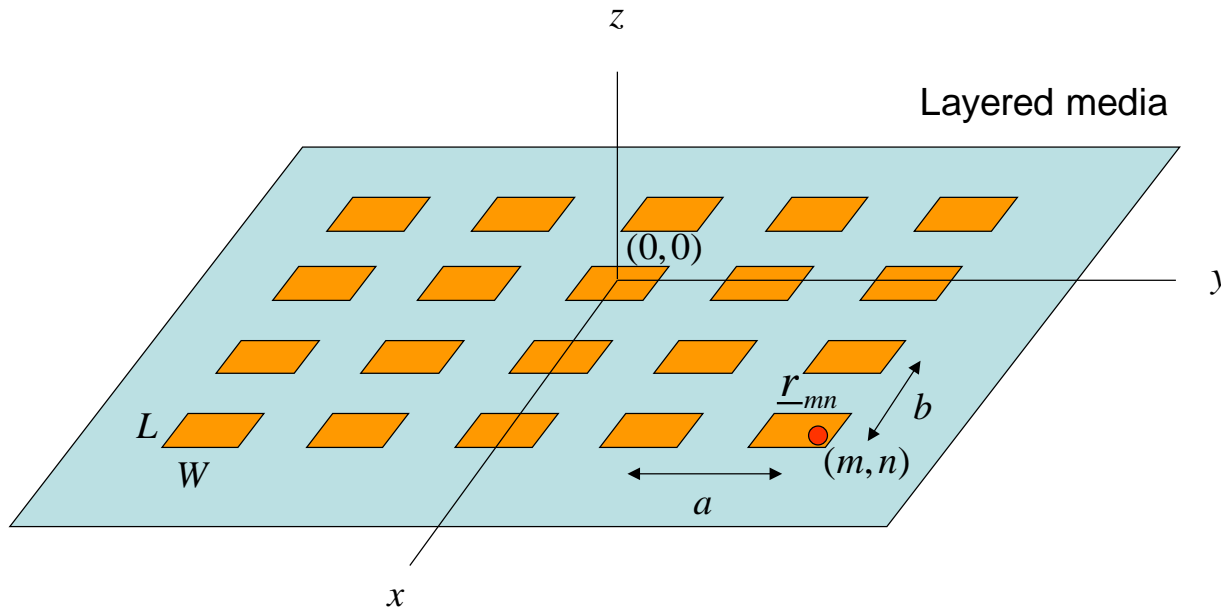
$$\psi(x+a, y) = \psi(x, y)e^{-jk_{x0}a}$$
$$\psi(x, y+b) = \psi(x, y)e^{-jk_{y0}b}$$



$$\psi(x, y) = e^{-j(k_{x0}x+k_{y0}y)}P(x, y)$$

where

$$P(x+a, y) = P(x, y)$$
$$P(x, y+b) = P(x, y)$$



Floquet Waves (cont.)

$$\psi(x, y) = e^{-j(k_{x0}x + k_{y0}y)} P(x, y)$$

From Fourier-series theory, we know that the 2D periodic function P can be represented as

$$P(x, y) = \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} A_{pq} e^{-j\left(\frac{2\pi p}{a}x + \frac{2\pi q}{b}y\right)}$$

Hence we have

$$\psi(x, y) = \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} A_{pq} e^{-j\left(\left(k_{x0} + \frac{2\pi p}{a}\right)x + \left(k_{y0} + \frac{2\pi q}{b}\right)y\right)}$$

Floquet Waves (cont.)

Hence, the surface current or field can be expanded in a set of Floquet waves:

$$\psi(x, y) = \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} A_{pq} e^{-j(k_{xp}x + k_{yq}y)}$$

$$k_{xp} \equiv k_{x0} + \frac{2\pi p}{a}$$

$$k_{yq} \equiv k_{y0} + \frac{2\pi q}{b}$$

(k_{xp}, k_{yq}) = wavenumbers of (p, q) Floquet wave

$$\underline{k}_{tpq} = \underline{\hat{x}} \underline{k}_{xp} + \underline{\hat{y}} \underline{k}_{yq}$$

$$\underline{k}_{tpq} = \left(\underline{\hat{x}} k_{x0} + \underline{\hat{y}} k_{y0} \right) + \left[\left(\frac{2\pi p}{a} \right) \underline{\hat{x}} + \left(\frac{2\pi q}{b} \right) \underline{\hat{y}} \right]$$

Incident part

Periodic part

Floquet Waves (cont.)

Note: Each Floquet wave repeats from one unit cell to the next, except for a phase shift that corresponds to that of the *incident wave*.

$$\begin{aligned}\psi_{pq}(x+a, y) &= e^{-j(k_{xp}(x+a)+k_{yq}y)} \\ &= e^{-j(k_{xp}a)} e^{-j(k_{xp}x+k_{yq}y)} \\ &= e^{-j(k_{x0}a)} e^{-j\left(\frac{2\pi p}{a}a\right)} e^{-j(k_{xp}x+k_{yq}y)} \\ &= e^{-j(k_{x0}a)} e^{-j(k_{xp}x+k_{yq}y)} \\ &= e^{-j(k_{x0}a)} \psi_{pq}(x, y)\end{aligned}$$

Hence

$$\psi_{pq}(x+a, y) = e^{-j(k_{x0}a)} \psi_{pq}(x, y)$$

Similarly,

$$\psi_{pq}(x, y+b) = e^{-j(k_{y0}b)} \psi_{pq}(x, y)$$

Periodic SDI

The **surface current** on the periodic structure is represented in terms of Floquet waves:

$$\underline{J}_s(x, y) = \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \underline{a}_{pq} e^{-jk_{pq} \cdot \underline{r}} \quad \underline{r} = \underline{\hat{x}} x + \underline{\hat{y}} y$$

To solve for the unknown coefficients, multiply both sides by $e^{jk_{p'q'} \cdot \underline{r}}$ and integrate over the (0,0) unit cell S_0 :

$$\begin{aligned} \int_{S_0} \underline{J}_s(x, y) e^{jk_{p'q'} \cdot \underline{r}} dS &= \int_{S_0} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \underline{a}_{pq} e^{-jk_{pq} \cdot \underline{r}} e^{jk_{p'q'} \cdot \underline{r}} dS \\ &= \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \int_{S_0} \underline{a}_{pq} e^{-j\left(\frac{2\pi}{a}(p-p')x + \frac{2\pi}{b}(q-q')y\right)} dS \end{aligned}$$

Use orthogonality: $\int_{S_0} \underline{J}_s(x, y) e^{jk_{p'q'} \cdot \underline{r}} dS = \underline{a}_{p'q'} A$

Periodic SDI (cont.)

Hence, we have:

$$\underline{a}_{pq} = \frac{1}{A} \int_{S_0} \underline{J}_s(x, y) e^{jk_{tpq} \cdot \underline{r}} dS$$

Therefore we have:

$$\begin{aligned} \underline{a}_{pq} &= \frac{1}{A} \int_{S_0} \underline{J}_s(x, y) e^{jk_{tpq} \cdot \underline{r}} dS \\ &= \frac{1}{A} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \underline{J}_s^{00}(x, y) e^{-j(k_{xp}x + k_{yq}y)} dS \\ &= \frac{1}{A} \tilde{\underline{J}}_s^{00}(k_{xp}, k_{yq}) \\ &= \frac{1}{A} \tilde{\underline{J}}_s^{00}(k_{tpq}) \end{aligned}$$

The current \underline{J}_s^{00} is the current on the (0,0) patch.

so

$$\underline{a}_{pq} = \frac{1}{A} \tilde{\underline{J}}_s^{00}(k_{xp}, k_{yq})$$

Periodic SDI (cont.)

Hence the current on the 2D periodic structure can be represented as

$$\underline{J}_s(x, y) = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{J}_s^{00}(k_{xp}, k_{yq}) e^{-jk_{pq} \cdot r}$$

We now calculate the **Fourier transform** of the 2D periodic current $\underline{J}_s(x, y)$ (this is what we need in the SDI method):

$$\begin{aligned} F \left[e^{-jk_{pq} \cdot r} \right] &= F \left[e^{-jk_{xp}x} e^{-jk_{yq}y} \right] \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left[e^{-jk_{xp}x} e^{-jk_{yq}y} \right] e^{+j(k_x x + k_y y)} dx dy \\ &= \int_{-\infty}^{\infty} e^{-jk_{xp}x} e^{+jk_x x} dx \int_{-\infty}^{\infty} e^{-jk_{yq}y} e^{+jk_y y} dy \\ &= 2\pi \delta(k_x - k_{xp}) 2\pi \delta(k_y - k_{yq}) \end{aligned}$$

Periodic SDI (cont.)

Hence

$$\underline{\tilde{J}}_s(k_x, k_y) = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \underline{\tilde{J}}_s^{00}(k_{xp}, k_{yq}) 2\pi\delta(k_x - k_{xp}) 2\pi\delta(k_y - k_{yq})$$

Next, we calculate the field produced by the periodic patch currents:

$$\underline{\tilde{E}}(k_x, k_y, z) = \underline{\underline{\tilde{G}}}(k_x, k_y; z, z') \cdot \underline{\tilde{J}}_s(k_x, k_y)$$

$$\underline{E}(x, y, z) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \underline{\underline{\tilde{G}}}(k_x, k_y; z, z') \cdot \underline{\tilde{J}}_s(k_x, k_y) e^{-j(k_x x + k_y y)} dk_x dk_y$$

Periodic SDI (cont.)

Hence, we have

$$\underline{E}(x, y, z) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \underline{\tilde{G}}(k_x, k_y; z, z') \cdot \left[\frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \underline{\tilde{J}}_s^{00}(k_{xp}, k_{yq}) 2\pi\delta(k_x - k_{xp}) 2\pi\delta(k_y - k_{yq}) \right] e^{-j(k_x x + k_y y)} dk_x dk_y$$

Periodic SDI (cont.)

Therefore, integrating over the delta functions, we have:

$$\underline{E}(x, y, z) = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \underline{\underline{G}}(k_{xp}, k_{yq}; z, z') \cdot \underline{J}_s^{00}(k_{xp}, k_{yq}) e^{-j(k_{xp}x + k_{yq}y)}$$

The field is thus in the form of a double summation of Floquet waves.

Periodic SDI (cont.)

Compare:

Single element (non-periodic):

$$\underline{E}(x, y, z) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \underline{\tilde{G}}(k_x, k_y; z, z') \cdot \underline{\tilde{J}}_s(k_x, k_y) e^{-j(k_x x + k_y y)} dk_x dk_y$$

Periodic array of phased elements:

$$\underline{E}(x, y, z) = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \underline{\tilde{G}}(k_{xp}, k_{yq}; z, z') \cdot \underline{\tilde{J}}_s^{00}(k_{xp}, k_{yq}) e^{-j(k_{xp} x + k_{yq} y)}$$

Periodic SDI (cont.)

Conclusion:

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} F(k_x, k_y) dk_x dk_y \rightarrow \frac{(2\pi)^2}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} F(k_{xp}, k_{yq})$$

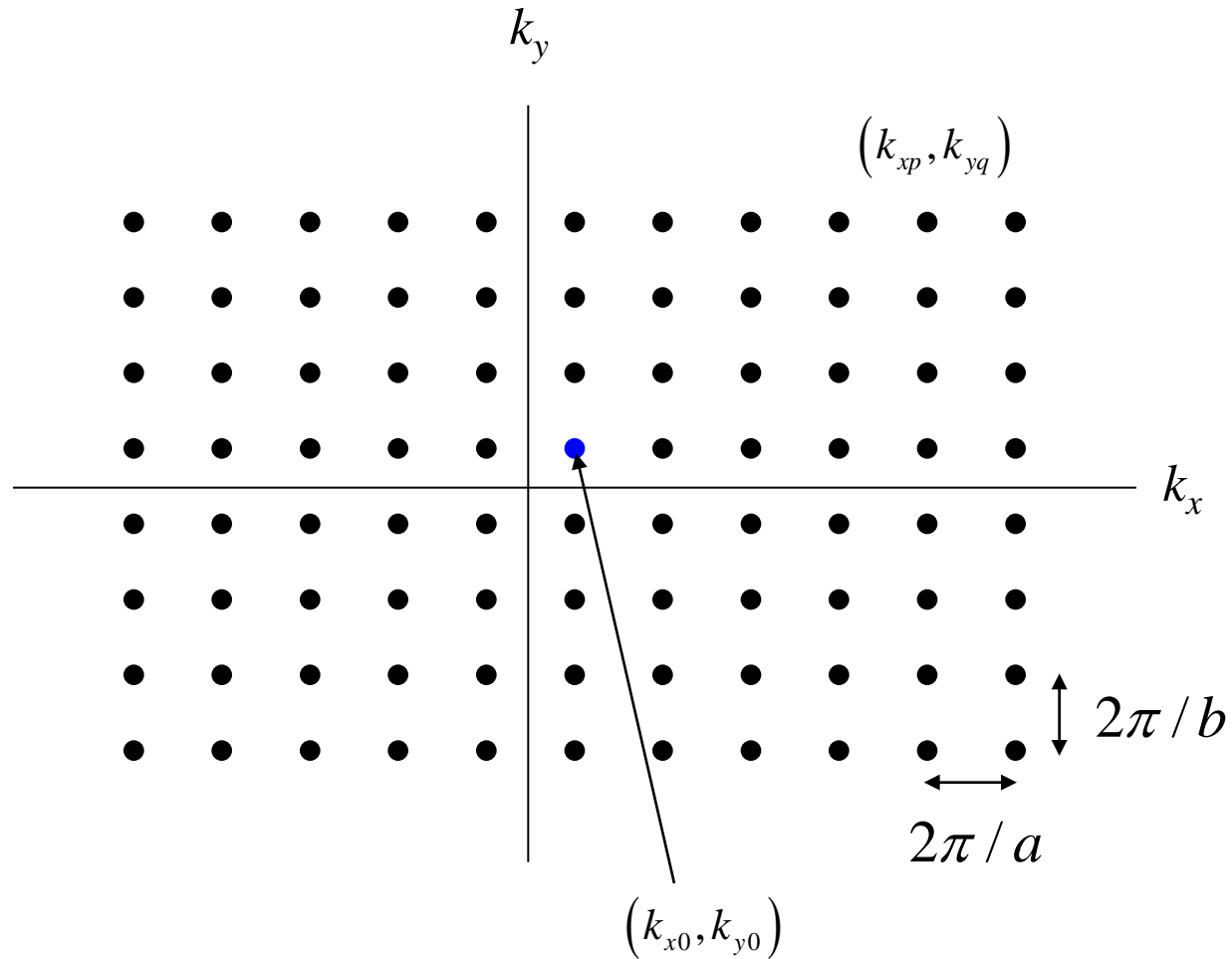
where

$$\begin{aligned} \underline{k}_{tpq} &= (\underline{\hat{x}}k_{xp} + \underline{\hat{y}}k_{yq}) \\ &= (\underline{\hat{x}}k_{x0} + \underline{\hat{y}}k_{y0}) + \left[\left(\frac{2\pi p}{a} \right) \underline{\hat{x}} + \left(\frac{2\pi q}{b} \right) \underline{\hat{y}} \right] \end{aligned}$$

The double integral is replaced by a double sum, and a factor is introduced.

Periodic SDI (cont.)

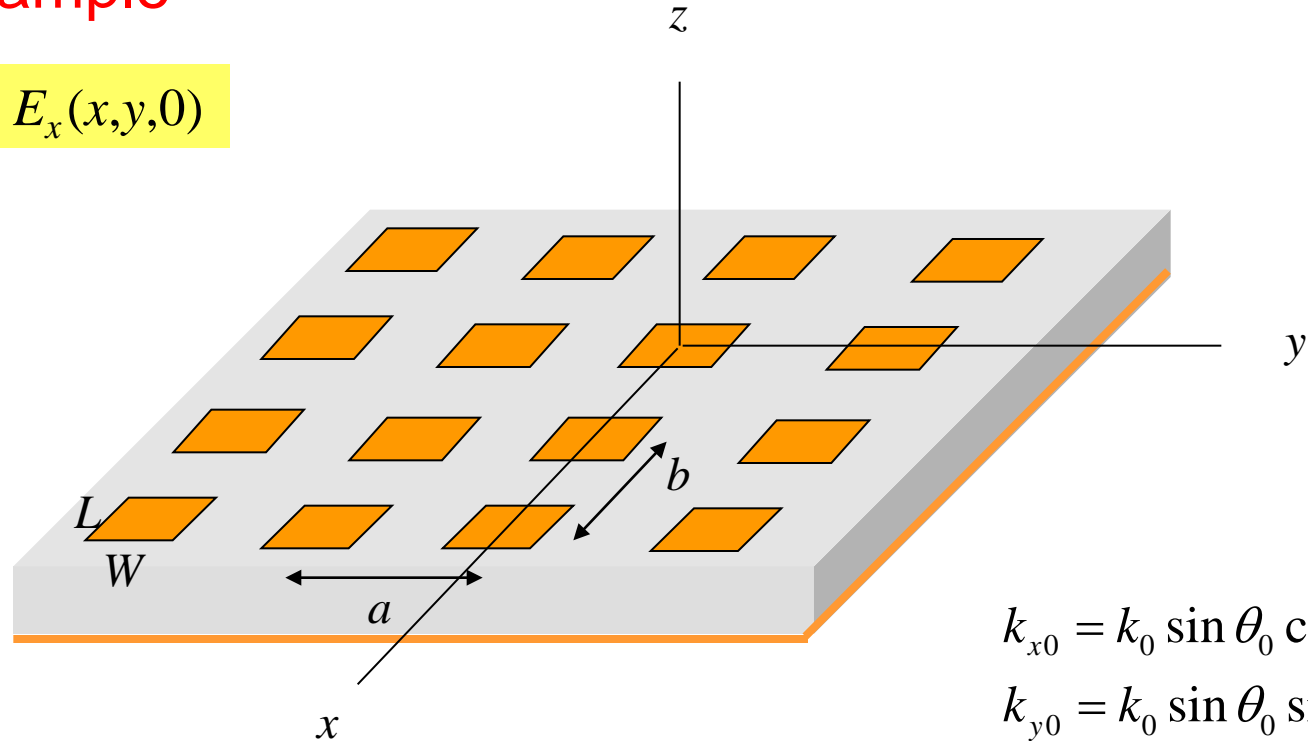
Sample points in the (k_x, k_y) plane



Microstrip Patch Phased Array

Example

Find $E_x(x,y,0)$



Microstrip Patch Phased Array

Phased Array (cont.)

Single patch:

$$E_x(x, y, 0) = \frac{1}{(2\pi)^2} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} -\frac{1}{k_t^2} \tilde{J}_{sx}(k_x, k_y) \cdot \left[\frac{k_x^2}{D_m(k_t)} + \frac{k_y^2}{D_e(k_t)} \right] e^{-j(k_x x + k_y y)} dk_x dk_y$$

$$J_{sx}(x, y) = \cos\left(\frac{\pi x}{L}\right)$$

$$\tilde{J}_{sx}(k_x, k_y) = \left(\frac{\pi}{2} LW\right) \text{sinc}\left(k_y \frac{W}{2}\right) \left[\frac{\cos\left(k_x \frac{L}{2}\right)}{\left(\frac{\pi}{2}\right)^2 - \left(k_x \frac{L}{2}\right)^2} \right]$$

Phased Array (cont.)

2D phased array of patches:

$$E_x(x, y, 0) = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} -\frac{1}{k_{tpq}^2} \tilde{J}_{sx}^{00}(k_{xp}, k_{yq}) \left[\frac{k_{xp}^2}{D_m(k_{tpq})} + \frac{k_{yq}^2}{D_e(k_{tpq})} \right] e^{-j(k_{xp}x + k_{yq}y)}$$

where

$$J_{sx}^{00}(x, y) = \cos\left(\frac{\pi x}{L}\right)$$

$$\tilde{J}_{sx}^{00}(k_{xp}, k_{yq}) = \left(\frac{\pi}{2} LW\right) \text{sinc}\left(k_{yq} \frac{W}{2}\right) \left[\frac{\cos\left(k_{xp} \frac{L}{2}\right)}{\left(\frac{\pi}{2}\right)^2 - \left(k_{xp} \frac{L}{2}\right)^2} \right]$$

$$k_{tpq} = \sqrt{k_{xp}^2 + k_{yq}^2}$$

Phased Array (cont.)

The field is of the form

$$\begin{aligned} E_x(x, y, 0) &= \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} A_{pq} e^{-j(k_{xp}x + k_{yq}y)} \\ &= \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} A_{pq} e^{-j\underline{k}_{pq} \cdot \underline{r}} \\ &= \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} A_{pq} \psi_{pq}(x, y) \end{aligned}$$

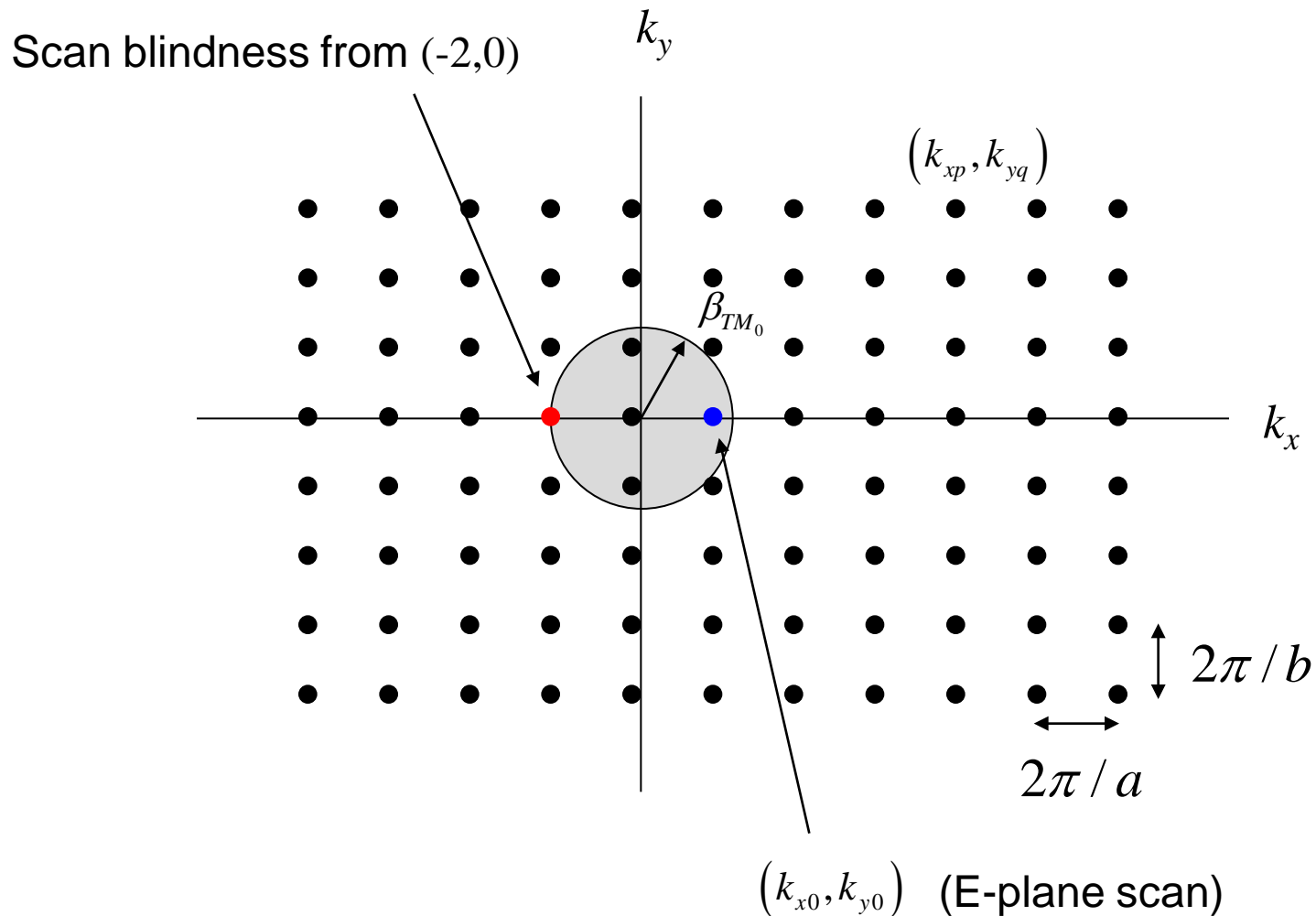
where

$$\underline{k}_{pq} = \underline{\hat{x}}k_{xp} + \underline{\hat{y}}k_{yq} = \left(\underline{\hat{x}}k_{x0} + \underline{\hat{y}}k_{y0} \right) + \left[\left(\frac{2\pi p}{a} \right) \underline{\hat{x}} + \left(\frac{2\pi q}{b} \right) \underline{\hat{y}} \right]$$

The field is thus represented as a “sum of Floquet waves.”

Scan Blindness in Phased Array

This occurs when one of the sample points (p,q) lies on the surface-wave circle (shown for $(-2, 0)$).



Scan Blindness (cont.)

The scan blindness condition is:

$$k_{tpq} = |k_{-tpq}| = \beta_{TM_0} \quad (\text{for some } (p, q))$$

$$E_x(x, y, 0) = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} -\frac{1}{k_{tpq}^2} \tilde{J}_{sx}^{00}(k_{xp}, k_{yq}) \left[\frac{k_{xp}^2}{D_m(k_{tpq})} + \frac{k_{yq}^2}{D_e(k_{tpq})} \right] e^{-j(k_{xp}x + k_{yq}y)}$$

$$D_m(k_{tpq}) = D_m(\beta_{TM_0}) = 0$$

The field produced by an *impressed* set of infinite periodic phased surface-current sources will be **infinite**.

Scan Blindness (cont.)

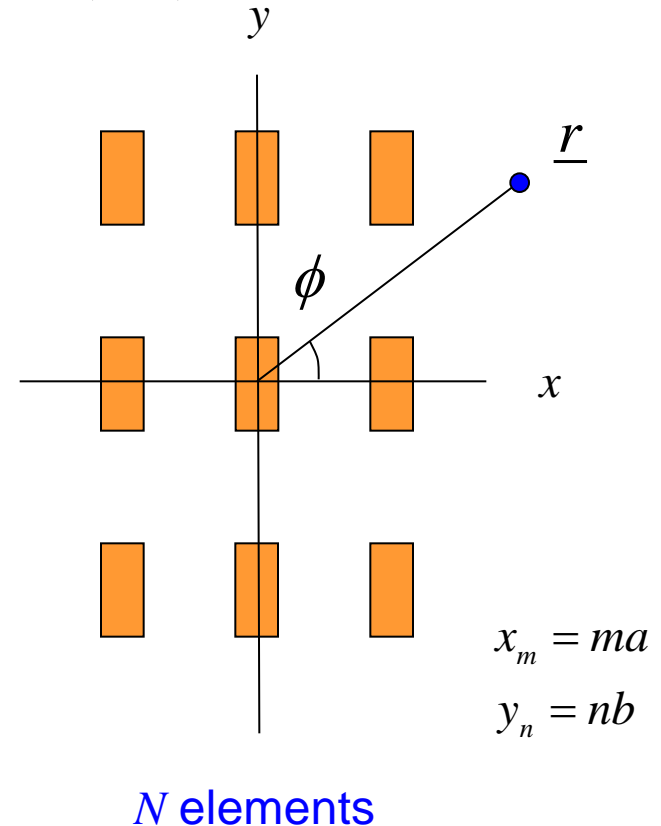
Physical interpretation: All of the surface-wave fields excited from the patches add up in phase in the direction of the transverse phasing vector:

$$\underline{k}_{tpq} = \underline{\hat{x}}k_{xp} + \underline{\hat{y}}k_{yq} \quad \Rightarrow \quad \cos \phi = \left(\frac{k_{xp}}{k_{tpq}} \right)$$

Proof:

Start with the *surface-wave array factor*:

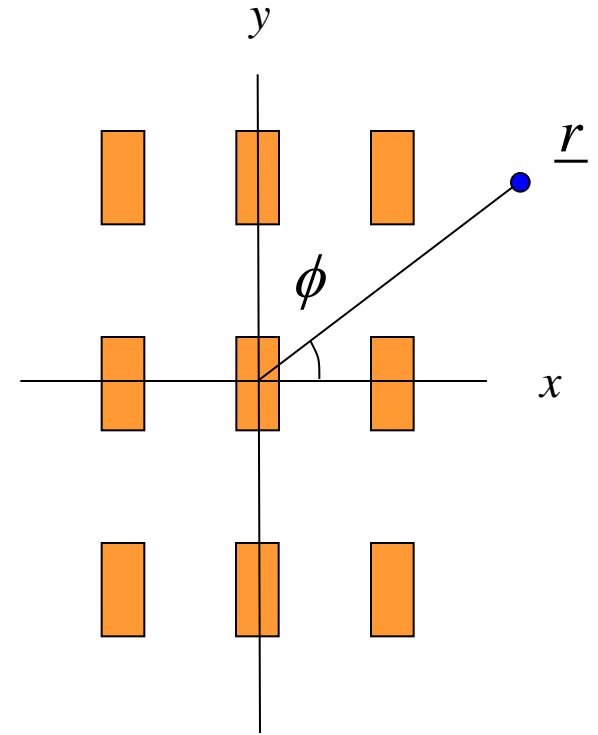
$$\begin{aligned} AF_{sw} &= \sum_{m,n} A_{mn} e^{+j(\beta_{TM0}x_m \cos \phi + \beta_{TM0}y_n \sin \phi)} \\ &= \sum_{m,n} A_{mn} e^{+j\left(\beta_{TM0}x_m \left(\frac{k_{xp}}{k_{tpq}}\right) + \beta_{TM0}y_n \left(\frac{k_{yq}}{k_{tpq}}\right)\right)} \\ &= \sum_{m,n} A_{mn} e^{+j\left(\beta_{TM0}x_m \left(\frac{k_{xp}}{\beta_{TM0}}\right) + \beta_{TM0}y_n \left(\frac{k_{yq}}{\beta_{TM0}}\right)\right)} \end{aligned}$$



Scan Blindness (cont.)

Hence we have, in this direction, that

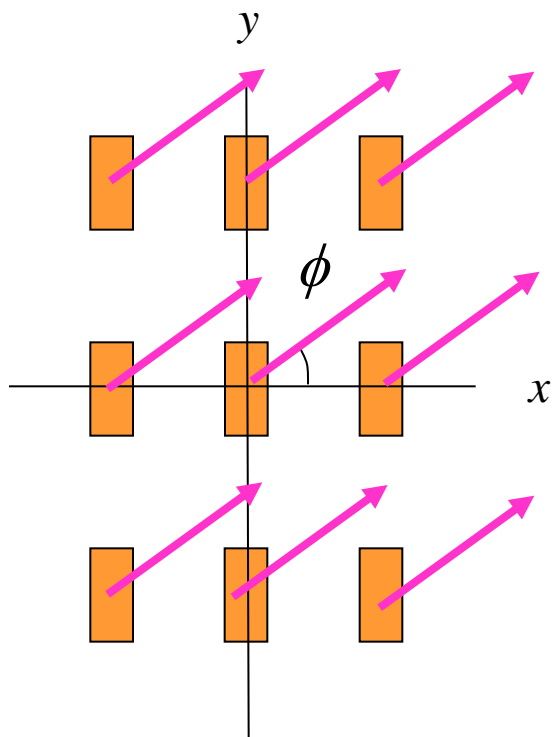
$$\begin{aligned}
 AF_{sw} &= \sum_{m,n} A_{mn} e^{+j(k_{xp}x_m + k_{yq}y_n)} \\
 &= \sum_{m,n} A_{mn} e^{+j\left(\left(k_{x0} + \frac{2\pi p}{a}\right)x_m + \left(k_{y0} + \frac{2\pi q}{b}\right)y_n\right)} \\
 &= \sum_{m,n} A_{mn} e^{+j\left(\left(k_{x0} + \frac{2\pi p}{a}\right)(x_0 + ma) + \left(k_{y0} + \frac{2\pi q}{b}\right)(y_0 + nb)\right)} \\
 &= e^{+jk_{xp}x_0} e^{+jk_{yq}y_0} \sum_{m,n} A_{mn} e^{+j(k_{x0}ma + k_{y0}nb)} e^{+j\left(\frac{2\pi p}{a}\right)ma} e^{+j\left(\frac{2\pi q}{b}\right)nb} \\
 &= e^{+jk_{xp}x_0} e^{+jk_{yq}y_0} \sum_{m,n} A_{mn} e^{+j(k_{x0}ma + k_{y0}nb)} \\
 &= e^{+jk_{xp}x_0} e^{+jk_{yq}y_0} \sum_{m,n} A_{00} e^{-j(k_{x0}ma + k_{y0}nb)} e^{+j(k_{x0}ma + k_{y0}nb)} \\
 &= e^{+jk_{xp}x_0} e^{+jk_{yq}y_0} A_{00} N
 \end{aligned}$$



N elements

$$\cos \phi = \left(\frac{k_{xp}}{k_{tpq}} \right)$$

Scan Blindness (cont.)



N elements

TM_0 surface wave

In the direction ϕ , the surface fields from each patch add up in phase.

$$\cos \phi = \left(\frac{k_{xp}}{\beta_{TM_0}} \right)$$

$$\Rightarrow AF_{sw} = N \left(A_{00} e^{+jk_{xp}x_0} e^{+jk_{yq}y_0} \right)$$

Note: There is also an element pattern as well, with the field decaying as $1/\rho^{1/2}$, but this is ignored here.

Scan Blindness (cont.)

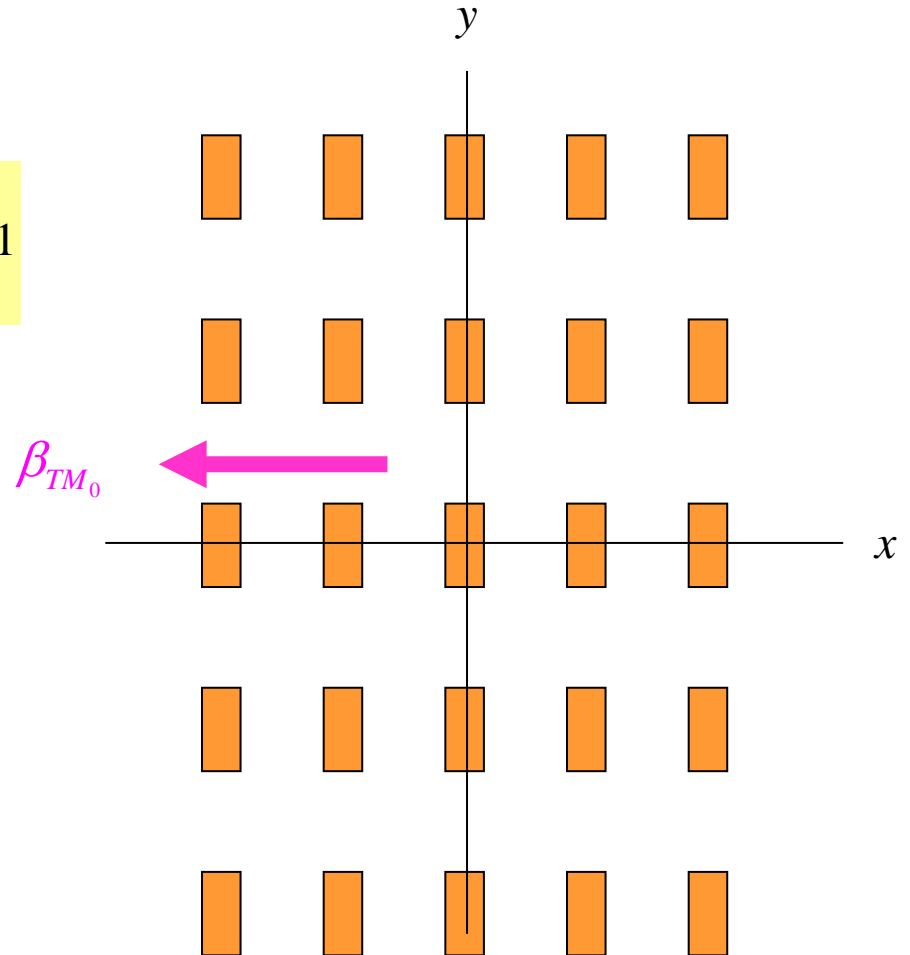
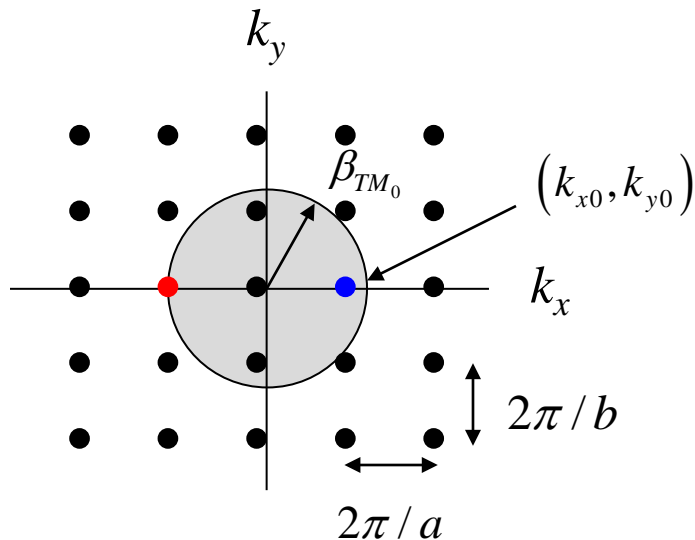
Example

$$p = -2, \quad q = 0$$

$$k_{xp} = -\beta_{TM_0}$$

$$k_{yq} = 0$$

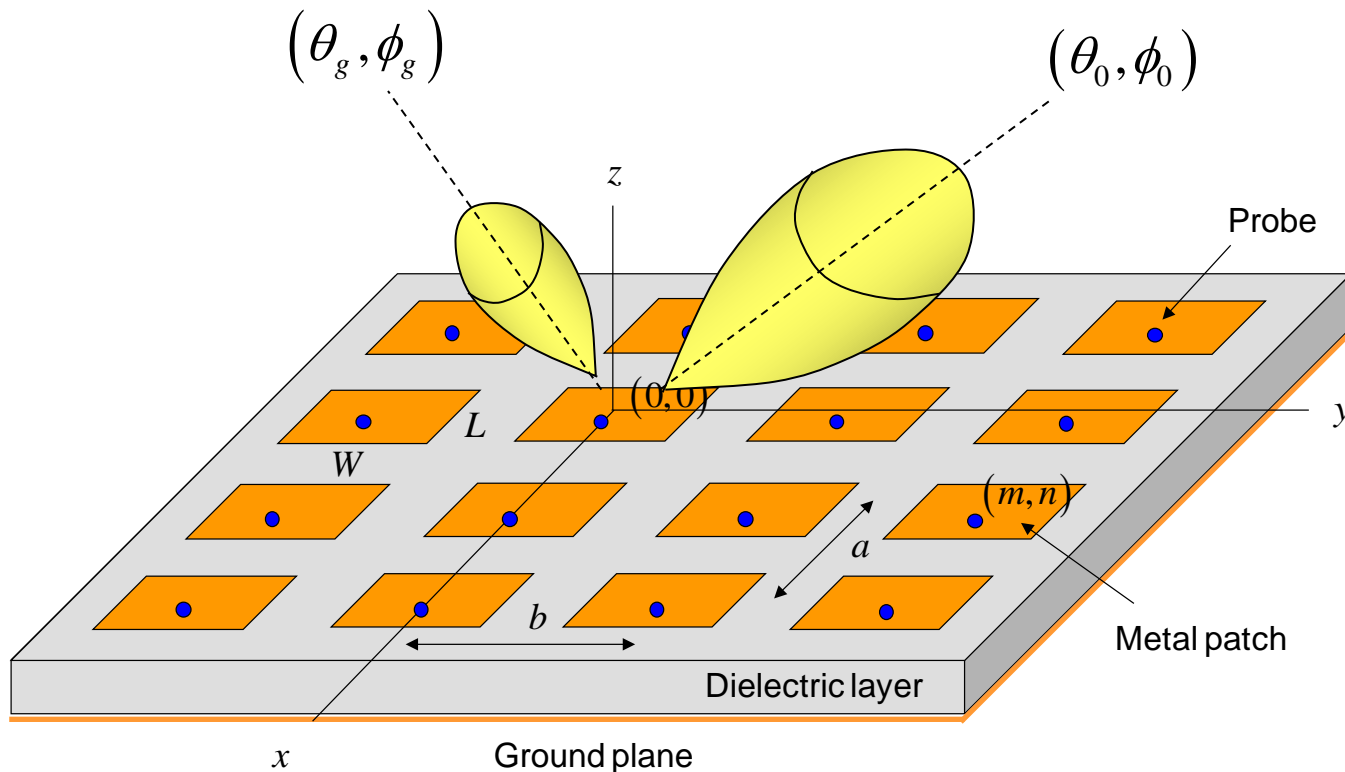
$$\cos \phi = \left(\frac{-\beta_{TM_0}}{\beta_{TM_0}} \right) = -1$$



E-plane scan

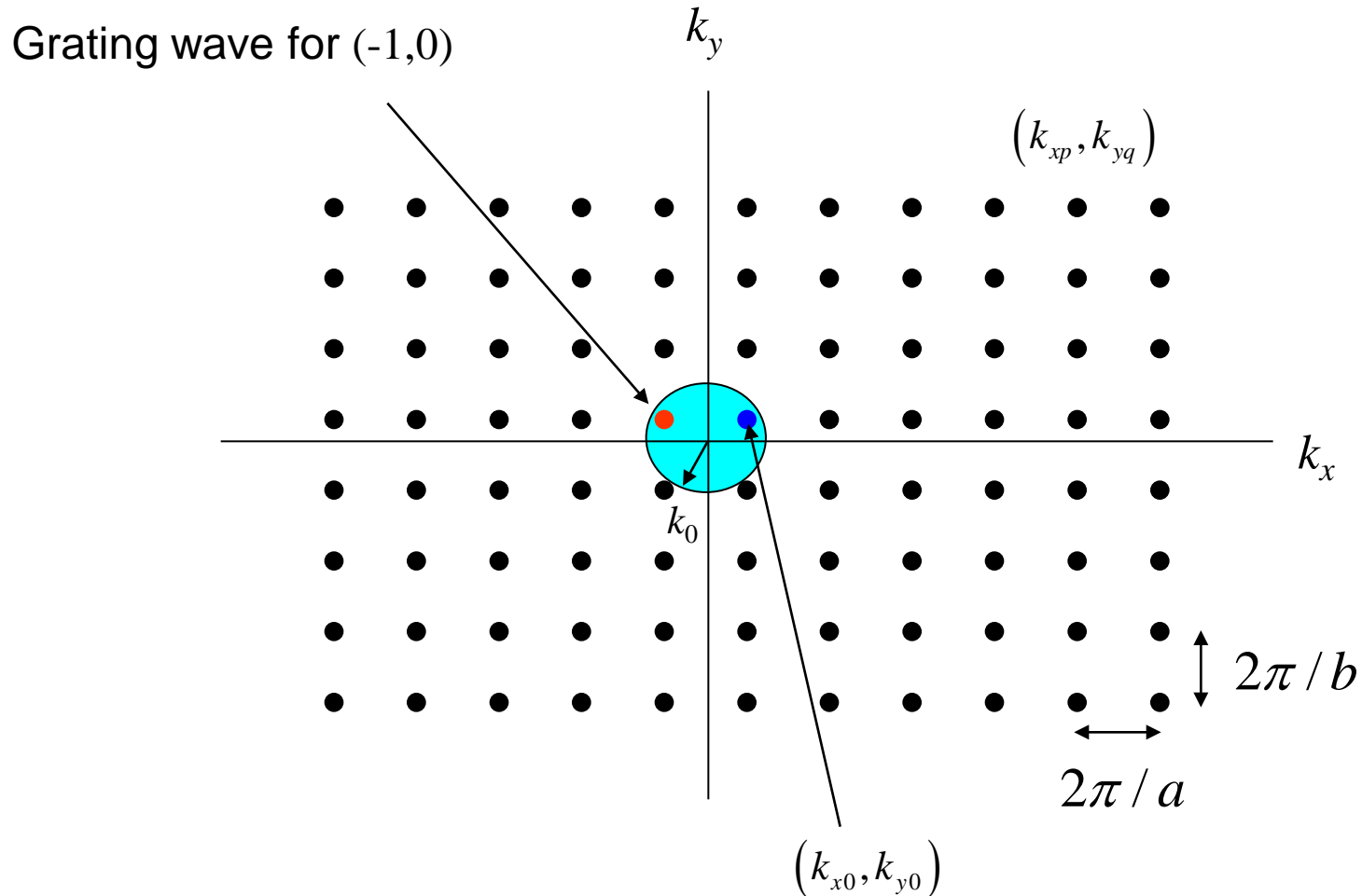
Grating Lobes

- ❖ Grating lobes occur when one or more of the higher-order Floquet waves propagates in space.
- ❖ For a finite-size array, this corresponds to a secondary beam that gets radiated.



Grating Lobes (cont.)

$$k_{tpq} < k_0 \quad (\text{for some } (p, q) \neq (0, 0))$$



Pozar Circle Diagram

Define

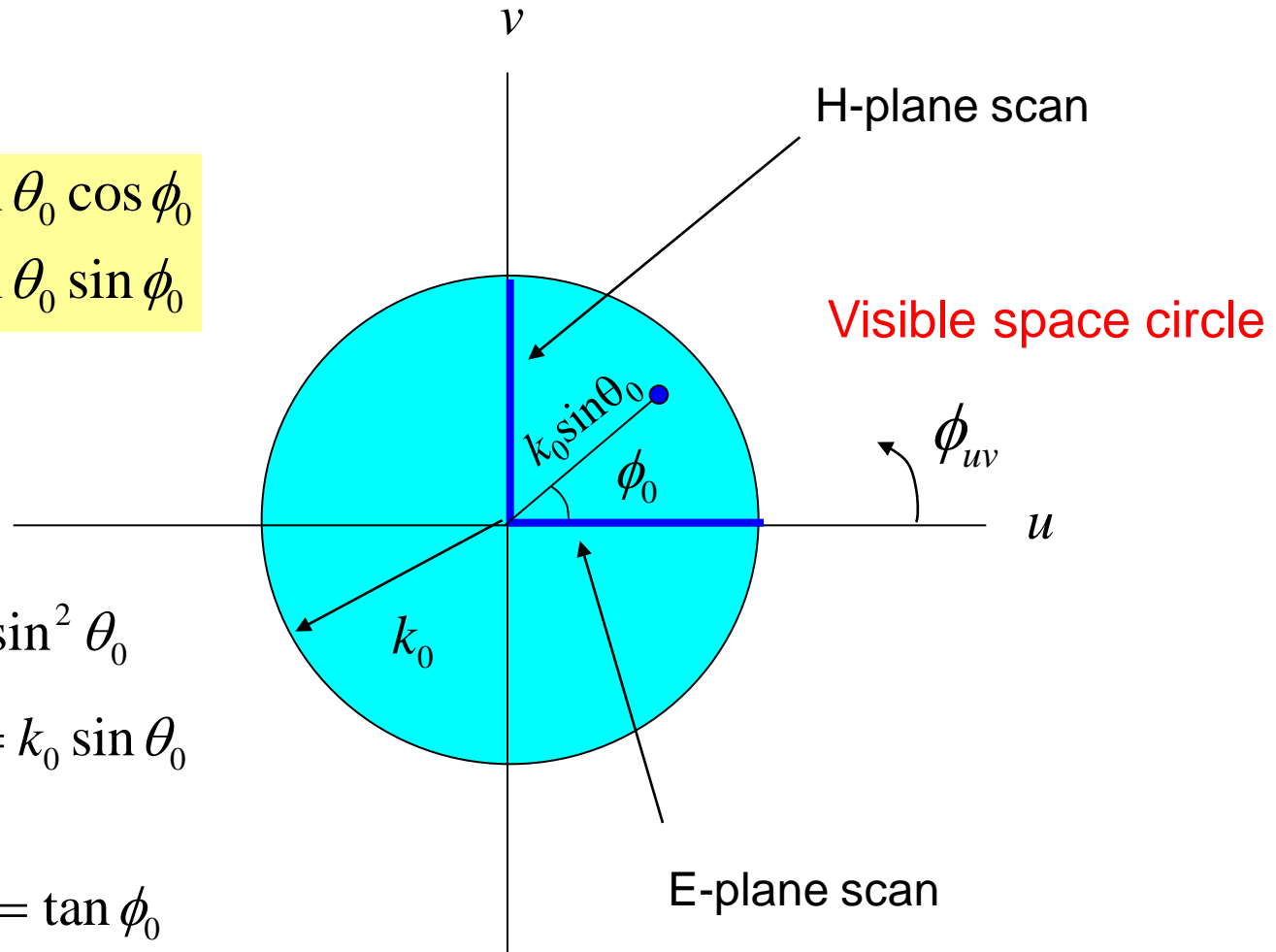
$$u \equiv k_{x0} = k_0 \sin \theta_0 \cos \phi_0$$

$$v \equiv k_{y0} = k_0 \sin \theta_0 \sin \phi_0$$

$$u^2 + v^2 = k_0^2 \sin^2 \theta_0$$
$$\Rightarrow \sqrt{u^2 + v^2} = k_0 \sin \theta_0$$

$$\tan \phi_{uv} = v / u = \tan \phi_0$$

$$\Rightarrow \phi_{uv} = \phi_0$$



Pozar Circle Diagram (cont.)

Grating Lobes

$$k_{tpq} < k_0 \quad \text{for } (u, v) \in \text{visible space circle}$$

So, we require that

$$k_{xp}^2 + k_{yq}^2 < k_0^2 \quad \text{for } u^2 + v^2 < k_0^2$$

The first inequality gives us

$$\left(k_{x0} + \frac{2\pi p}{a}\right)^2 + \left(k_{y0} + \frac{2\pi q}{b}\right)^2 < k_0^2$$

or

$$\left(k_0 \sin \theta_0 \cos \phi_0 + \frac{2\pi p}{a}\right)^2 + \left(k_0 \sin \theta_0 \sin \phi_0 + \frac{2\pi q}{b}\right)^2 < k_0^2$$

or

$$\left(u + \frac{2\pi p}{a}\right)^2 + \left(v + \frac{2\pi q}{b}\right)^2 < k_0^2$$

Pozar Circle Diagram (cont.)

or

$$\left(u - \left(-\frac{2\pi p}{a}\right)\right)^2 + \left(v - \left(-\frac{2\pi q}{b}\right)\right)^2 < k_0^2$$

or

$$(u - u_p)^2 + (v - v_q)^2 < k_0^2 \quad (\text{we are inside a shifted } (p, q) \text{ visible space circle})$$

$$u_p \equiv -\frac{2\pi p}{a}, \quad v_q \equiv -\frac{2\pi q}{b}$$

Summary of grating lobe condition:

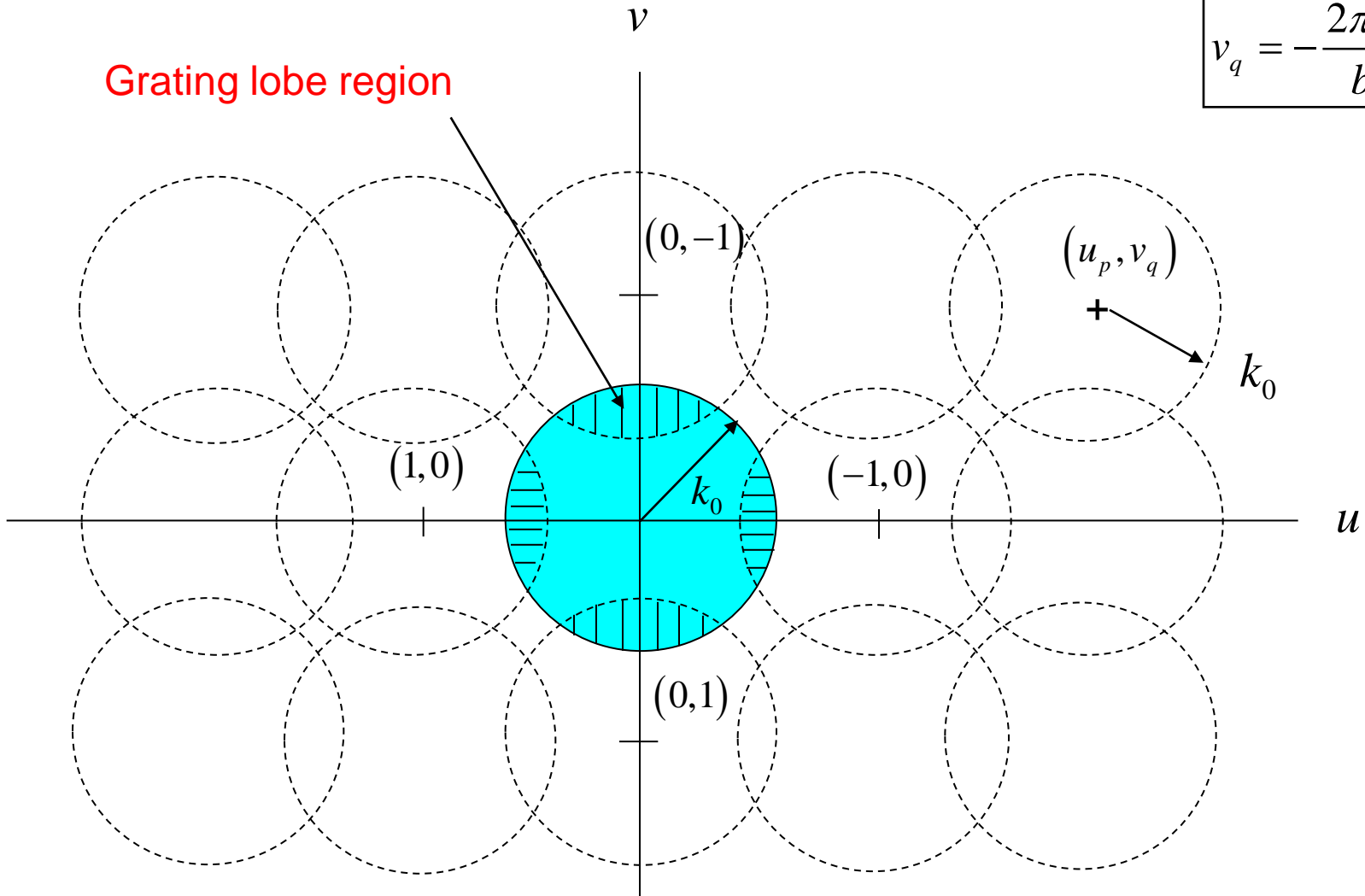
$$\begin{aligned} (u - u_p)^2 + (v - v_q)^2 &< k_0^2 \\ u^2 + v^2 &< k_0^2 \end{aligned}$$

Part of the *interior* of the (p, q) circle is also inside the visible space circle.

Pozar Circle Diagram (cont.)

$$(u - u_p)^2 + (v - v_q)^2 < k_0^2$$
$$u^2 + v^2 < k_0^2$$

$$u_p = -\frac{2\pi p}{a}$$
$$v_q = -\frac{2\pi q}{b}$$

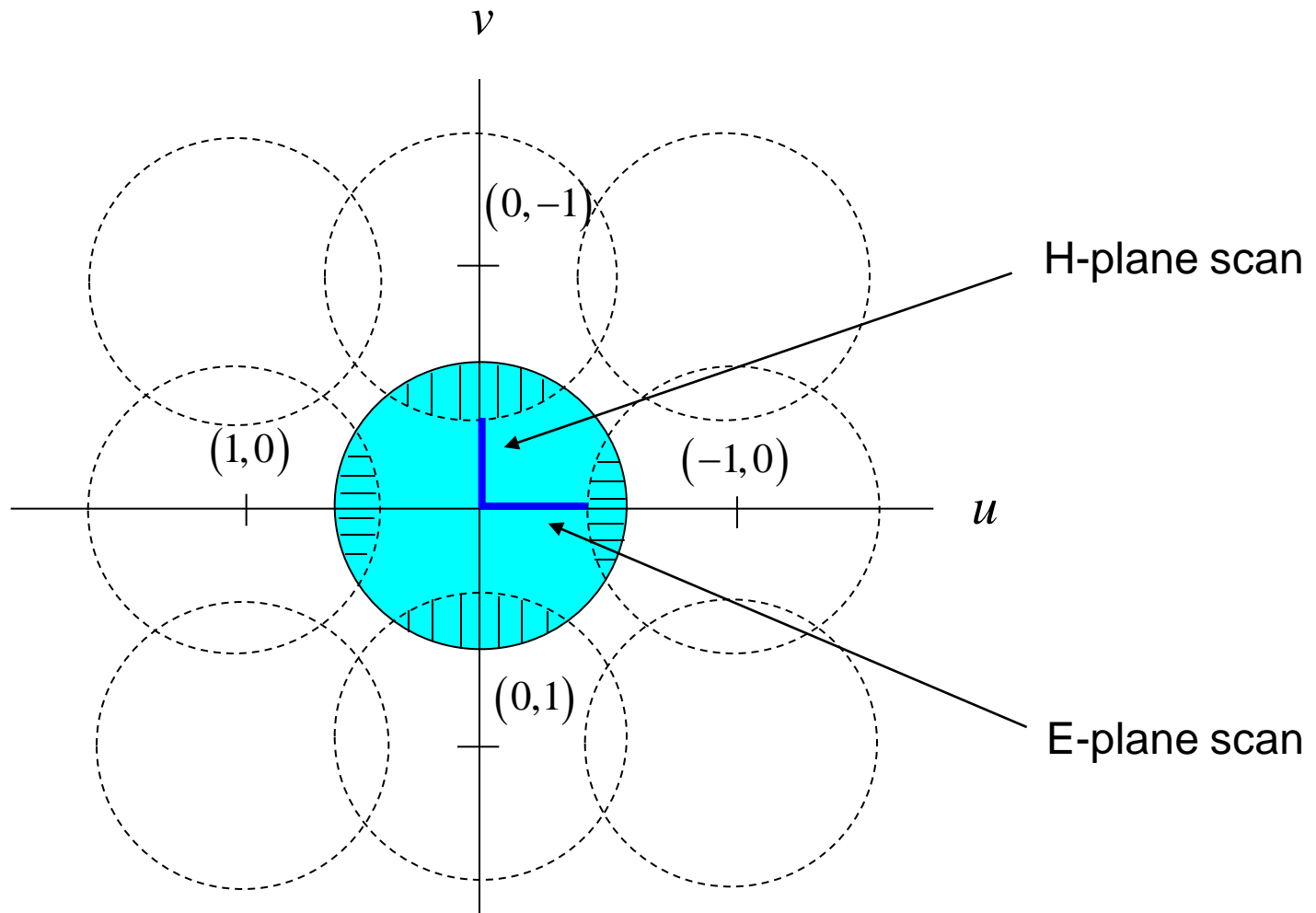


Pozar Circle Diagram (cont.)

This diagram shows when grating lobes occur in the principal scan planes.

$$u = k_0 \sin \theta_0 \cos \phi_0$$

$$v = k_0 \sin \theta_0 \sin \phi_0$$



Pozar Circle Diagram (cont.)

To avoid grating lobes for all scan angles, we require:

$$u_{-1} > 2k_0$$

$$v_{-1} > 2k_0$$

(The circles do not overlap.)

or

$$\frac{2\pi}{a} > 2k_0$$

$$\frac{2\pi}{b} > 2k_0$$

or

$$k_0 a < \pi$$

$$k_0 b < \pi$$

Hence

$$a < \lambda_0 / 2$$

$$b < \lambda_0 / 2$$

Pozar Circle Diagram (cont.)

Scan Blindness

$$k_{tpq} = \beta_{TM_0} \text{ for } (u, v) \in \text{visible space circle}$$

So, we require that

$$k_{xp}^2 + k_{yq}^2 = \beta_{TM_0}^2 \quad \text{for } u^2 + v^2 < k_0^2$$

The equation gives us

$$\left(k_{x0} + \frac{2\pi p}{a} \right)^2 + \left(k_{y0} + \frac{2\pi q}{b} \right)^2 = \beta_{TM_0}^2$$

or

$$\left(k_0 \sin \theta_0 \cos \phi_0 + \frac{2\pi p}{a} \right)^2 + \left(k_0 \sin \theta_0 \sin \phi_0 + \frac{2\pi q}{b} \right)^2 = \beta_{TM_0}^2$$

or

$$\left(u + \frac{2\pi p}{a} \right)^2 + \left(v + \frac{2\pi q}{b} \right)^2 = \beta_{TM_0}^2$$

Pozar Circle Diagram (cont.)

or

$$\left(u - \left(-\frac{2\pi p}{a}\right)\right)^2 + \left(v - \left(-\frac{2\pi q}{b}\right)\right)^2 = \beta_{TM_0}^2$$

or

$$(u - u_p)^2 + (v - v_q)^2 = \beta_{TM_0}^2$$

where

$$u_p = -\frac{2\pi p}{a}$$

$$v_q = -\frac{2\pi q}{b}$$

Summary of scan blindness condition:

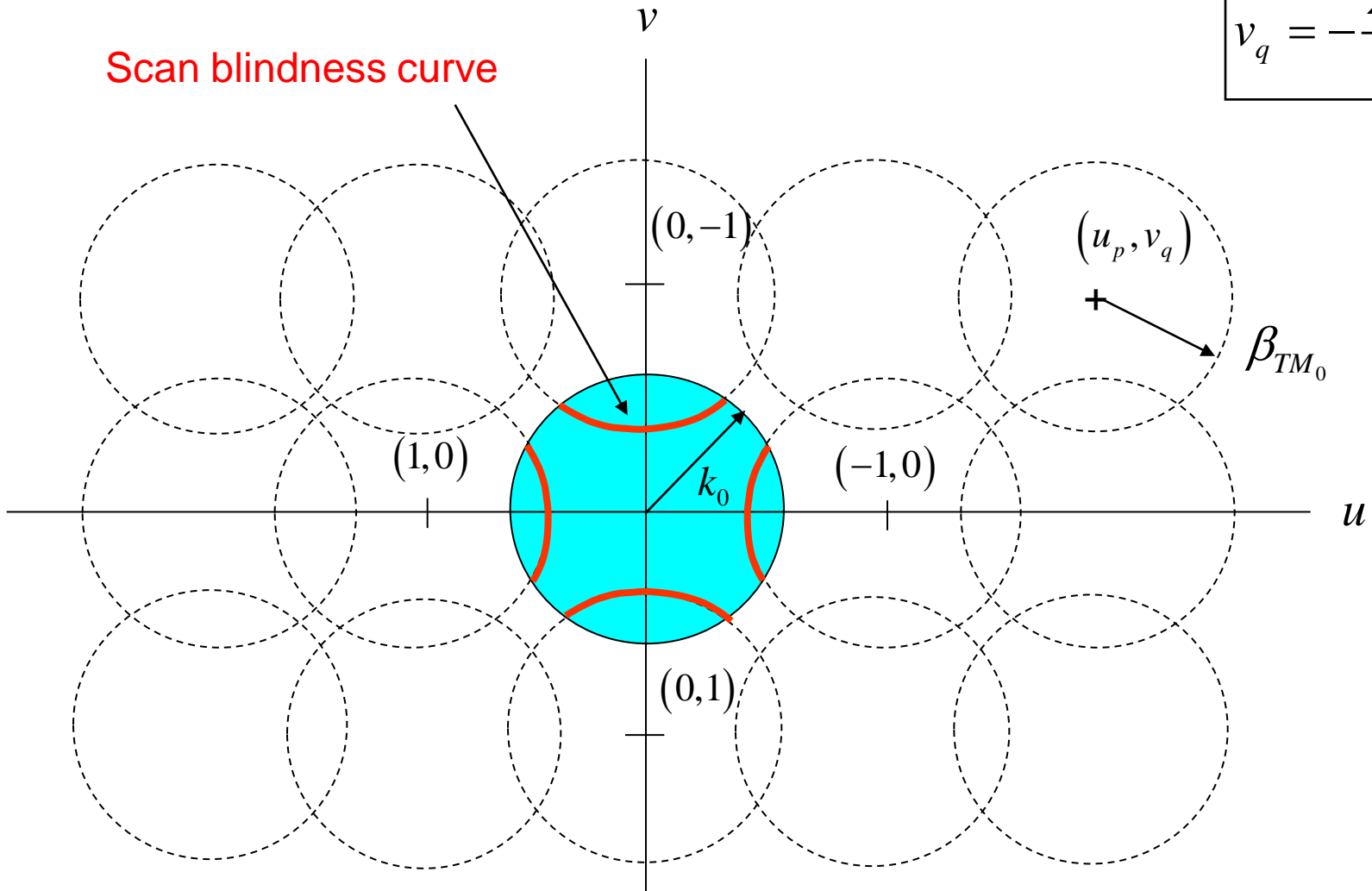
$$(u - u_p)^2 + (v - v_q)^2 = \beta_{TM_0}^2$$
$$u^2 + v^2 < k_0^2$$

Part of the *boundary* of the (p,q) circle is inside the visible space circle.

Pozar Circle Diagram (cont.)

$$(u - u_p)^2 + (v - v_q)^2 = \beta_{TM_0}^2$$
$$u^2 + v^2 < k_0^2$$

$$u_p = -\frac{2\pi p}{a}$$
$$v_q = -\frac{2\pi q}{b}$$



Pozar Circle Diagram (cont.)

To avoid scan blindness for all scan angles, we require

$$u_{-1} > \beta_{TM_0} + k_0$$

$$v_{-1} > \beta_{TM_0} + k_0$$

(The circles do not overlap.)

or

$$\frac{2\pi}{a} > \beta_{TM_0} + k_0$$

$$\frac{2\pi}{b} > \beta_{TM_0} + k_0$$

or

$$\frac{2\pi}{k_0 a} > \beta_{TM_0} / k_0 + 1$$

$$\frac{2\pi}{k_0 b} > \beta_{TM_0} / k_0 + 1$$

Hence

$$a / \lambda_0 < \frac{1}{\beta_{TM_0} / k_0 + 1}$$

$$b / \lambda < \frac{1}{\beta_{TM_0} / k_0 + 1}$$