# **ECE 3317**Applied Electromagnetic Waves

#### **Final Exam**

Dec. 7, 2023


#### **General Information:**

The exam is open-book and open-notes. You are not allowed to use any device that has communication functionality (laptop, cell phone, ipad, etc.).

#### Instructions:

- Show all of your work. No credit will be given if the work required to obtain the solutions is not shown.
- Write neatly. You will not be given credit for work that is not easily legible.
- Leave answers in terms of the parameters given in the problem.
- Show units in all of your final answers.
- Circle your final answers.
- Double-check your answers. For simpler problems, partial credit may not be given.
- If you have any questions, ask the instructor. You will not be given credit for work that is based on a wrong assumption.
- Make sure you sign the academic honesty statement below.

# **Academic Honesty Statement**

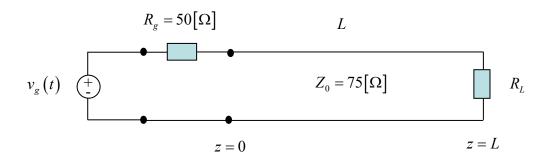
By tak	ing this	exam,	you agr	ee to a	bide	by th	ne UH	Acade	mic	Honesty	/ Poli	cy dur	ing t	his
exam.	You u	ndersta	nd and	agree	that	the	punish	ment f	for v	riolating	this	policy	will	be
most s	severe,	includin	g gettin	g an F	in the	e cla	ss and	getting	g ex	pelled fr	om th	ne Uni	versi	ity.

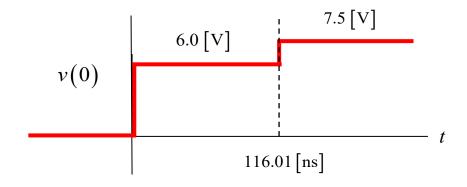
Signature:	

# Problem 1 (25 pts)

A TDR (time-domain reflectometer) has a generator voltage  $v_g(t)$  that is a step function with an amplitude of  $V_0$  volts. The TDR has a 50  $[\Omega]$  Thévenin impedance. The TDR is connected to a transmission line with a characteristic impedance of 75  $[\Omega]$ . At the end of the line there is a load  $R_L$ . The transmission line is a coax that has a Teflon filling (with a relative permittivity of 2.1). The TDR records the total voltage v(0) at z = 0, and this is shown in the plot below.

- (a) What is the length of the line *L* in meters?
- (b) What is the amplitude  $V_0$  of the step function  $v_g(t)$ ?
- (c) What is the load resistance  $R_L$ ?





# Part (a)

The speed of the signal is the velocity of light in the dielectric. We have

$$c_d = \frac{c}{\sqrt{\varepsilon_r}} = 2.06876 \times 10^8 [\text{m/s}].$$

The length of the line is related to the time  $t_d$  that the change in the voltage is recorded by the TDR.

$$2L = c_d t_d$$
.

Solving for L we have

$$L = 12.000 [m]$$
.

# Part (b)

From the voltage divider equation we have

$$V^+ = V_0 \left( \frac{Z_0}{R_g + Z_0} \right).$$

Hence,

$$6.0 = V_0 \left( \frac{75}{50 + 75} \right).$$

This gives us

$$V_0 = 10 [V].$$

# Part (c)

We have

$$V^+ \left( 1 + \Gamma_L + \Gamma_L \Gamma_g \right) = 7.5 \left[ V \right].$$

Hence, we have

$$6.0(1+\Gamma_L+\Gamma_L(-0.2))=7.5[V]$$

or

$$6.0(1+\Gamma_L(0.8))=7.5[V]$$

or

$$\Gamma_L = 0.3125.$$

We also have

$$\Gamma_L = \frac{R_L - Z_0}{R_L + Z_0} = \frac{R_L - 75}{R_L + 75} \,.$$

Hence,

$$\frac{R_L - 75}{R_L + 75} = 0.3125.$$

This gives us

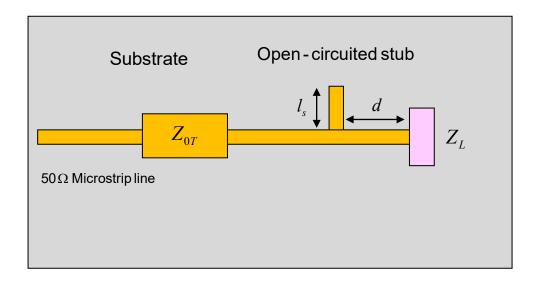
$$R_L = 143.18 \left[\Omega\right].$$

# Problem 2 (25 pts)

A device (load) on a printed circuit board has an input impedance of  $Z_L = 100 + j50$  [ $\Omega$ ]. We want to match the load to an incoming 50 [ $\Omega$ ] microstrip feed line. To do this we put an open-circuited stub in parallel with the main feed line at a distance  $d = 0.15\lambda_g$  from the load. The stub has a length of  $l_s$  and also has a characteristic impedance of 50 [ $\Omega$ ]. A quarter-wave transformer is then placed at a distance of  $\lambda_g / 2$  from the stub.

The frequency is 5 [GHz] and the relative effective permittivity of the microstrip lines is 1.75.

- a) What is the normalized input admittance just to the right of the stub? Use the <u>first</u> Smith chart on the next pages.
- b) Design the stub length  $l_s$  in terms of  $\lambda_g$ . Use the <u>second</u> Smith chart on the next pages.
- c) Find the value of  $\lambda_g$  in mm.
- d) Find value of the transformer characteristic impedance  $Z_{0T}$ .



# Part (a)

From the first Smith chart we have

$$Y_{in}^{N} = 0.65 + j(0.65).$$

# Part (b)

From the second Smith chart we have

$$l_s = 0.408 \lambda_g.$$

# Part (c)

We have

$$\lambda_g = rac{\lambda_0}{\sqrt{{\cal E}_r^{
m eff}}} \, .$$

This gives us

$$\lambda_g = 45.324 \, [\text{mm}]$$
.

# Part (d)

At a point just to the right of the stub, the normalized input admittance (from the first smith chart) is 0.65. The normalized impedance is then 1 / 0.65 = 1.54. Unnormalized, this corresponds to  $76.9 [\Omega]$ .

7

We the have

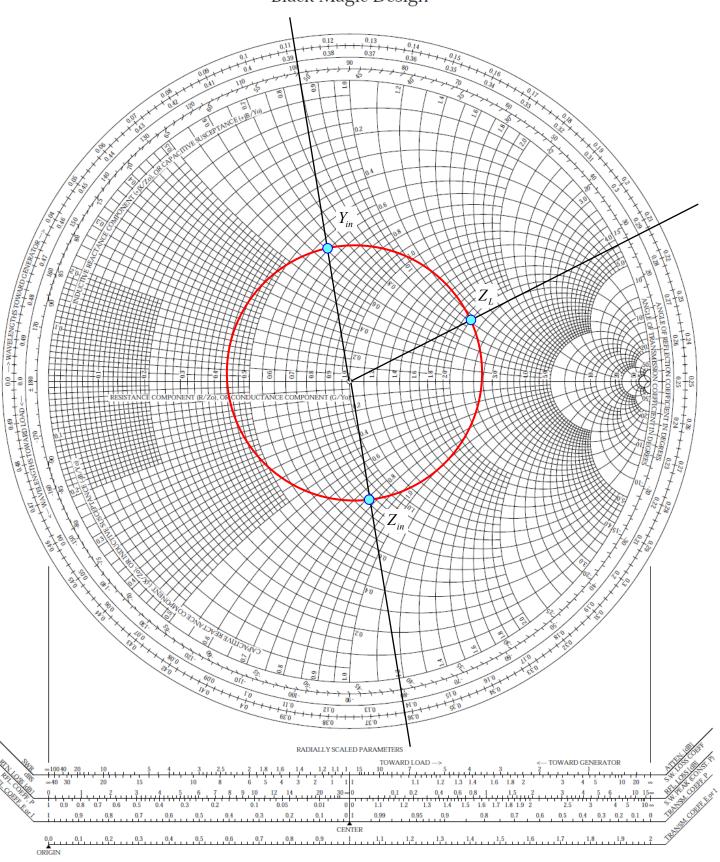
$$Z_{0T} = \sqrt{(50)(76.9)}$$
.

Hence,

$$Z_{\rm OT} = 62.0 \left[ \Omega \right].$$

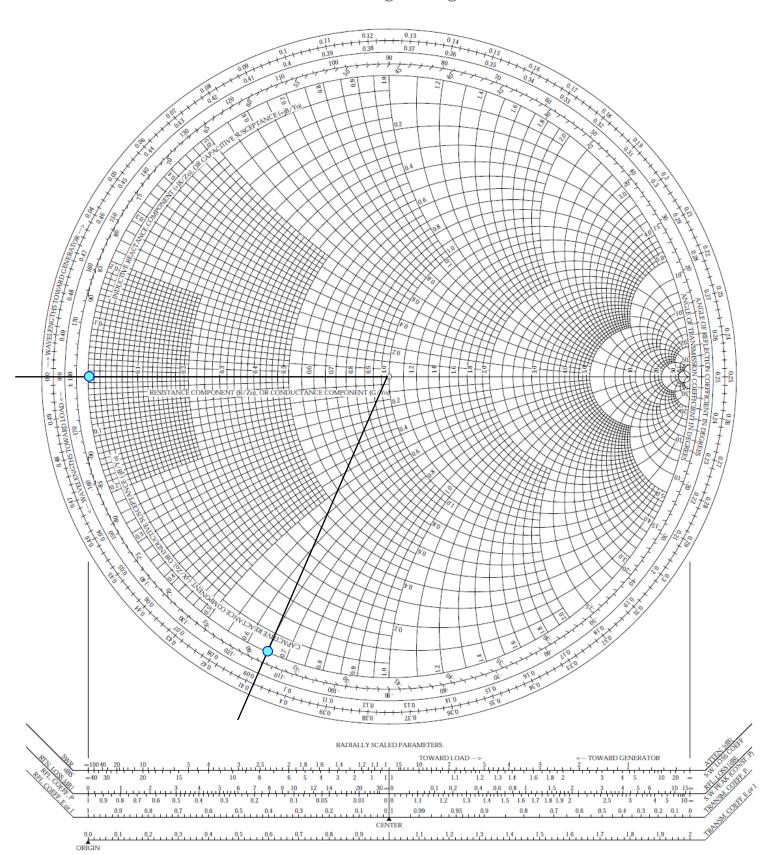
# The Complete Smith Chart

Black Magic Design



# The Complete Smith Chart

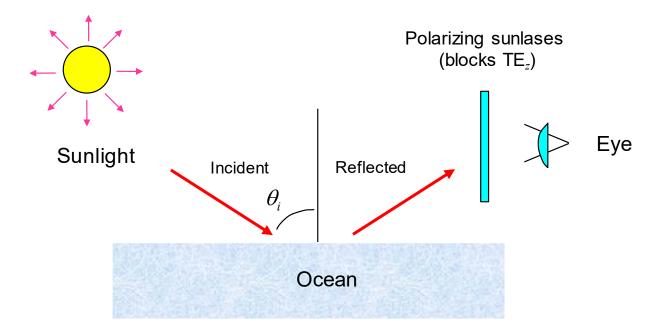
Black Magic Design



# Problem 3 (25 pts)

Sunlight is incident on the ocean, which at optical frequencies is assumed to be lossless (and nonmagnetic) with a relative permittivity of 1.7689. The sunlight is randomly polarized, so that it has equal power densities in the  $TM_z$  and  $TE_z$  parts. The incident angle  $\theta_i$  is 60°. The sunlight reflects off of the ocean and then goes through polarizing sunglasses to reach a person's eyes. The polarizing sunglasses allow the  $TM_z$  polarization to go through, but they block the  $TE_z$  polarization.

Find the percentage of the incident power density that makes it through the sunglasses, after reflecting off the ocean.



#### Part (a)

The transmitted angle is, from Snell's law,

$$\theta_t = 0.70909 \text{ [radians]} = 40.628^{\circ}.$$

Only the TM reflected wave makes it thought the sunglasses. Therefore, the percent power that makes it through the sunglasses is (assuming the incident power density is  $1.0 \, [W/m^2]$ )

$$P_r^{\%} = 100 \left( \frac{1}{2} |\Gamma_{\text{TM}}|^2 \right).$$

We have

$$\Gamma_{\text{TM}} = \frac{Z_2^{\text{TM}} - Z_1^{\text{TM}}}{Z_2^{\text{TM}} + Z_1^{\text{TM}}}$$

$$Z_{1}^{\text{TM}} = \frac{k_{z1}}{\omega \varepsilon_{1}} = \frac{k_{1} \cos \theta_{i}}{\omega \varepsilon_{0}} = \frac{k_{0} \cos \theta_{i}}{\omega \varepsilon_{0}} = \eta_{0} \cos \theta_{i} = (376.7303) \cos(60^{\circ}) = 188.37 \left[\Omega\right]$$

$$Z_{2}^{\mathrm{TM}} = \frac{k_{z2}}{\omega \varepsilon_{2}} = \frac{k_{2} \cos \theta_{t}}{\omega \varepsilon_{0} \varepsilon_{r}} = \frac{k_{0} \sqrt{\varepsilon_{r}} \cos \theta_{t}}{\omega \varepsilon_{0} \varepsilon_{r}} = \frac{\eta_{0}}{\sqrt{\varepsilon_{r}}} \cos \theta_{t} = \left(\frac{376.7303}{\sqrt{1.7689}}\right) \cos \left(40.628^{\circ}\right) = 215.00 \left[\Omega\right].$$

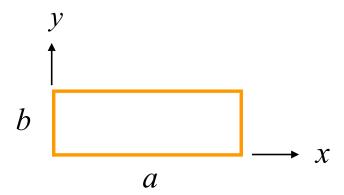
This gives us

$$\Gamma_{\text{TM}} = \frac{Z_2^{\text{TM}} - Z_1^{\text{TM}}}{Z_2^{\text{TM}} + Z_1^{\text{TM}}} = \frac{26.630}{403.37} = 0.0660$$

$$P_r^{\%} = 0.217$$
.

# Problem 4 (25 pts)

- a) Design the dimensions a and b of an air-filled rectangular waveguide that is to be used for transmission of electromagnetic power at 6.0 [GHz]. This frequency should be at the center of the operating frequency band, which is the frequency band over which only the  $TE_{10}$  mode can propagate. Choose the height b of the waveguide so that it can carry maximum power without sacrificing the bandwidth of the operating frequency band.
- b) Find the power in watts that the waveguide can carry at 6.0 [GHz] if the magnitude of the electric field inside the waveguide is not allowed to exceed a value of  $E_c = 3.0 \times 10^6$  [V/m] (the breakdown field strength of air at normal atmospheric pressure).



# Part (a)

The design frequency should be halfway between the cutoff frequencies of the  $TE_{10}$  mode and the  $TE_{20}$  mode, since b = a/2. Therefore, we have

$$f_0 = 1.5 f_c^{10} = 1.5 \left( \frac{c}{2a} \right).$$

This gives us

$$a = 3.7474$$
 [cm].

We then have

$$b = 1.8737$$
 [cm].

Note that

$$f_c^{10} = 4.0 \, [\text{GHz}].$$

# Part (b)

We use

$$P_{z} = \left(\frac{ab}{4\omega\mu_{0}}\right)\beta \left|E_{10}\right|^{2}.$$

We set 
$$|E_{10}| = 3.0 \times 10^6 \text{ [V/m]}$$
.

We also have

$$\beta = \frac{2\pi}{\lambda_g} = \frac{2\pi}{\lambda_0} \sqrt{1 - \left(\frac{f_c^{10}}{f_0}\right)^2} = 93.729 \text{ [radians/m]}.$$

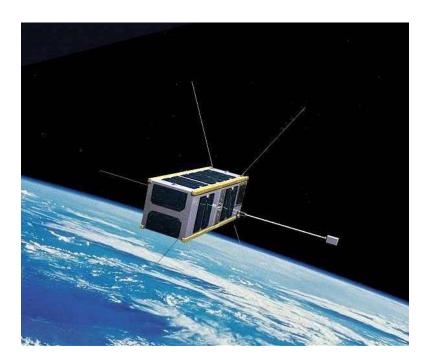
We then have

$$P_z = 3.1257 \times 10^6 [W] = 3.1257 [MW].$$

# **Bonus Problem (20 pts)**

A CubeSat satellite orbits the Earth as shown below. It radiates at 3.0 GHz with 2 [W] of power that is input to a dipole antenna that has a gain of G = 1.5. A student on earth receives the signal from the CubeSat using a Yagi antenna that has a gain of G = 30. The receive antenna (the Yagi) has an input impedance of 50 [ $\Omega$ ] and is connected to a receiver that is modeled as a 50 [ $\Omega$ ] load. The CubeSat is at an altitude of 350 [km]. Both antennas may be assumed to be lossless.

- a) Calculate the power received by the receiver circuit that is connected to the Yagi antenna.
- b) Calculate the magnitude of the open-circuit (Thévenin) signal voltage of the Yagi antenna.



A CubeSat orbiting the Earth.

# Part (a)

The power received is

$$\begin{split} P_{\text{rec}} = & \left[ \left( \frac{P_{\text{in}}}{4\pi r^2} \right) G_{\text{trans}} \right] A_e^{\text{rec}} \\ = & \left[ \left( \frac{P_{\text{in}}}{4\pi r^2} \right) G_{\text{trans}} \right] \left[ G_{\text{rec}} \left( \frac{\lambda_0^2}{4\pi} \right) \right]. \end{split}$$

Inserting the numbers, we have

$$P_{\text{rec}} = \left[ \left( \frac{2}{4\pi \left( 3.5 \times 10^5 \right)^2} \right) 1.5 \right] \left[ 30 \left( \frac{\left( 0.099931 \right)^2}{4\pi} \right) \right].$$

This gives us

$$P_{\text{rec}} = 4.6461 \times 10^{-14} \text{ [W]}.$$

# Part (b)

We have

$$P_{\text{rec}} = \frac{\left|V_{\text{Th}}/2\right|^2}{2R_L} = \frac{\left|V_{\text{Th}}/2\right|^2}{2(50)} = \left|V_{\text{Th}}\right|^2 (0.0025000).$$

This gives us

$$|V_{\rm Th}|^2 (0.0025000) = 4.6461 \times 10^{-14}$$

so that

$$|V_{\text{Th}}| = 4.3110 \times 10^{-6} \text{ [V]} = 4.3110 \text{ [}\mu\text{V]}.$$