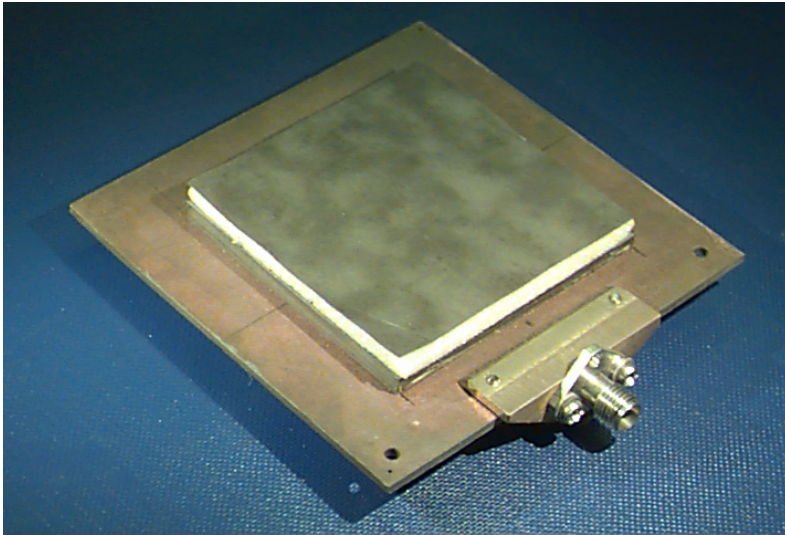


# ECE 6345

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Notes 16

# Overview

In this set of notes we calculate the power radiated into space by the circular patch.

This will lead to  $Q_{sp}$  of the circular patch.

# Radiated Power of Circular Patch

Assumption:

$$E_z(a, \phi) = \cos \phi$$

From Notes 10 we have:

$$E_{\theta}^{FF}(r, \theta, \phi) = \frac{E_0}{\eta_0} (ah) \cos \phi \operatorname{tanc}(k_{z1} h) Q(\theta) 2\pi J_1'(k_0 a \sin \theta)$$

$$E_{\phi}^{FF}(r, \theta, \phi) = -\frac{E_0}{\eta_0} (ah) \sin \phi \operatorname{tanc}(k_{z1} h) P(\theta) 2\pi J_{inc}(k_0 a \sin \theta)$$

where

$$Q(\theta) = 1 - \Gamma^{TM}(\theta)$$

$$P(\theta) \equiv \cos \theta (1 - \Gamma^{TE}(\theta))$$

$$J_{inc}(x) \equiv \frac{J_1(x)}{x}$$

# Radiated Power of Circular Patch (cont.)

The power density in the far field from the Poynting vector is

$$\begin{aligned} S_r(r, \theta, \phi) &= \frac{1}{2\eta_0} \left[ |E_\theta|^2 + |E_\phi|^2 \right] \\ &= \frac{1}{2\eta_0} \frac{|E_0|^2}{\eta_0^2} (ah)^2 \text{tanc}^2(k_{z1}h) (2\pi)^2 \\ &\quad \cdot \left[ \cos^2 \phi J_1'^2(k_0 a \sin \theta) |Q(\theta)|^2 + \sin^2 \phi J_{inc}^2(k_0 a \sin \theta) |P(\theta)|^2 \right] \end{aligned}$$

Next, use  $|E_0| = \frac{\omega \mu_0}{4\pi r} = \frac{k_0 \eta_0}{4\pi r}$

# Radiated Power of Circular Patch (cont.)

We then have

$$S_r(r, \theta, \phi) = \frac{1}{8\eta_0} (k_0 a)^2 h^2 \operatorname{tanc}^2(k_{z1} h) \cdot \left[ \cos^2 \phi |Q(\theta)|^2 J_1'^2(k_0 a \sin \theta) + \sin^2 \phi |P(\theta)|^2 J_{inc}^2(k_0 a \sin \theta) \right] \frac{1}{r^2}$$

The space-wave power is

$$P_{sp} = \int_0^{2\pi} \int_0^{\pi/2} S_r(r, \theta, \phi) r^2 \sin \theta d\theta d\phi$$

Performing the  $\phi$  integrals,

$$P_{sp} = \pi \frac{1}{8\eta_0} (k_0 a)^2 h^2 \cdot \int_0^{\pi/2} \operatorname{tanc}^2(k_{z1} h) \sin \theta \left[ |Q(\theta)|^2 J_1'^2(k_0 a \sin \theta) + |P(\theta)|^2 J_{inc}^2(k_0 a \sin \theta) \right] d\theta$$

# Radiated Power of Circular Patch (cont.)

Define

$$I_c = \int_0^{\pi/2} C(\theta) d\theta$$

where

$$C(\theta) = \sin \theta \operatorname{tanc}^2(k_{z1} h) \left[ |Q(\theta)|^2 J_1'^2(k_0 a \sin \theta) + |P(\theta)|^2 J_{inc}^2(k_0 a \sin \theta) \right]$$

We then have

$$P_{sp} = \frac{\pi}{8\eta_0} (k_0 a)^2 h^2 I_c$$

Note: We will get a CAD formula for  $I_c$  later.

# Calculation of $Q_{sp}$

The  $Q$  formula is  $Q_{sp} = \omega_0 \left( \frac{U_S}{P_{sp}} \right)$

$$\begin{aligned} U_S &= 2U_E \\ &= 2 \int_V \frac{1}{4} \epsilon_0 \epsilon_r |E_z|^2 dV \\ &= \frac{1}{2} \epsilon_0 \epsilon_r h \int_S |E_z|^2 dS \\ &= \frac{1}{2} \epsilon_0 \epsilon_r h \int_0^{2\pi} \int_0^a |E_z|^2 \rho d\rho d\phi \\ &= \pi \frac{1}{2} \epsilon_0 \epsilon_r h \int_0^a |E_z|^2 \rho d\rho \end{aligned}$$

The electric field is

$$E_z(\rho, \phi) = \cos \phi \left[ \frac{J_1(k\rho)}{J_1(ka)} \right]$$

Note:

$$E_z(a, \phi) = \cos \phi$$

# Calculation of $Q_{sp}$ (cont.)

The stored energy is then

$$U_s = \frac{1}{2} \varepsilon_0 \varepsilon_r h \pi \frac{1}{J_1^2(ka)} \int_0^a J_1^2(k\rho) \rho d\rho$$

Denote

$$\begin{aligned} I_1 &= \int_0^a J_1^2(k\rho) \rho d\rho = \left[ \frac{1}{2} \rho^2 J_1'^2(k\rho) + \frac{1}{2} \rho^2 \left( 1 - \frac{1}{(k\rho)^2} \right) J_1^2(k\rho) \right]_0^a \\ &= \frac{a^2}{2} \left[ J_1'^2(ka) + \left( 1 - \frac{1}{(ka)^2} \right) J_1^2(ka) \right] \end{aligned}$$



# Calculation of $Q_{sp}$ (cont.)

Recall that  $k = \frac{x'_{11}}{a}$       $x'_{11} = 1.84118$

so  $J'_1(ka) = J'_1(x'_{11}) = 0$

Hence  $I_1 = \frac{a^2}{2} \left( 1 - \frac{1}{x'^2_{11}} \right) J_1^2(x'_{11})$

We then have

$$U_S = \frac{1}{2} \varepsilon_0 \varepsilon_r h \pi \left( \frac{1}{J_1^2(x'_{11})} \right) \left[ \left( \frac{a^2}{2} \right) \left( 1 - \frac{1}{x'^2_{11}} \right) J_1^2(x'_{11}) \right]$$

or  $U_S = \frac{1}{2} \varepsilon_0 \varepsilon_r h \pi \left[ \left( \frac{a^2}{2} \right) \left( 1 - \frac{1}{x'^2_{11}} \right) \right]$

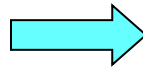
# Calculation of $Q_{sp}$ (cont.)

The formula for  $Q_{sp}$  then becomes

$$Q_{sp} = \omega_0 \left( \frac{\frac{1}{2} \varepsilon_0 \varepsilon_r h \pi \left( \frac{a^2}{2} \right) \left( 1 - \frac{1}{x'_{11}{}^2} \right)}{\frac{\pi}{8 \eta_0} (k_0 a)^2 h^2 I_c} \right)$$

This may be simplified by using the following expressions to eliminate  $\omega_0$  and  $k_0$ :

$$\begin{aligned} k_0 \sqrt{\mu_r \varepsilon_r} a &= x'_{11} \\ \omega_0 \sqrt{\mu_0 \varepsilon_0} \sqrt{\mu_r \varepsilon_r} a &= x'_{11} \end{aligned}$$



$$\begin{aligned} k_0 a &= \frac{x'_{11}}{\sqrt{\mu_r \varepsilon_r}} \\ \omega_0 &= \frac{x'_{11}}{a \sqrt{\mu_0 \varepsilon_0} \sqrt{\mu_r \varepsilon_r}} \end{aligned}$$

# Calculation of $Q_{sp}$ (cont.)

We then have

$$Q_{sp} = \frac{2}{x'_{11}} (x'_{11}{}^2 - 1) \left( \frac{1}{k_0 h} \right) \epsilon_r \left[ \frac{1}{I_c} \right]$$

Note that  $Q_{sp}$  is proportional to the substrate permittivity and inversely proportional to the substrate thickness.

# Calculation of $Q_{sp}$ (cont.)

Summary (exact  $Q_{sp}$ )

$$Q_{sp} = 2 \frac{1}{x'_{11}} (x'_{11}{}^2 - 1) \left( \frac{1}{I_c} \right) \left( \frac{1}{k_0 h} \right) \varepsilon_r$$

$$I_c \equiv \int_0^{\pi/2} C(\theta) d\theta$$

$$x'_{11} = 1.84118$$

$$C(\theta) = \sin \theta \operatorname{tanc}^2(k_{z1} h) \left[ |Q(\theta)|^2 J_1'^2(k_0 a \sin \theta) + |P(\theta)|^2 J_{inc}^2(k_0 a \sin \theta) \right]$$

# The $p$ Factor

We can express the  $Q_{sp}$  formula in terms of a  $p$  factor (which will eventually be approximated in closed form).

Define:

$$C_0(\theta) \equiv C(\theta) \Big|_{a \rightarrow 0}$$

$$I_0 \equiv \int_0^{\pi/2} C_0(\theta) d\theta$$

The term  $C_0$  ignores the patch array factor.

Also, define:

$$p \equiv \frac{I_c}{I_0} = \frac{\int_0^{\pi/2} C(\theta) d\theta}{\int_0^{\pi/2} C_0(\theta) d\theta}$$

The  $p$  term gives the ratio of the power radiated by the actual patch to the power radiated if we ignore the array factor, and collapse the magnetic current down to a single dipole.

(See the end of the notes for a derivation of the equivalent dipole moment of the circular patch.)

# The $p$ Factor (cont.)

Then we have

$$Q_{sp} = 2 \frac{1}{x_{11}'^2} (x_{11}'^2 - 1) \left( \frac{1}{p} \right) \left( \frac{1}{I_0} \right) \left( \frac{1}{k_0 h} \right) \varepsilon_r$$

Note that as  $x \rightarrow 0$

$$J_1'(x) \rightarrow \frac{1}{2}$$

$$J_{inc}(x) \rightarrow \frac{1}{2}$$

This allows us to express  $I_0$  in a simpler form without the Bessel functions:

$$I_0 = \int_0^{\pi/2} \sin \theta \operatorname{tanc}^2(k_0 h N_1(\theta)) \frac{1}{4} \left[ |P(\theta)|^2 + |Q(\theta)|^2 \right] d\theta$$

# The $p$ Factor (cont.)

For the  $p$  factor we have:

$$p = \frac{\int_0^{\pi/2} \sin \theta \operatorname{tanc}^2(k_0 h N_1(\theta)) \left[ |Q(\theta)|^2 J_1'^2(k_0 a \sin \theta) + |P(\theta)|^2 J_{inc}^2(k_0 a \sin \theta) \right] d\theta}{\int_0^{\pi/2} \sin \theta \operatorname{tanc}^2(k_0 h N_1(\theta)) \frac{1}{4} \left[ |P(\theta)|^2 + |Q(\theta)|^2 \right] d\theta}$$

The term  $p$  depends on the patch radius  $a$  and the substrate parameters.  
(After making some approximations, it will depend only on the patch radius.)

# Approximation for a Thin Substrate

For a thin substrate, we have:

$$\text{tanc}^2(k_0 h N_1(\theta)) \approx 1$$

so

$$I_0 \approx \int_0^{\pi/2} \sin \theta \frac{1}{4} \left[ |P(\theta)|^2 + |Q(\theta)|^2 \right] d\theta$$

$$p \approx \frac{\int_0^{\pi/2} \sin \theta \left[ |Q(\theta)|^2 J_1'^2(k_0 a \sin \theta) + |P(\theta)|^2 J_{inc}^2(k_0 a \sin \theta) \right] d\theta}{\int_0^{\pi/2} \sin \theta \frac{1}{4} \left[ |P(\theta)|^2 + |Q(\theta)|^2 \right] d\theta}$$



# Approximation for a Thin Substrate (cont.)

From Notes 9 we also have

$$P(\theta) = \cos \theta (1 - \Gamma^{TE}(\theta)) = \frac{2 \cos \theta}{1 + j \left( \frac{\mu_r \cos \theta}{N_1(\theta)} \right) \tan(k_0 h N_1(\theta))}$$

$$Q(\theta) = 1 - \Gamma^{TM}(\theta) = \frac{2}{1 + j \left( \frac{N_1(\theta) \sec \theta}{\epsilon_r} \right) \tan(k_0 h N_1(\theta))}$$

For a thin substrate we then have

$$P(\theta) \approx 2 \cos \theta$$

$$Q(\theta) \approx 2$$

# Approximation for a Thin Substrate (cont.)

For the  $I_0$  term (the denominator of the  $p$  function) we then have:

$$\begin{aligned} I_0 &\approx \int_0^{\pi/2} \frac{1}{4} \sin \theta \left[ 4(\cos^2 \theta + 1) \right] d\theta \\ &= \int_0^{\pi/2} \sin \theta (\cos^2 \theta + 1) d\theta \end{aligned}$$

This yields

$$I_0 \approx \frac{4}{3}$$

# Approximation for a Thin Substrate (cont.)

The formula for the  $p$  function then becomes

$$p \approx \frac{3}{4} \int_0^{\pi/2} \sin \theta \left[ |2|^2 J_1'^2(k_0 a \sin \theta) + |2 \cos \theta|^2 J_{inc}^2(k_0 a \sin \theta) \right] d\theta$$

so that

$$p \approx 3 \int_0^{\pi/2} \sin \theta \left[ J_1'^2(k_0 a \sin \theta) + \cos^2 \theta J_{inc}^2(k_0 a \sin \theta) \right] d\theta$$

The  $p$  factor now only depends only on the patch size.

# Approximation for a Thin Substrate (cont.)

Summary (approximate  $Q_{sp}$ )

$$Q_{sp} = 2 \frac{1}{x'_{11}} (x'_{11}{}^2 - 1) \left( \frac{1}{p} \right) \left( \frac{1}{I_0} \right) \left( \frac{1}{k_0 h} \right) \epsilon_r$$

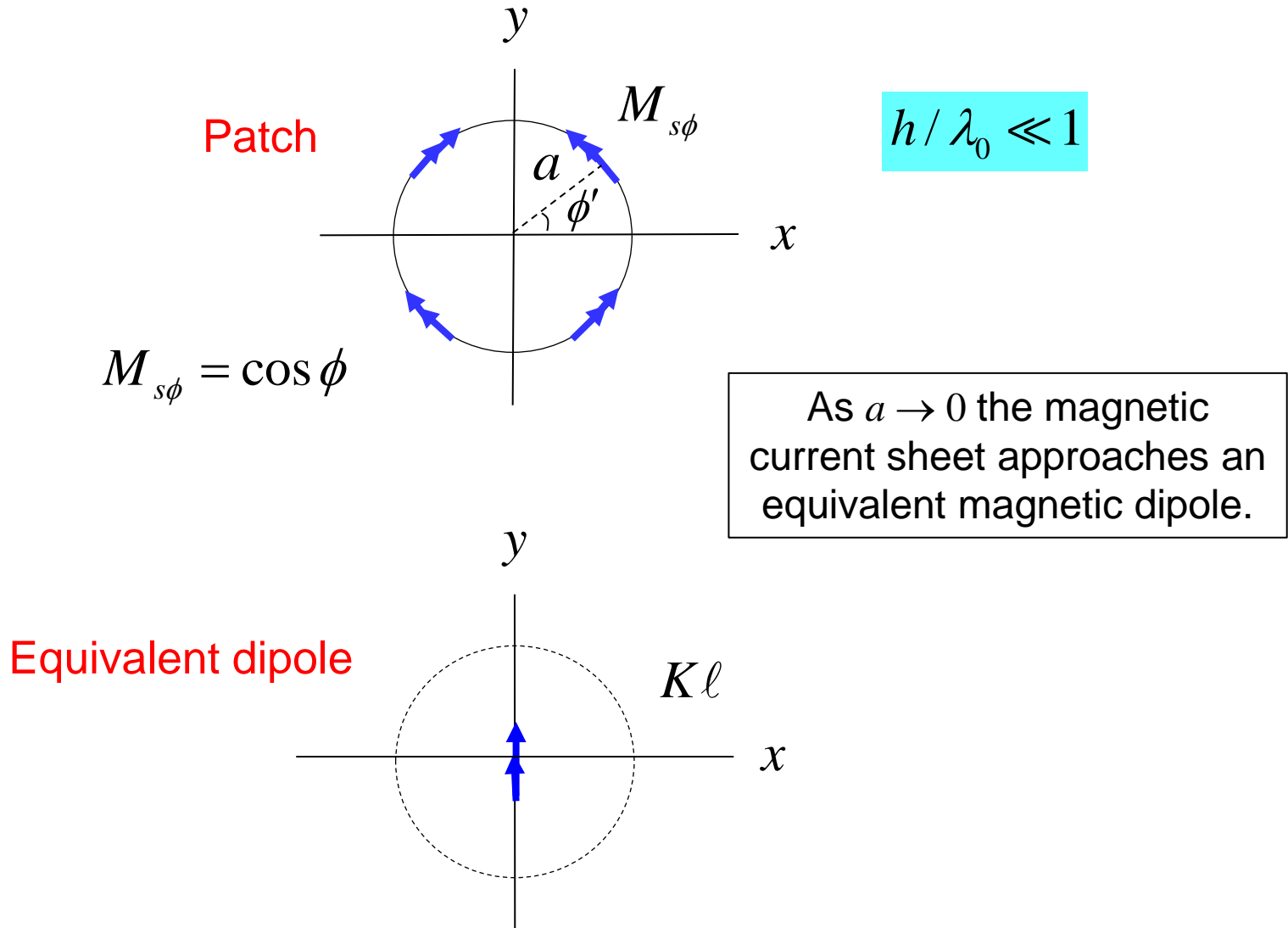
$$x'_{11} = 1.84118$$

$$I_0 \approx \frac{4}{3}$$

$$p \approx 3 \int_0^{\pi/2} \sin \theta \left[ J_1'^2(k_0 a \sin \theta) + \cos^2 \theta J_{inc}^2(k_0 a \sin \theta) \right] d\theta$$

# Equivalent Dipole Moment of Circular Patch

Consider an equivalent magnetic dipole that models the patch:



# Equivalent Dipole Moment of Circular Patch (cont.)

The dipole moment of the equivalent magnetic dipole is calculated:

$$Kl = \int_S \underline{M}_s \cdot \underline{\hat{y}} dS = h \int_0^{2\pi} M_{s\phi} \cos \phi a d\phi = h \int_0^{2\pi} \cos \phi \cos \phi a d\phi =$$
$$ha \int_0^{2\pi} \cos^2 \phi a d\phi$$

This yields  $Kl = \pi ah$

# Equivalent Dipole Moment of Circular Patch (cont.)

We can therefore physically interpret the  $p$  factor as follows:

$$p = \frac{P_{rad}^{patch}}{P_{rad}^{dip}}$$

where

$P_{rad}^{patch}$  = power radiated by circular patch

$P_{rad}^{dip}$  = power radiated by magnetic dipole of equal moment

$$( Kl = \pi ah )$$

# CAD Formula for $p$

In the next set of notes we will obtain approximate closed-form CAD expression for  $p$ .