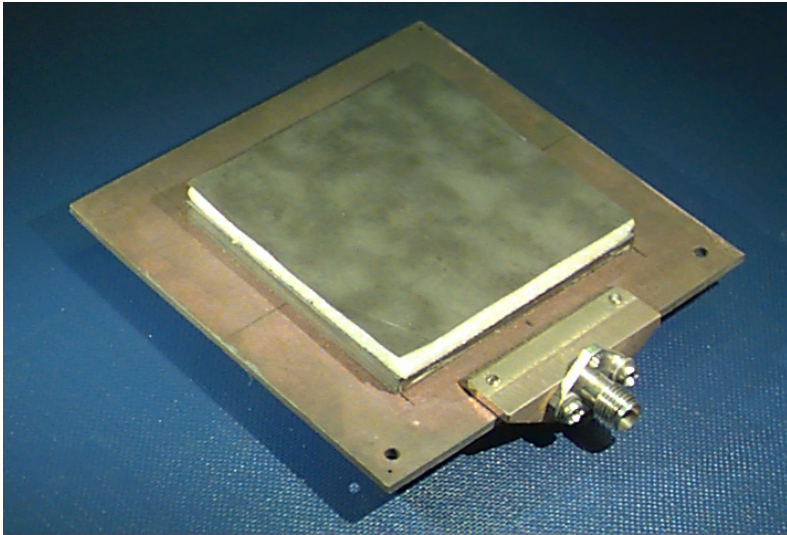


# ECE 6345

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Notes 9

# Overview

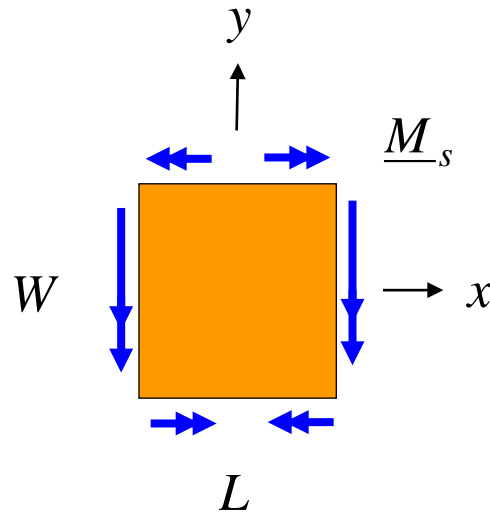
In this set of notes we calculate the far field of a rectangular patch using the magnetic current model.

The analysis assumes an infinite substrate, but for a truncated substrate we can use the same final result, setting the substrate permittivity to that of air (please see the discussion in Notes 6).

# Magnetic Current Model

Assume:

$$E_z^{1,0} = -\sin\left(\frac{\pi x}{L}\right)$$

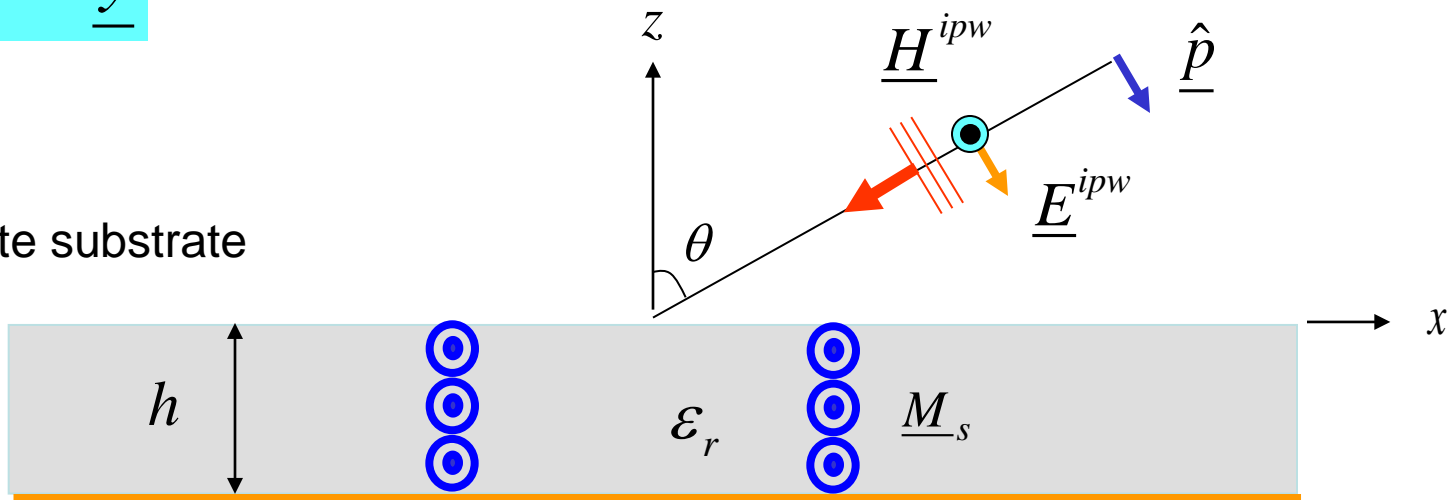


Only the radiating edges contribute to the E- and H-plane patterns, so we will ignore the non-radiating edges.

Radiating edges:

$$\underline{M}_s = -\hat{y}$$

Infinite substrate



# Magnetic Current Model (cont.)

$$\begin{aligned} E_p^{FF}(r, \theta, \phi) &= \langle a, b \rangle \\ &= \langle b, a \rangle \\ &= - \int_S \left( \underline{H}^{pw} \cdot \underline{M}_s^a \right) dS \\ &= - \int_S H_y^{pw} M_{sy}^a dS \end{aligned}$$

$$S = S_L + S_R \quad (\text{left+right edges})$$

$$M_{sy} = -1$$

# Magnetic Current Model (cont.)

TEN modeling equation:

$$H_y^{pw}(x, y, z) = \psi_t(x, y) I(z)$$

$$\psi_t(x, y) = e^{j(k_x x + k_y y)}$$

$$k_x = k_0 \sin \theta \cos \phi$$

$$k_y = k_0 \sin \theta \sin \phi$$

# Magnetic Current Model (cont.)

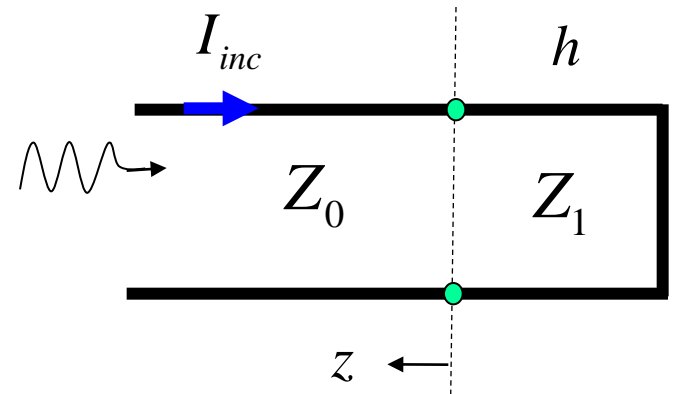
$$\begin{aligned}
 H_y^{pw}(x, y, z) &= \psi_t(x, y) I(z) \\
 &= \psi_t(x, y) I(0) \left[ \frac{\cos(k_{z1}(z+h))}{\cos(k_{z1}h)} \right] \\
 &= H_y^{pw}(x, y, 0) \left[ \frac{\cos(k_{z1}(z+h))}{\cos(k_{z1}h)} \right]
 \end{aligned}$$

Also,

$$H_y^{pw}(x, y, 0) = H_y^{ipw}(x, y, 0)(1 - \Gamma^{TM/TE})$$

$$TM_z : \underline{\hat{p}} = \underline{\hat{\theta}}$$

$$TE_z : \underline{\hat{p}} = \underline{\hat{\phi}}$$



# Magnetic Current Model (cont.)

$$\underline{\hat{p}} = \underline{\hat{\theta}} :$$

$$\underline{H}^{ipw} = -\underline{\hat{\phi}} \frac{E_{\theta}^{ipw}}{\eta_0} = -\underline{\hat{\phi}} \left( \frac{E_0}{\eta_0} \right) \psi(x, y, z) = -\underline{\hat{\phi}} \left( \frac{E_0}{\eta_0} \right) \psi_t(x, y) e^{jk_z z}$$

$$H_y^{ipw}(x, y, 0) = \left( \frac{E_0}{\eta_0} \right) (-\cos \phi) \psi_t(x, y)$$

$$\underline{\hat{p}} = \underline{\hat{\phi}} :$$

$$\underline{H}^{ipw} = \underline{\hat{\theta}} \frac{E_{\phi}^{ipw}}{\eta_0} = \underline{\hat{\theta}} \left( \frac{E_0}{\eta_0} \right) \psi(x, y, z) = \underline{\hat{\theta}} \left( \frac{E_0}{\eta_0} \right) \psi_t(x, y) e^{jk_z z}$$

$$H_y^{ipw}(x, y, 0) = \left( \frac{E_0}{\eta_0} \right) (\cos \theta \sin \phi) \psi_t(x, y)$$

# Magnetic Current Model (cont.)

Therefore we have

$$H_y^{pw}(x, y, z) = e^{j(k_x x + k_y y)} I^+ (1 - \Gamma^{TM/TE}) \sec(k_{z1} h) \cos k_{z1} (z + h)$$

where

$$I^+ = \left( \frac{E_0}{\eta_0} \right) (-\cos \phi), E_\theta (TM_z)$$

$$I^+ = \left( \frac{E_0}{\eta_0} \right) (\cos \theta \sin \phi), E_\phi (TE_z)$$

We can thus now consider

$$E_p^{FF}(r, \theta, \phi) = - \int_{S_L + S_R} H_y^{pw}(x, y, z) (-1) dS$$

$M_{sy} = -1$   
↙



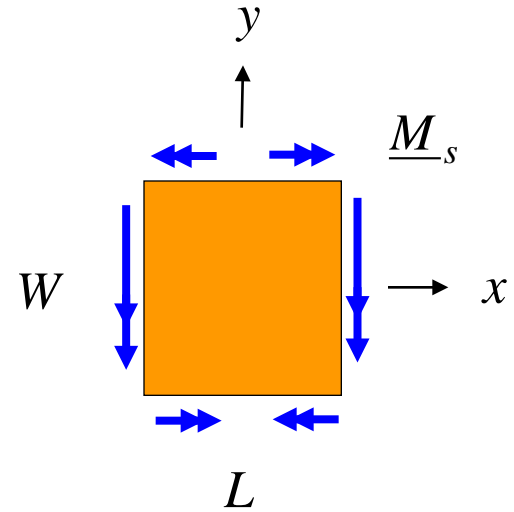
# Magnetic Current Model (cont.)

Consider  $S_R$  :

$$x = \frac{L}{2}$$

$$y \in \left( -\frac{W}{2}, \frac{W}{2} \right)$$

$$z \in (-h, 0)$$



Therefore we have

$$E_p^{right}(r, \theta, \phi) = \int_{-h}^0 \int_{-\frac{W}{2}}^{\frac{W}{2}} e^{j\left(k_x \frac{L}{2}\right)} e^{jk_y y} I^+ \left(1 - \Gamma^{TM/TE}\right) \sec(k_{z1} h) \cos k_{z1} (z + h) dy dz$$

# Magnetic Current Model (cont.)

$$E_p^{right}(r, \theta, \phi) = I^+ (1 - \Gamma) \sec(k_{z1} h) e^{j\left(k_x \frac{L}{2}\right)} \underbrace{\int_{-\frac{W}{2}}^{+\frac{W}{2}} e^{jk_y y} dy}_{\text{integral1}} \underbrace{\int_{-h}^0 \cos k_{z1} (z + h) dz}_{\text{integral2}}$$

Integral 1:  $W \operatorname{sinc}\left(\frac{k_y W}{2}\right)$

Integral 2:  $h \operatorname{sinc}(k_{z1} h)$

Hence we have

$$E_p^{right}(r, \theta, \phi) = I^+ (1 - \Gamma^{TM/TE}) e^{jk_x \frac{L}{2}} (Wh) \operatorname{sinc}\left(\frac{k_y W}{2}\right) \operatorname{tanc}(k_{z1} h)$$

where  $\operatorname{tanc}(x) \equiv \frac{\tan x}{x}$

# Magnetic Current Model (cont.)

For  $S_L$ : Replace  $\frac{L}{2} \rightarrow -\frac{L}{2}$

For  $S_L + S_R$ :  $e^{jk_x \frac{L}{2}} + e^{-jk_x \frac{L}{2}}$

which yields  $2 \cos\left(k_x \frac{L}{2}\right)$

Hence we have

$$E_p^{FF}(r, \theta, \phi) = I^+ (1 - \Gamma^{TM/TE}) 2 \cos\left(k_x \frac{L}{2}\right) (Wh) \text{sinc}\left(k_y \frac{W}{2}\right) \text{tanc}(k_{z1} h)$$

# Magnetic Current Model (cont.)

Substituting for  $I^+$  in the  $TM_z$  and  $TE_z$  cases, we have

$$E_{\theta}^{FF}(r, \theta, \phi) = -2Wh \left( \frac{E_0}{\eta_0} \right) \cos \phi (1 - \Gamma^{TM}(\theta)) \cos \left( k_x \frac{L}{2} \right) \text{sinc} \left( k_y \frac{W}{2} \right) \text{tanc}(k_{z1}h)$$

$$E_{\phi}^{FF}(r, \theta, \phi) = 2Wh \left( \frac{E_0}{\eta_0} \right) (\cos \theta \sin \phi) (1 - \Gamma^{TE}(\theta)) \cos \left( k_x \frac{L}{2} \right) \text{sinc} \left( k_y \frac{W}{2} \right) \text{tanc}(k_{z1}h)$$

$$E_0 = \left( \frac{-j\omega\mu_0}{4\pi r} \right) e^{-jk_0 r} \quad \begin{aligned} k_x &= k_0 \sin \theta \cos \phi \\ k_y &= k_0 \sin \theta \sin \phi \end{aligned}$$

# Magnetic Current Model (cont.)

Examine the reflection coefficient term:

$$1 - \Gamma = 1 - \left( \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \right) \\ = \frac{2Z_0}{Z_{in} + Z_0}$$

$$\Gamma = \Gamma^{TM} \quad \text{for} \quad \underline{\hat{p}} = \underline{\hat{\theta}}$$

$$\Gamma = \Gamma^{TE} \quad \text{for} \quad \underline{\hat{p}} = \underline{\hat{\phi}}$$

$$Z_{in}^{TM/TE} = jZ_1^{TM/TE} \tan(k_{z1}h) \\ = jZ_1^{TM/TE} \tan(k_0 N_1(\theta)h)$$

$$Z_1^{TM} = \frac{\eta_0}{\epsilon_r} N_1(\theta)$$

$$Z_1^{TE} = \frac{\eta_0 \mu_r}{N_1(\theta)}$$

$$Z_0^{TM} = \eta_0 \cos \theta$$

$$Z_0^{TE} = \frac{\eta_0}{\cos \theta}$$

# Magnetic Current Model (cont.)

Substituting in for the impedances and simplifying the results, we have

$$1 - \Gamma^{TM}(\theta) = \frac{2}{1 + j \left( \frac{N_1(\theta) \sec \theta}{\epsilon_r} \right) \tan(k_0 h N_1(\theta))}$$

$$1 - \Gamma^{TE}(\theta) = \frac{2}{1 + j \left( \frac{\mu_r \cos \theta}{N_1(\theta)} \right) \tan(k_0 h N_1(\theta))}$$