ECE 6340 Intermediate EM Waves

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Reciprocity Theorem

Consider two sets of sources, radiating in the same environment.



Note: The same "body" (dielectric or PEC) exists in both cases.

$$\nabla \times \underline{H}^{a} = \underline{J}^{ia} + j\omega\varepsilon_{c}\underline{E}^{a}$$
$$\underline{E}^{b} \cdot (\nabla \times \underline{H}^{a}) = \underline{E}^{b} \cdot \underline{J}^{ia} + j\omega\varepsilon_{c}\underline{E}^{b} \cdot \underline{E}^{a}$$

Also,

$$\nabla \times \underline{E}^{b} = -\underline{M}^{ib} - j\omega\mu\underline{H}^{b}$$

$$\underline{H}^{a} \cdot (\nabla \times \underline{E}^{b}) = -\underline{H}^{a} \cdot \underline{M}^{ib} - j\omega\mu\underline{H}^{a} \cdot \underline{H}^{b}$$

Subtract:

$$\underline{E}^{b} \cdot (\nabla \times \underline{H}^{a}) - \underline{H}^{a} \cdot (\nabla \times \underline{E}^{b}) = \underline{E}^{b} \cdot \underline{J}^{ia} + j\omega\varepsilon_{c} \underline{E}^{b} \cdot \underline{E}^{a} + \underline{H}^{a} \cdot \underline{M}^{ib} + j\omega\mu\underline{H}^{a} \cdot \underline{H}^{b}$$

Vector identity:

$$\nabla \cdot (\underline{H}^{a} \times \underline{E}^{b}) = \underline{E}^{b} \cdot (\nabla \times \underline{H}^{a}) - \underline{H}^{a} \cdot (\nabla \times \underline{E}^{b})$$

Hence,

$$\nabla \cdot (\underline{H}^{a} \times \underline{E}^{b}) = \underline{E}^{b} \cdot \underline{J}^{ia} + j\omega\varepsilon_{c} \underline{E}^{b} \cdot \underline{E}^{a} + \underline{H}^{a} \cdot \underline{M}^{ib} + j\omega\mu\underline{H}^{a} \cdot \underline{H}^{b}$$

From duality (or repeating derivation using Faraday's Law for "a" and Ampere's Law for "b") we have:

$$-\nabla \cdot (\underline{E}^{a} \times \underline{H}^{b}) = \underline{H}^{b} \cdot \underline{M}^{ia} + j\omega\mu\underline{H}^{b} \cdot \underline{H}^{a}$$
$$+\underline{E}^{a} \cdot \underline{J}^{ib} + j\omega\varepsilon_{c}\underline{E}^{a} \cdot \underline{E}^{b}$$

$$\nabla \cdot (\underline{H}^{a} \times \underline{E}^{b}) = \underline{E}^{b} \cdot \underline{J}^{ia} + j\omega\varepsilon_{c} \underline{E}^{b} \cdot \underline{E}^{a} + \underline{H}^{a} \cdot \underline{M}^{ib} + j\omega\mu\underline{H}^{a} \cdot \underline{H}^{b}$$

$$-\nabla \cdot (\underline{E}^{a} \times \underline{H}^{b}) = \underline{H}^{b} \cdot \underline{M}^{ia} + j\omega\mu\underline{H}^{b} \cdot \underline{H}^{a}$$
$$+\underline{E}^{a} \cdot \underline{J}^{ib} + j\omega\varepsilon_{c}\underline{E}^{a} \cdot \underline{E}^{b}$$

Multiply first equation by -1 and then add:

$$-\nabla \cdot (\underline{H}^{a} \times \underline{E}^{b}) - \nabla \cdot (\underline{E}^{a} \times \underline{H}^{b}) = -\underline{E}^{b} \cdot \underline{J}^{ia} - \underline{H}^{a} \cdot \underline{M}^{ib} + \underline{H}^{b} \cdot \underline{M}^{ia} + \underline{E}^{a} \cdot \underline{J}^{ib}$$

$$-\nabla \cdot (\underline{H}^{a} \times \underline{E}^{b}) - \nabla \cdot (\underline{E}^{a} \times \underline{H}^{b}) = -\underline{E}^{b} \cdot \underline{J}^{ia} - \underline{H}^{a} \cdot \underline{M}^{ib} + \underline{H}^{b} \cdot \underline{M}^{ia} + \underline{E}^{a} \cdot \underline{J}^{ib}$$

Reversing the order of the cross products in the first term on the LHS,

$$\nabla \cdot (\underline{E}^{b} \times \underline{H}^{a} - \underline{E}^{a} \times \underline{H}^{b}) = \underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib}$$
$$-\underline{E}^{b} \cdot \underline{J}^{ia} + \underline{H}^{b} \cdot \underline{M}^{ia}$$

Next, integrate both sides over an arbitrary volume *V* and then apply the divergence theorem:



$$\oint_{S} (\underline{E}^{b} \times \underline{H}^{a} - \underline{E}^{a} \times \underline{H}^{b}) \cdot \underline{\hat{n}} \, dS$$

$$= \int_{V} (\underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib} - \underline{E}^{b} \cdot \underline{J}^{ia} + \underline{H}^{b} \cdot \underline{M}^{ia}) \, dV$$

Now let $S \to S_{\infty}$

In the far-field,
$$\underline{H} \sim \frac{1}{\eta} (\hat{\underline{r}} \times \underline{E})$$

Hence

$$(\underline{E}^{b} \times \underline{H}^{a} - \underline{E}^{a} \times \underline{H}^{b}) \sim \frac{1}{\eta} \Big[\underline{E}^{b} \times (\hat{\underline{r}} \times \underline{E}^{a}) - \underline{E}^{a} \times (\hat{\underline{r}} \times \underline{E}^{b}) \Big]$$

$$(\underline{E}^{b} \times \underline{H}^{a} - \underline{E}^{a} \times \underline{H}^{b}) \sim \frac{1}{\eta} \Big[\underline{E}^{b} \times (\hat{\underline{r}} \times \underline{E}^{a}) - \underline{E}^{a} \times (\hat{\underline{r}} \times \underline{E}^{b}) \Big]$$

Now use a vector identity:

$$\underline{A} \times (\underline{B} \times \underline{C}) = (\underline{A} \cdot \underline{C}) \underline{B} - (\underline{A} \cdot \underline{B}) \underline{C}$$

So,

$$(\underline{E}^{b} \times \underline{H}^{a} - \underline{E}^{a} \times \underline{H}^{b}) \sim \frac{1}{\eta} \Big[\underline{\hat{r}} (\underline{E}^{b} \cdot \underline{E}^{a}) - (\underline{\hat{r}} \cdot \underline{E}^{b}) \underline{E}^{a} - \underline{\hat{r}} (\underline{E}^{a} \cdot \underline{E}^{b}) + (\underline{\hat{r}} \cdot \underline{E}^{a}) \underline{E}^{b} \Big]$$

$$= \frac{1}{\eta} \Big[-(\underline{\hat{r}} \cdot \underline{E}^{b}) \underline{E}^{a} + (\underline{\hat{r}} \cdot \underline{E}^{a}) \underline{E}^{b} \Big]$$

$$= O\left(\frac{1}{r^{3}}\right)$$

Hence

$$\oint_{S} (\underline{E}^{b} \times \underline{H}^{a} - \underline{E}^{a} \times \underline{H}^{b}) \cdot \underline{\hat{n}} \, dS \to 0$$

Therefore,

$$\oint_{S} (\underline{E}^{b} \times \underline{H}^{a} - \underline{E}^{a} \times \underline{H}^{b}) \cdot \underline{\hat{n}} \, dS$$

$$= \int_{V} (\underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib} - \underline{E}^{b} \cdot \underline{J}^{ia} + \underline{H}^{b} \cdot \underline{M}^{ia}) \, dV$$

$$\bigcup$$

$$\int_{V} (\underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib} - \underline{E}^{b} \cdot \underline{J}^{ia} + \underline{H}^{b} \cdot \underline{M}^{ia}) dV = 0$$

Final form of reciprocity theorem:

$$\int_{V} (\underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib}) dV = \int_{V} (\underline{E}^{b} \cdot \underline{J}^{ia} - \underline{H}^{b} \cdot \underline{M}^{ia}) dV$$

LHS: Fields of "*a*" dotted with the sources of "*b*" RHS: Fields of "*b*" dotted with the sources of "*a*"

$$\int_{V} (\underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib}) dV = \int_{V} (\underline{E}^{b} \cdot \underline{J}^{ia} - \underline{H}^{b} \cdot \underline{M}^{ia}) dV$$

Define "reactions":

$$< a, b >= \int_{V} (\underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib}) dV$$
$$< b, a >= \int_{V} (\underline{E}^{b} \cdot \underline{J}^{ia} - \underline{H}^{b} \cdot \underline{M}^{ia}) dV$$

Then

Extension: Anisotropic Case

$$\underline{D} = \underline{\underline{\varepsilon}} \cdot \underline{\underline{E}}$$
$$\underline{B} = \underline{\underline{\mu}} \cdot \underline{\underline{H}}$$

 $\underline{\underline{\varepsilon}} = \begin{bmatrix} \varepsilon_{xx} & \varepsilon_{xy} & \varepsilon_{xz} \\ \varepsilon_{yx} & \varepsilon_{yy} & \varepsilon_{yz} \\ \varepsilon_{zx} & \varepsilon_{zy} & \varepsilon_{zz} \end{bmatrix} \qquad \underline{\underline{\mu}} = \begin{bmatrix} \mu_{xx} & \mu_{xy} & \mu_{xz} \\ \mu_{yx} & \mu_{yy} & \mu_{yz} \\ \mu_{zx} & \mu_{zy} & \mu_{zz} \end{bmatrix}$

If $\varepsilon_{ij} = \varepsilon_{ji}$ and $\mu_{ij} = \mu_{ji}$ (symmetric matrices) then reciprocity holds. These are called "reciprocal" materials.

"Testing" Current

Some Basic Observations

- To make the reciprocity theorem useful to us, we usually choose the "b" current to be a "testing" current or "measuring" current.
- > The "b" current thus allows us to sample a quantity of interest.
- This allows us to determine some property about the quantity of interest, or in some cases, to calculate it (or at least calculate it in a simpler way).

Dipole "Testing" Current



$$\langle a,b \rangle = \int_{V} \left(\underline{E}^{a} \cdot \underline{J}^{ib} - \underline{H}^{a} \cdot \underline{M}^{ib} \right) dV$$

$$= \int_{V} \left(\underline{E}^{a} \cdot \hat{\underline{p}} \right) \delta\left(\underline{r} - \underline{r}_{0} \right) dV$$

$$= \hat{\underline{p}} \cdot \underline{E}^{a} \left(\underline{r}_{0} \right)$$
 We sample a field component at a point.

Filament "Testing" Current



$$\langle a,b \rangle = \int_{V} \underline{E}^{a} \cdot \underline{J}^{b} dV \qquad \qquad \underline{J}^{b} = \hat{\underline{l}} J_{l}^{b}$$

$$= \int_{C} \underline{E}^{a} \cdot \hat{\underline{l}} dl \qquad \qquad \int_{\Delta V} J_{l}^{b} dV = \int_{\Delta S} J_{l}^{b} dS \Delta l = I \Delta l = \Delta l$$

$$= \int_{C} \underline{E}^{a} \cdot d\underline{r}$$

$$= V_{AB} \qquad \text{We sample a voltage drop between two points.}$$

Magnetic Frill "Testing" Current



$$< a, b > = \int_{V} -\underline{H}^{a} \cdot \underline{M}^{b} dV$$
$$= -K \int_{C} \underline{H}^{a} \cdot \underline{\hat{l}} dl$$
$$= -\int_{C} \underline{H}^{a} \cdot d\underline{r}$$

Note:

There is no displacement current through the loop if it hugs the PEC wire.

=-I We sample a <u>current on a wire</u>.



Two infinitesimal unit-amplitude electric dipoles



$$\langle a,b\rangle = \langle b,a\rangle$$
$$\int_{V} \underline{E}^{a} \cdot \underline{J}^{b} - \underline{H}^{a} \cdot \underline{M}^{b} dV = \int_{V} \underline{E}^{b} \cdot \underline{J}^{a} - \underline{H}^{b} \cdot \underline{M}^{a} dV$$

$$E_z^a(\underline{r}_b) = E_z^b(\underline{r}_a)$$



Two infinitesimal unit-amplitude electric dipoles



$$\langle a,b\rangle = \langle b,a\rangle$$
$$\int_{V} \underline{E}^{a} \cdot \underline{J}^{b} - \underline{H}^{a} \cdot \underline{M}^{b} dV = \int_{V} \underline{E}^{b} \cdot \underline{J}^{a} - \underline{H}^{b} \cdot \underline{M}^{a} dV$$

$$E_x^a(\underline{r}_b) = E_z^b(\underline{r}_a)$$



The far-field transmit and receive patterns of any antenna are the same.



$$T(\theta,\phi) \equiv E_p(\underline{r}_0)$$



$$R(\theta,\phi) \equiv V^{PW}$$



The antenna (and feed wires) is the "body."



Note: The black color is used to show where dipole "b" is, even though it is not radiating here.

Hence, we have

$$\langle a,b \rangle = T(\theta,\phi)$$

Example (cont.)



The voltage V^b is the open-circuit voltage due to a <u>unit-amplitude dipole</u> in the far field.

Note: The black color is used to show where filament "*a*" is, even though it is not radiating here.

As $r \rightarrow \infty$, the incident field from dipole "b" becomes a plane-wave field.



We need to determine the incident field \underline{E} from the dipole:

Let
$$\underline{\hat{p}} \to \underline{\hat{z}}' \qquad \underline{E} \sim \underline{\hat{\theta}}' \left(\frac{j\omega\mu_0}{4\pi r}\right) e^{-jkr} \sin\theta'$$

$$\theta' = \frac{\pi}{2}$$
 so $\underline{E} \sim \hat{\underline{\theta}}' \left(\frac{j\omega\mu_0}{4\pi r}\right) e^{-jkr} = -\hat{\underline{p}} \left(\frac{j\omega\mu_0}{4\pi r}\right) e^{-jkr}$

Define
$$E_0 \equiv \left(\frac{-j\omega\mu_0}{4\pi r}\right)e^{-jkr}$$



$$r \to \infty$$
 $\underline{E} \sim \underline{\hat{p}} E_0$



Hence $\underline{E}^{b,inc}(0,0,0) \approx E_0 \ \underline{\hat{p}}$

More generally,

$$\underline{E}^{b,inc}(x,y,z) \approx E_0 \underline{\hat{p}} e^{+j\underline{k}\cdot\underline{r}}$$

The incident field from the "testing" dipole thus acts as a plane wave polarized in the \hat{p} direction, with amplitude E_0 at the origin.

Hence

$$\langle b,a\rangle = V^b = E_0 V^{PW} = E_0 R(\theta,\phi)$$



Summarizing, we have:

$$\langle a,b \rangle = T(\theta,\phi)$$

$$\langle b, a \rangle = E_0 R(\theta, \phi)$$

From reciprocity:

$$\langle a, b \rangle = \langle b, a \rangle$$

SO

$$T(\theta,\phi) = E_0 R(\theta,\phi)$$

Hence, in summary we have:

$$T(\theta,\phi) = R(\theta,\phi) \left[\left(\frac{-j\omega\mu_0}{4\pi r} \right) e^{-jkr} \right]$$

The shape of the far-field transmit and receive patterns are the same.



Reciprocity in circuit theory

 V_2

 I_{12}

 I_{21}



 I_{21} = current at location 2 produced by V_1

 I_{12} = current at location 1 produced by V_2

Note: If $V_1 = V_2$, then the result becomes $I_{12} = I_{21}$.

Example (cont.)

Magnetic frill modeling of voltage source



K is the amplitude of the magnetic frill current that flows in the positive ϕ direction.



The sources (*a* and *b*) are the magnetic frills; the "environment" is the circuit.

$$\langle a,b\rangle = \int_{V} -\underline{H}^{a} \cdot \underline{M}^{b} dV = -K_{2} \int_{C_{2}} \underline{H}^{a} \cdot \underline{\hat{l}} dl = V_{2} \int_{C_{2}} \underline{H}^{a} \cdot \underline{\hat{l}} dl = V_{2} I_{21}$$

$$\langle b,a\rangle = \int_{V} -\underline{H}^{b} \cdot \underline{M}^{a} dV = -K_{1} \int_{C_{2}} \underline{H}^{b} \cdot \underline{\hat{l}} dl = V_{1} \int_{C_{1}} \underline{H}^{b} \cdot \underline{\hat{l}} dl = V_{1} I_{12}$$

From reciprocity: $\langle a, b \rangle = \langle b, a \rangle$

Hence

$$V_2 I_{21} = V_1 I_{12}$$

or

$$\frac{V_1}{I_{21}} = \frac{V_2}{I_{12}}$$