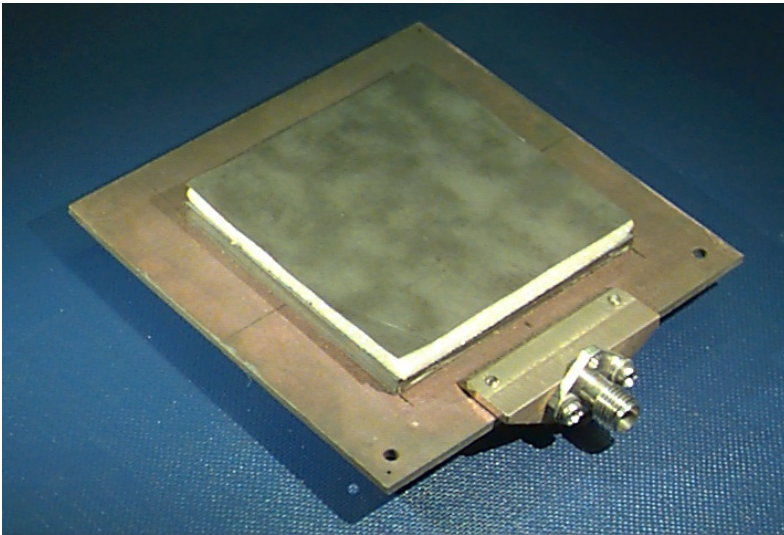


ECE 6345

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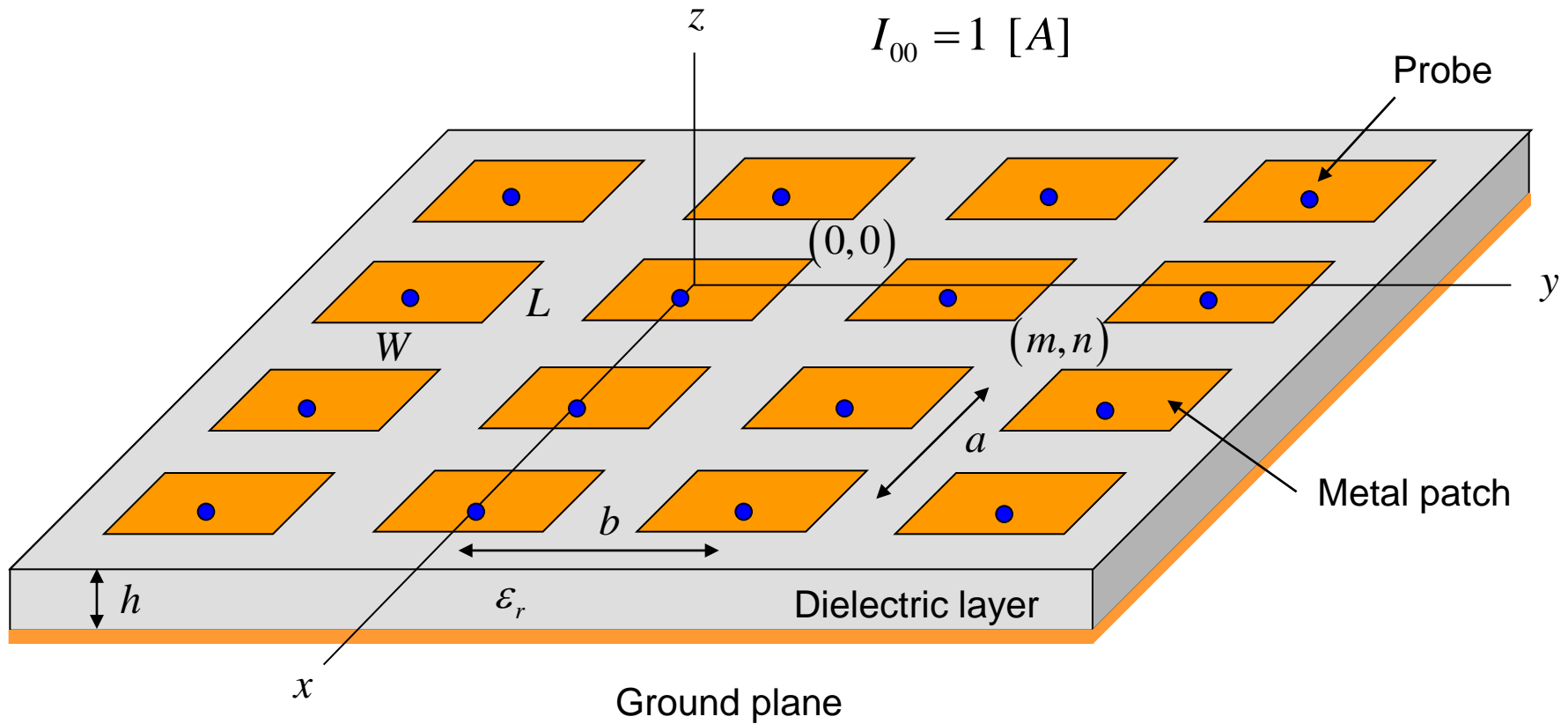
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Notes 34

Phased Array Geometry

$$I_{mn} = I_{00} e^{-j(k_{x0}ma + k_{y0}nb)} \quad (\text{probe currents})$$



Phased Array Analysis

Assume that the unknown current on the (0,0) patch is of the following form:

$$J_{sx}^{00}(x, y) = A_x^{00} B_x^{00}(x, y)$$

$$B_x^{00}(x, y) = \cos\left(\frac{\pi x}{L}\right), \quad |x| < L/2, \quad |y| < W/2$$

The EFIE (after Galerkin testing) is

$$A_x^{00} \int_{S_0} B_x^{00}(x, y) E_x^\infty [B_x^{00}] dS + \int_{S_0} B_x^{00}(x, y) E_x^\infty [J_z^i] dS = 0$$

Hence, we can write

$$A_x^{00} Z_{xx}^\infty + Z_{xz}^\infty = 0$$

The infinity superscript indicates the field from a periodic array of sources (patches or probes).

so

$$A_x^{00} = -\frac{Z_{xz}^\infty}{Z_{xx}^\infty}$$

Phased Array Analysis (cont.)

The “active” or “scan” input impedance is (following exactly the same procedure as done previously for the single patch):

$$\begin{aligned} Z_{in}^A &= Z_{probe} - A_x^{00} \left\langle B_x^\infty, J_z^i \right\rangle \\ &= Z_{probe} + A_x^{00} Z_{zx}^\infty \end{aligned}$$

This is the input impedance for a given patch when **all** patches are fed.

Hence we can write

$$Z_{in} = Z_{probe} - \frac{Z_{zx}^\infty Z_{xz}^\infty}{Z_{xx}^\infty}$$

Z_{zx}^∞ = field of infinite periodic patches, integrated over single probe.

Z_{xz}^∞ = field of infinite periodic probes, integrated over single patch.

Phased Array Analysis (cont.)

From reciprocity, it follows that

$$Z_{zx}^{\infty} = Z_{xz}^{\infty}$$

(though this is not obvious!)

LHS = field of periodic patches integrated over a single vertical probe.

RHS = field of periodic probes integrated over a single patch.

The proof is given on the next slide.

Phased Array Analysis (cont.)

To see this, consider the following:

$$\langle \mathbf{B}_x, \mathbf{J}_z^i \rangle = \langle \mathbf{J}_z^i, \mathbf{B}_x \rangle \quad (\text{single patch element})$$

Expressing the two reactions in the general form of spectral integrals, we have

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} F_1(k_x, k_y) e^{-j(k_x \Delta_x + k_y \Delta_y)} dk_x dk_y = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} F_2(k_x, k_y) e^{-j(k_x \Delta_x + k_y \Delta_y)} dk_x dk_y$$

where $(\Delta_x, \Delta_y) =$ arbitrary offset between elements

Since this holds for an arbitrary offset, we have

$$F_1(k_x, k_y) = F_2(k_x, k_y)$$

Phased Array Analysis (cont.)

Hence

$$\begin{aligned} \frac{(2\pi)^2}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} F_1(k_{xp}, k_{yq}) e^{-j(k_{xp}\Delta_x + k_{yq}\Delta_y)} \\ = \frac{(2\pi)^2}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} F_2(k_{xp}, k_{yq}) e^{-j(k_{xp}\Delta_x + k_{yq}\Delta_y)} \end{aligned}$$

so $\langle B_x^\infty, J_z^i \rangle = \langle J_z^{i\infty}, B_x \rangle$

or $Z_{zx}^\infty = Z_{xz}^\infty$

Phased Array Analysis (cont.)

The “active” or “scan” input impedance can thus be written as

$$Z_{in}^A = Z_{probe} - \frac{(Z_{zx}^\infty)^2}{Z_{xx}^\infty}$$

where

$$Z_{xx}^\infty = -\frac{1}{ab} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{G}_{xx}(k_{xp}, k_{yq}) \left[\tilde{B}_x^{00}(k_{xp}, k_{yq}) \right]^2$$

$$Z_{zx}^\infty = -\frac{1}{ab} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \frac{1}{j\omega\epsilon_1} (jk_{tpq}) (I_i^{TM}(-h)) \tilde{B}_x(k_{xp}, k_{yq}) \left(\frac{k_{xp}}{k_{tpq}} \right) h \operatorname{sinc}(k_{z1pq}h) e^{-j(k_{xp}x_0 + k_{yq}y_0)}$$

Phased Array Analysis (cont.)

At a scan blindness point:

$$Z_{zx}^{\infty} \rightarrow \infty$$

$$Z_{xx}^{\infty} \rightarrow \infty$$

$$Z_{in} = Z_{probe} - \frac{(Z_{zx}^{\infty})^2}{Z_{xx}^{\infty}}$$

so

$$Z_{in} \rightarrow \infty$$

Also,

$$A_x^{00} \rightarrow 0 \quad (\text{no current on the patches})$$

since
$$A_x^{00} = -\frac{Z_{xz}^{\infty}}{Z_{xx}^{\infty}}$$
 (The denominator has a stronger singularity than the numerator, since the patches radiate much more of a surface-wave field than do the probes.)

Phased Array Analysis (cont.)

From Waterhouse's short-course slides

