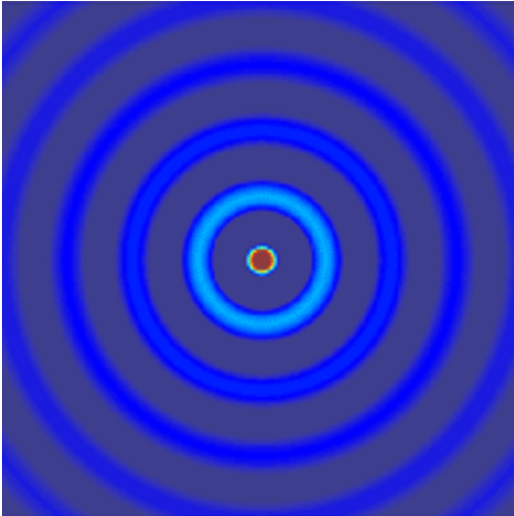


# ECE 6341

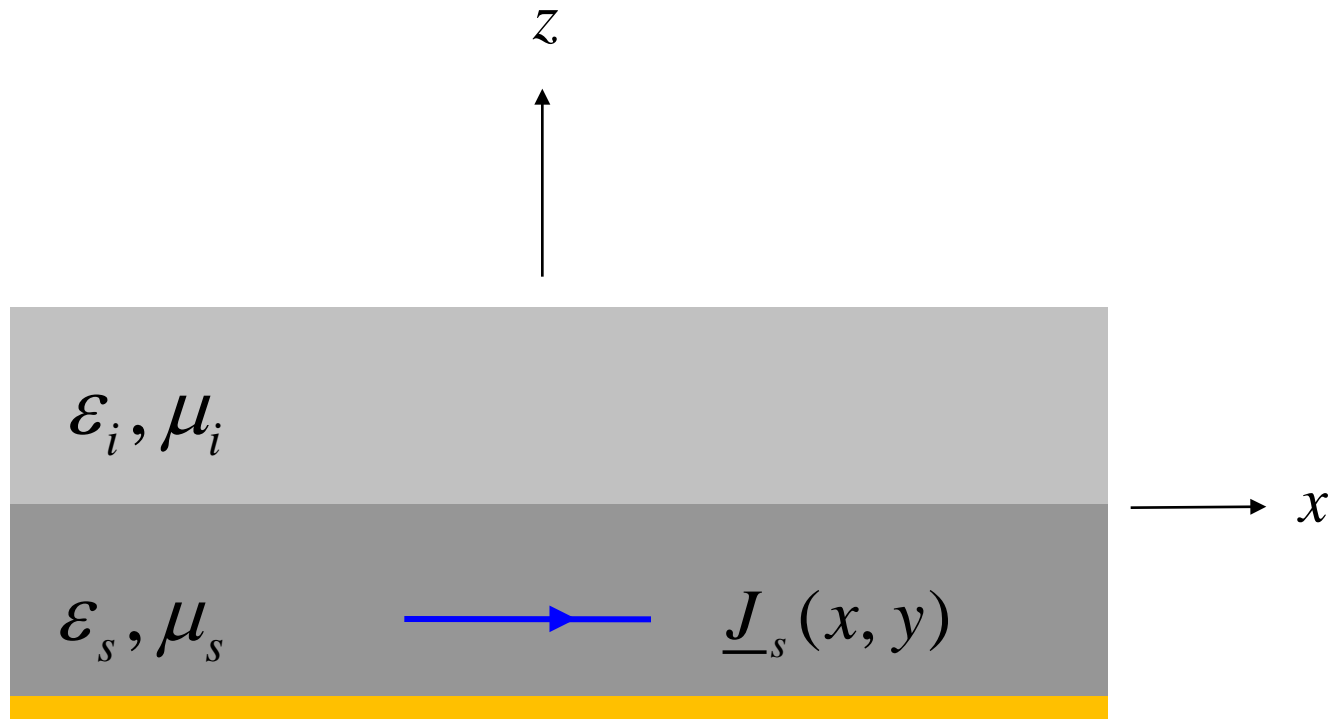
Spring 2016

Prof. David R. Jackson  
ECE Dept.



## Notes 38

# Spectral Domain Immittance (SDI) Method



$$\underline{J}_s(x, y) = \frac{1}{(2\pi)^2} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \tilde{\underline{J}}_s(k_x, k_y) e^{-j(k_x x + k_y y)} dk_x dk_y$$

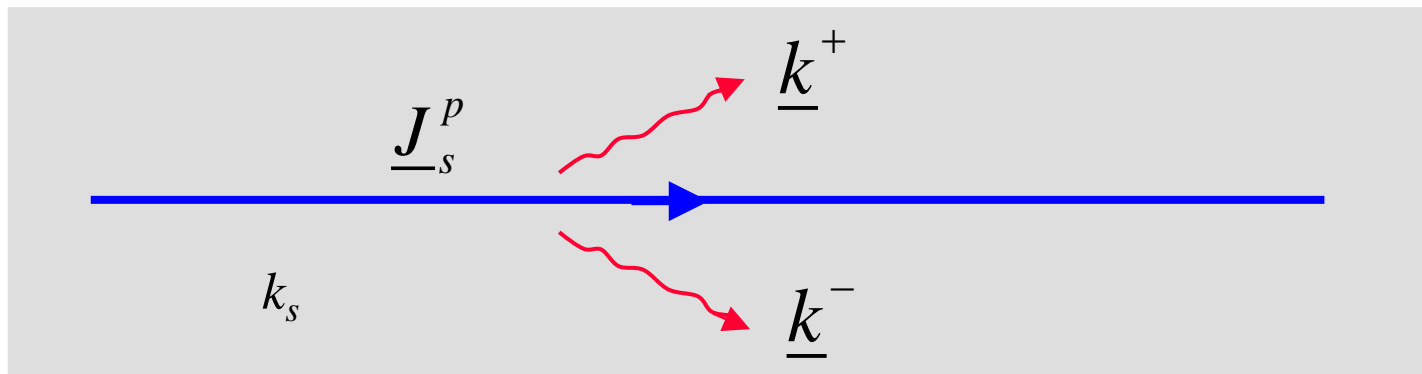
# SDI Method (cont.)

The finite current sheet is thus represented as a set of infinite phased current sheets:

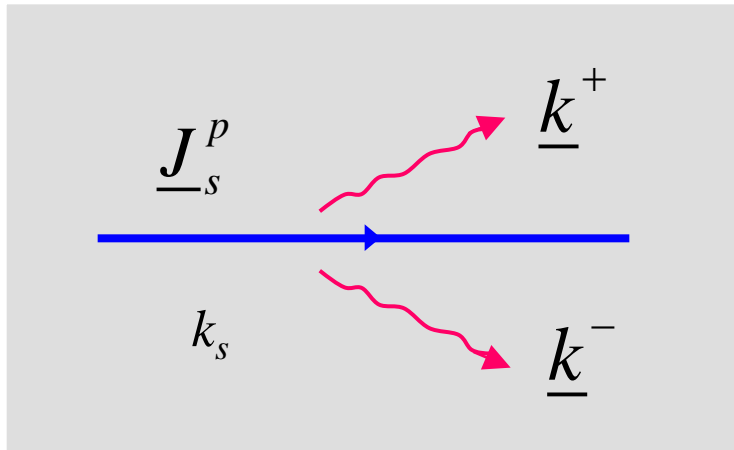
$$\underline{J}_s^P(x, y) = \underline{J}_{s0}^P e^{-j(k_x x + k_y y)}$$

where 
$$\underline{J}_{s0}^P = \frac{1}{(2\pi)^2} \tilde{\underline{J}}_s(k_x, k_y) dk_x dk_y$$

This phased current sheet launches a pair of plane waves as shown below:



# SDI Method (cont.)



$$\underline{k}^+ = \hat{x} k_x + \hat{y} k_y + \hat{z} k_{zs}$$

$$\underline{k}^- = \hat{x} k_x + \hat{y} k_y - \hat{z} k_{zs}$$

$$k_{zs} = \left( k_s^2 - k_t^2 \right)^{1/2}$$

$$k_t^2 = k_x^2 + k_y^2$$

Goal: Decompose the current into two parts: one that excites only a pair of  $\text{TM}_z$  plane waves, and one that excites only a pair of  $\text{TE}_z$  plane waves.

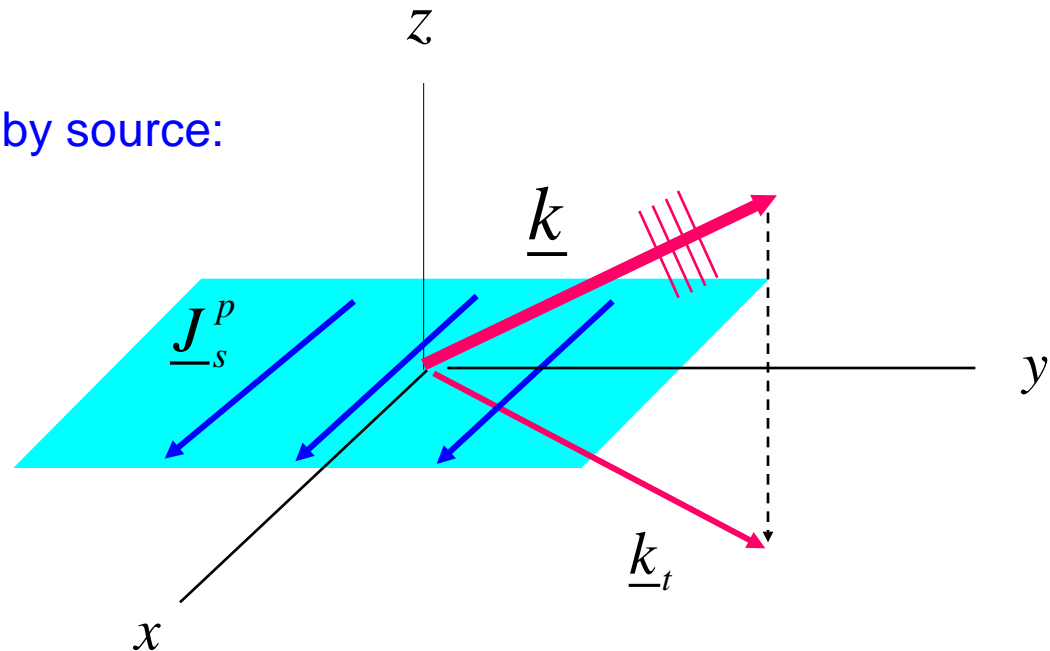
# SDI Method (cont.)

Define:

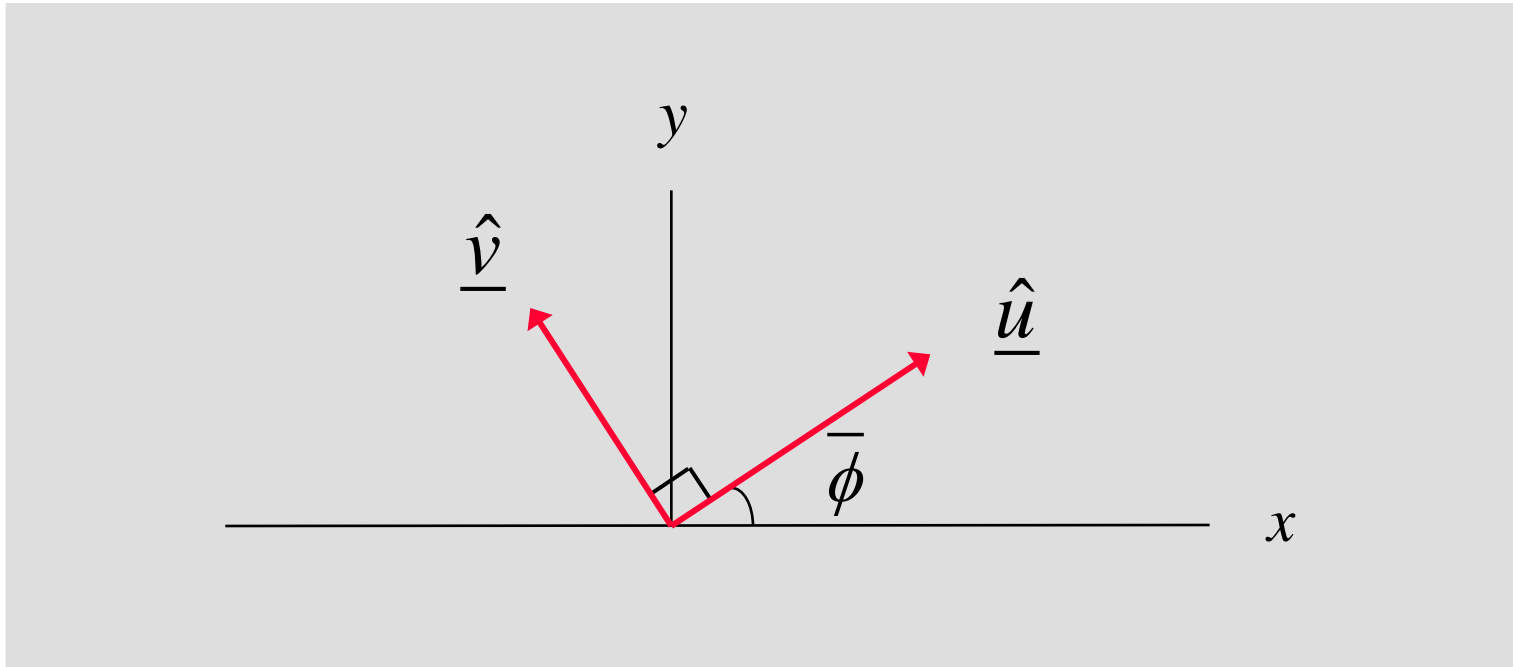
$$\underline{k}_t \equiv \hat{x} k_x + \hat{y} k_y$$

$$\underline{\hat{u}} \equiv \frac{\underline{k}_t}{k_t} \quad \underline{\hat{v}} \equiv \underline{\hat{z}} \times \underline{\hat{u}}$$

Launching of plane wave by source:

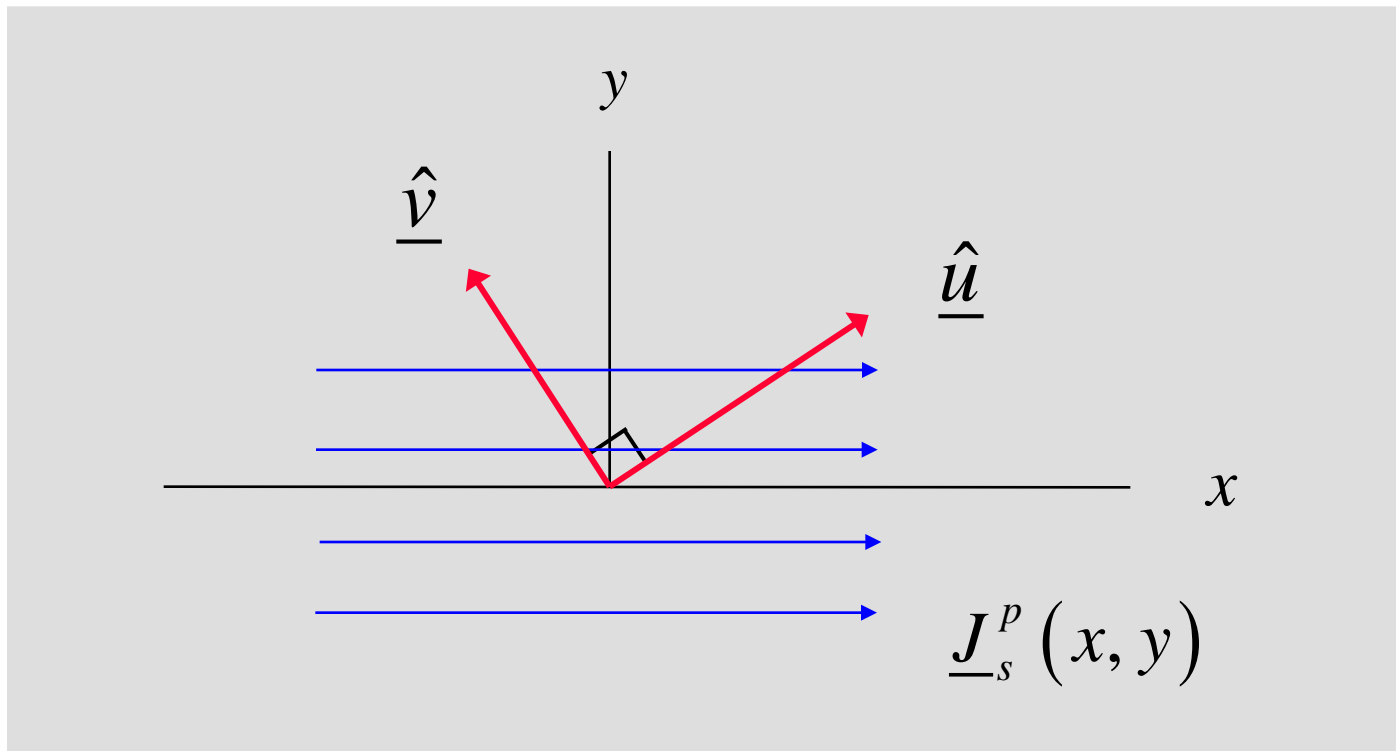


# SDI Method (cont.)



$$\cos \bar{\phi} = \frac{k_x}{k_t} \quad \sin \bar{\phi} = \frac{k_y}{k_t}$$

# SDI Method (cont.)



$\underline{J}_{su}^p(x, y)$ : Launches a  $TM_z$  wave

$\underline{J}_{sv}^p(x, y)$ : Launches a  $TE_z$  wave

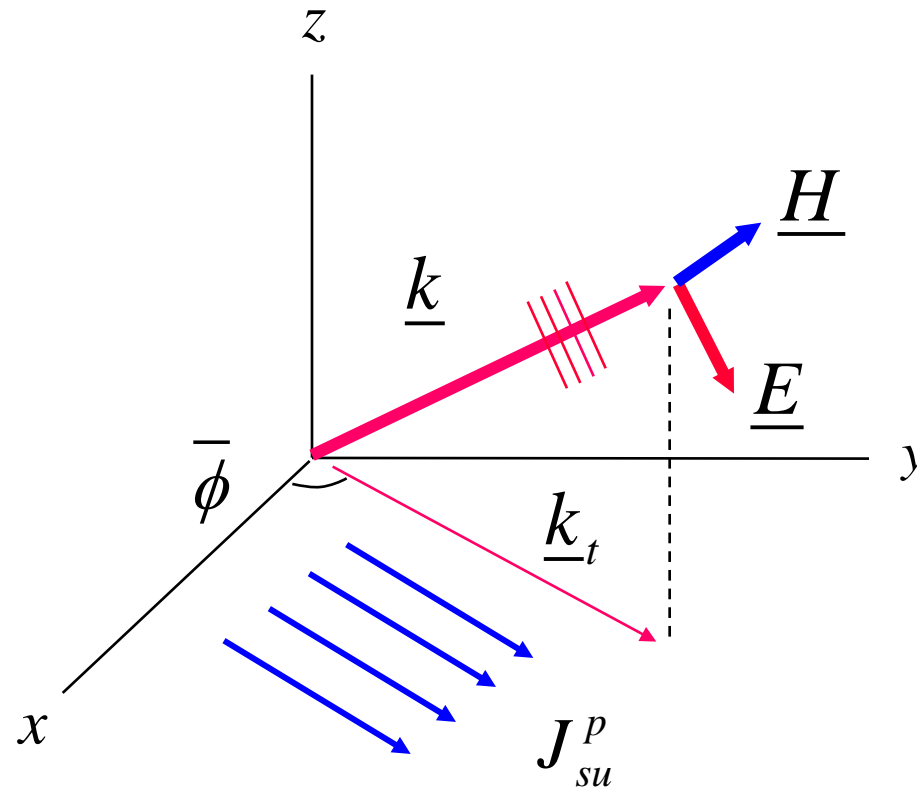
A proof of this is given next.

# SDI Method (cont.)

TM<sub>z</sub>

$$\underline{E}_t = \hat{u} E_u$$

$$\underline{H}_t = \hat{v} H_v$$



This figure shows the  $u$  component of the current launching a TM<sub>z</sub> plane wave.

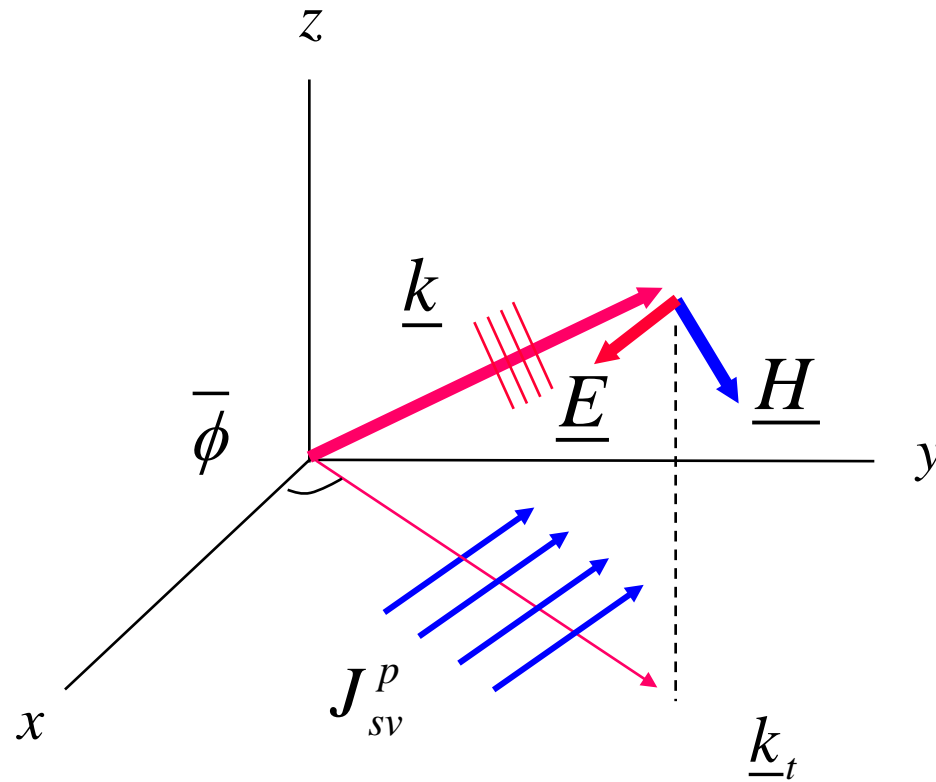


# SDI Method (cont.)

$TE_z$

$$\underline{E}_t = \hat{v} E_v$$

$$\underline{H}_t = \hat{u} H_u$$



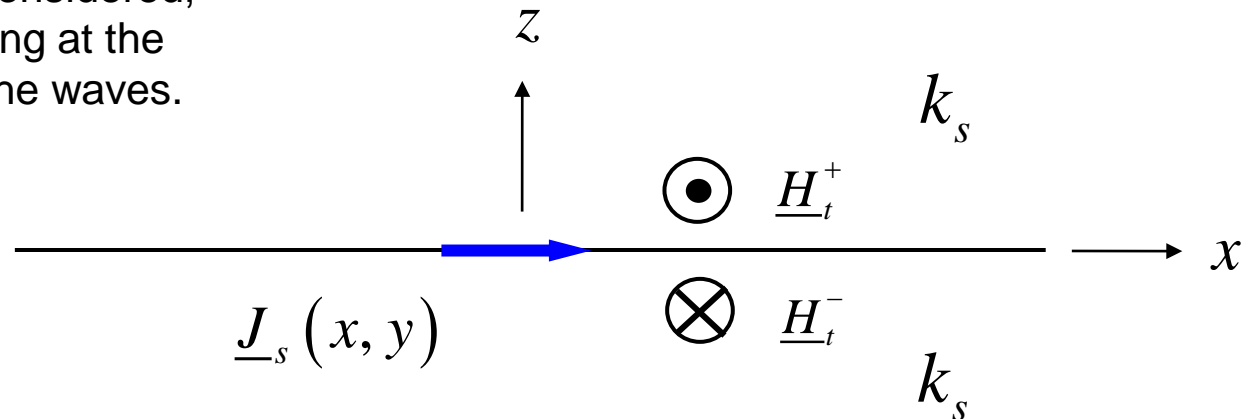
This figure shows the  $v$  component of the current launching a  $TE_z$  plane wave.

# SDI Method (cont.)

Proof of launching property:

Consider an arbitrary surface current.

An infinite medium is considered, since we are only looking at the launching property of the waves.

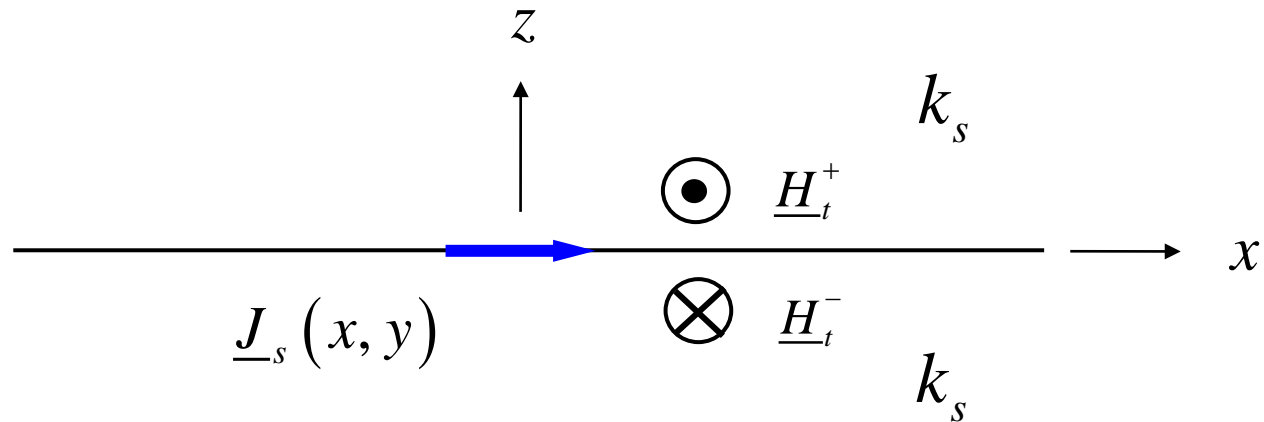


At  $z = 0$  we have that  $\underline{H}_t^+ = -\underline{H}_t^-$

Note: This follows from the fact that the magnetic vector potential component  $A_x$  is an even function of  $z$  (imagining the current to be in the  $x$  direction for simplicity here).

$$H_y = \frac{1}{\mu} \frac{\partial A_x}{\partial z}$$

# SDI Method (cont.)



$$\hat{\underline{z}} \times (\underline{H}_t^+ - \underline{H}_t^-) = \underline{J}_s$$

$$2 \hat{\underline{z}} \times \underline{H}_t^+ = \underline{J}_s$$

Hence

$$\underline{H}_t^+ = -\frac{1}{2} \hat{\underline{z}} \times \underline{J}_s$$

# SDI Method (cont.)

$$\underline{H}_t^+ = -\frac{1}{2} \underline{\hat{z}} \times \underline{J}_s$$

This is the tangential magnetic field just above the infinite current sheet, which gets launched by the current sheet.

Note: This result is general, and does not assume phased current sheets.

Two cases of interest for phased current sheets:

$$\underline{J}_s(x, y) = \underline{\hat{u}} J_{su}^p(x, y) \quad \Rightarrow \quad \underline{H}_t^+ = \underline{\hat{v}} H_v^+ \quad (TM_z)$$

$$\underline{J}_s(x, y) = \underline{\hat{v}} J_{sv}^p(x, y) \quad \Rightarrow \quad \underline{H}_t^+ = \underline{\hat{u}} H_u^+ \quad (TE_z)$$

# SDI Method (cont.)

Split original current into two parts:

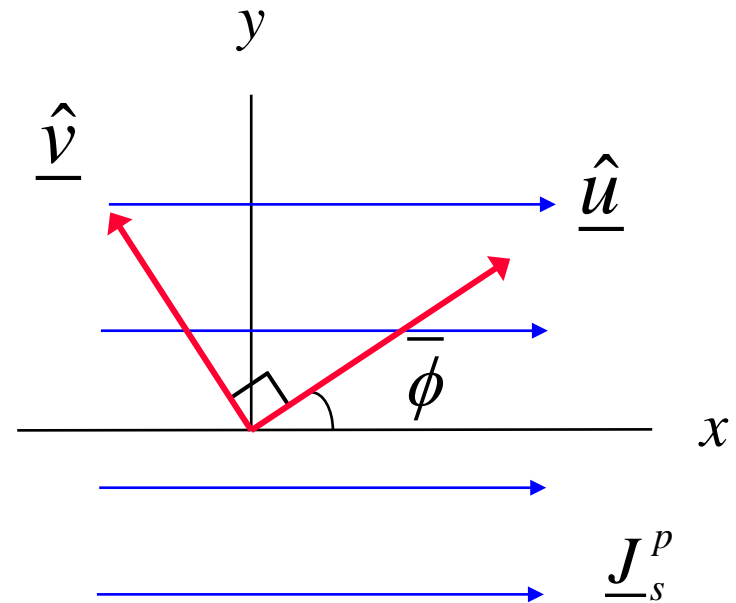
$$\underline{J}_s^P(x, y) = \underline{\hat{u}} J_{su}^P(x, y) + \underline{\hat{v}} J_{sv}^P(x, y)$$

Launches  $\text{TM}_z$

Launches  $\text{TE}_z$

$$J_{su}^P(x, y) = \underline{J}_s^P(x, y) \cdot \underline{\hat{u}}$$

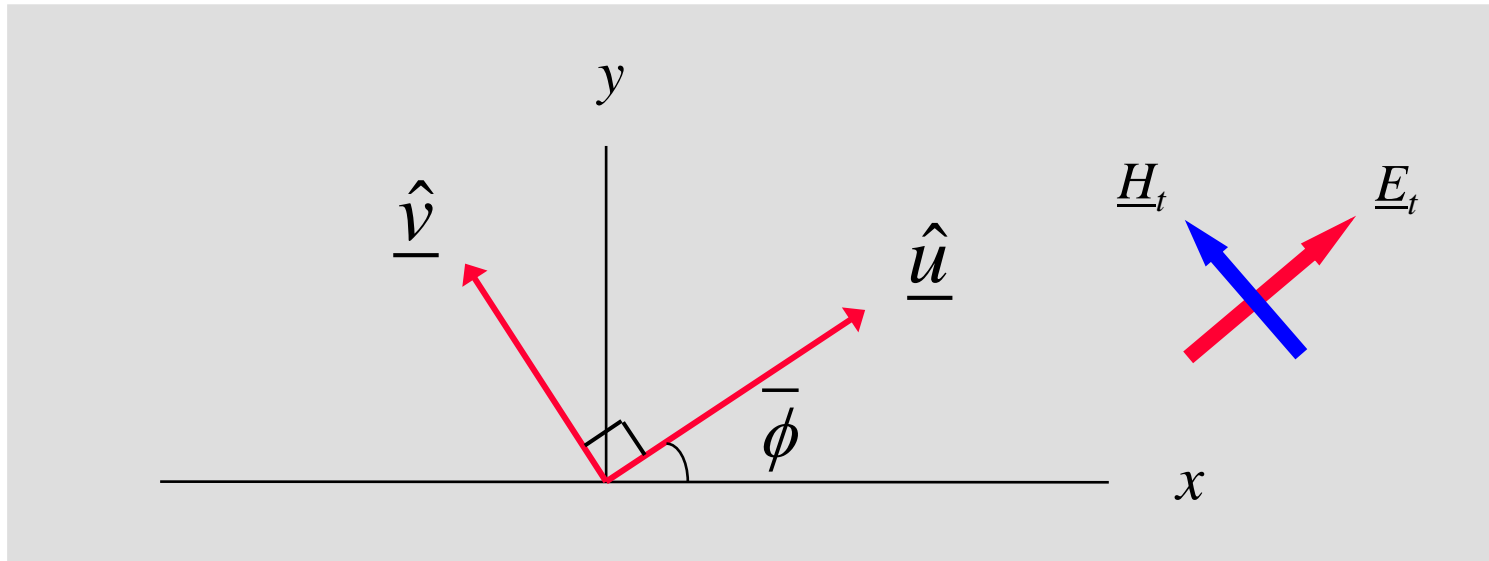
$$J_{sv}^P(x, y) = \underline{J}_s^P(x, y) \cdot \underline{\hat{v}}$$



# Transverse Fields

**TM<sub>z</sub>:**

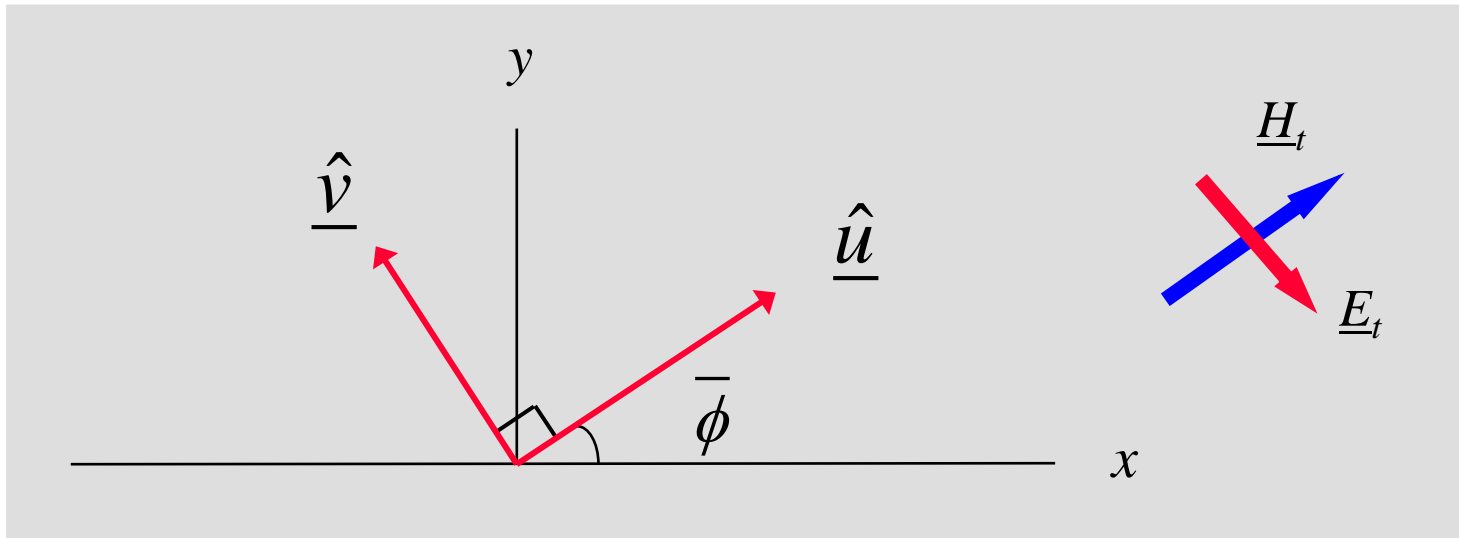
$$\underline{E}_t = \underline{\hat{u}} E_u(x, y, z) = \underline{\hat{u}} E_{u0}(z) e^{-j(k_x x + k_y y)}$$
$$\underline{H}_t = \underline{\hat{v}} H_v(x, y, z) = \underline{\hat{v}} H_{v0}(z) e^{-j(k_x x + k_y y)}$$



# Transverse Fields (cont.)

**TE<sub>z</sub>:**

$$\underline{E}_t = \underline{\hat{v}} E_v(x, y, z) = \underline{\hat{v}} E_{v0}(z) e^{-j(k_x x + k_y y)}$$
$$\underline{H}_t = \underline{\hat{u}} H_u(x, y, z) = \underline{\hat{u}} H_{u0}(z) e^{-j(k_x x + k_y y)}$$



# Transverse Equivalent Network

TEN modeling equations:

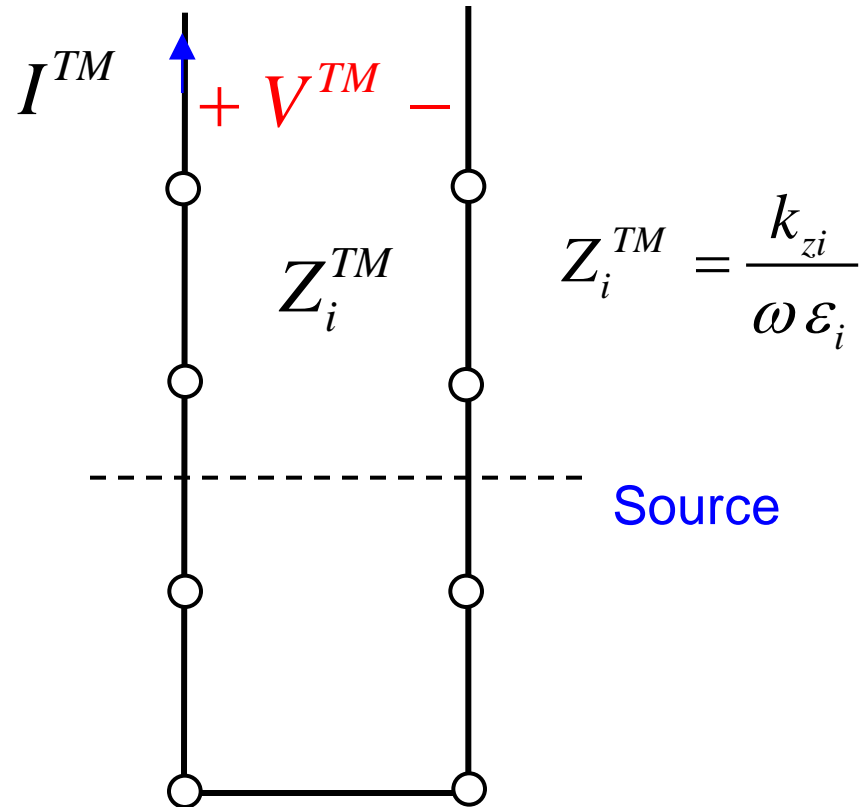
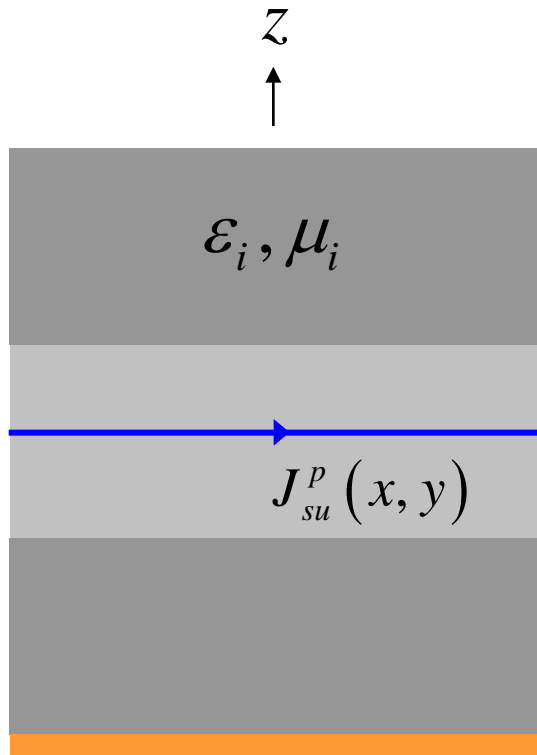
$$\begin{aligned} \text{TM}_z : \quad & V^{TM}(z) = E_{u0}(z) \\ & I^{TM}(z) = H_{v0}(z) \end{aligned}$$

$$\begin{aligned} \text{TE}_z : \quad & V^{TE}(z) = -E_{v0}(z) \\ & I^{TE}(z) = H_{u0}(z) \end{aligned}$$



# TEN (cont.)

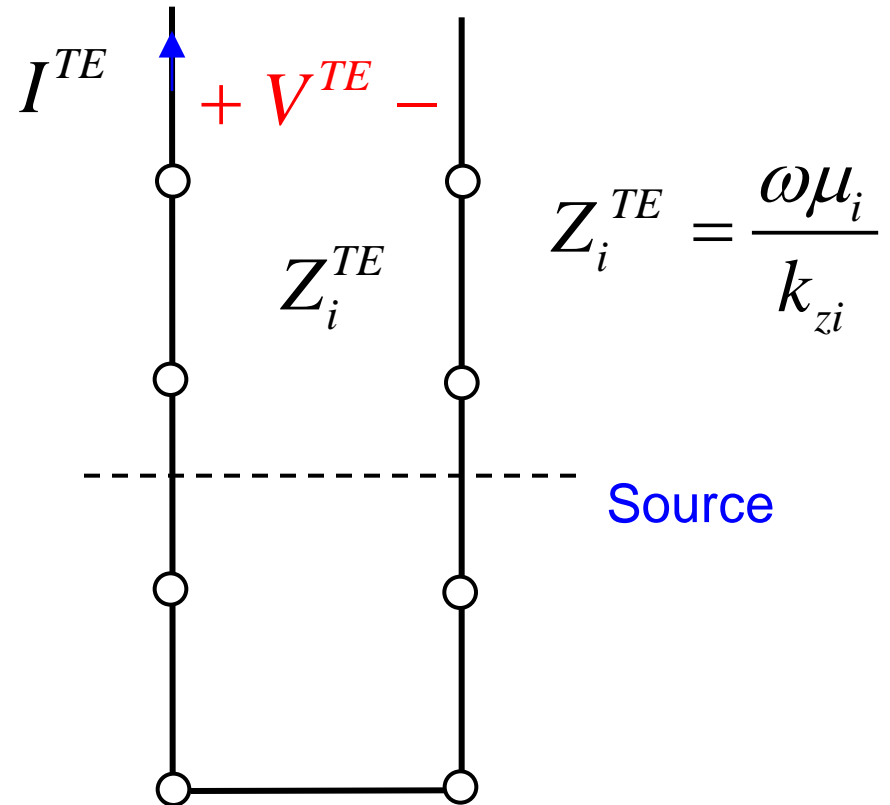
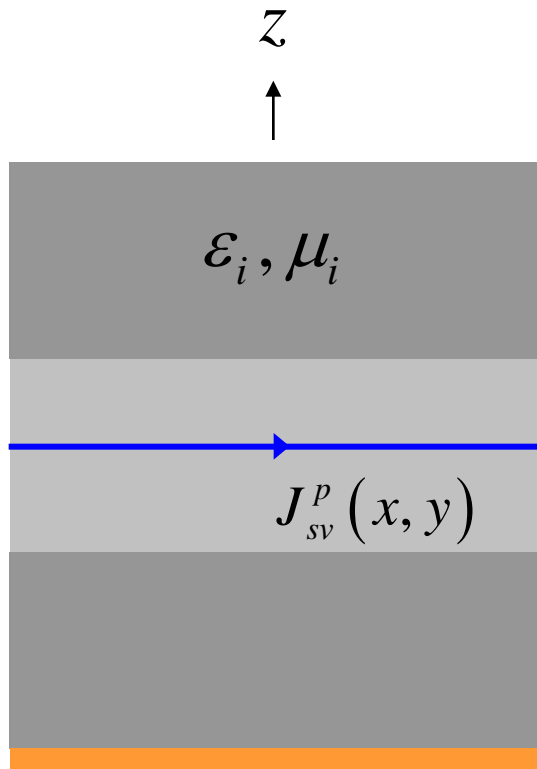
TM<sub>z</sub>



$$k_{zi} = \left( k_i^2 - k_x^2 - k_y^2 \right)^{1/2}$$

# TE<sub>z</sub> (cont.)

TE<sub>z</sub>

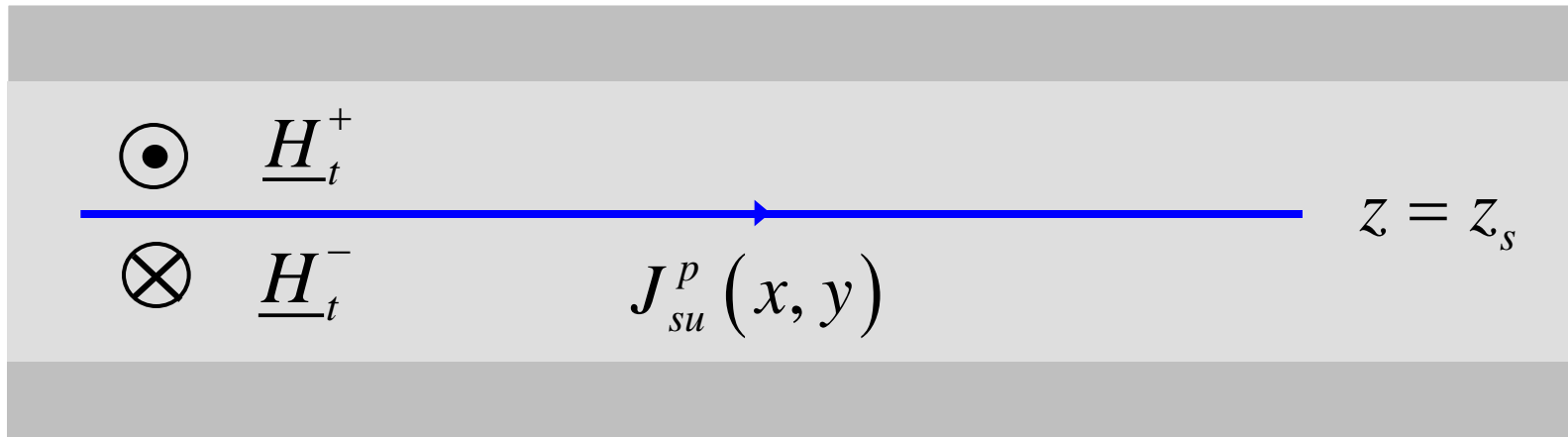


$$k_{zi} = \left(k_i^2 - k_x^2 - k_y^2\right)^{1/2}$$

# Source Model

TM<sub>z</sub>

Infinite phased current sheet inside layered medium



$$\hat{\underline{z}} \times (\underline{H}_t^+ - \underline{H}_t^-) = \underline{J}_s(x, y) = \hat{\underline{u}} J_{su}^p(x, y)$$

$$\hat{\underline{z}} \times \left[ \hat{\underline{v}} (H_v^+ - H_v^-) \right] = \hat{\underline{u}} J_{su}^p(x, y)$$

$$-\hat{\underline{u}} (H_v^+ - H_v^-) = \hat{\underline{u}} J_{su}^p(x, y)$$

# Source Model (cont.)

$$H_v^+(x, y) - H_v^-(x, y) = -J_{su}^p(x, y)$$

so

$$H_{v0}^+ - H_{v0}^- = -J_{su0}^p$$

Hence

$$I^{TM}(z_s^+) - I^{TM}(z_s^-) = -J_{su0}^p$$

Also  $\hat{z} \times (\underline{E}_t^+ - \underline{E}_t^-) = \underline{0}$

$$\longrightarrow (\hat{z} \times \hat{u})(E_u^+ - E_u^-) = \underline{0} \longrightarrow E_u^+ = E_u^- \longrightarrow E_{u0}^+ = E_{u0}^-$$

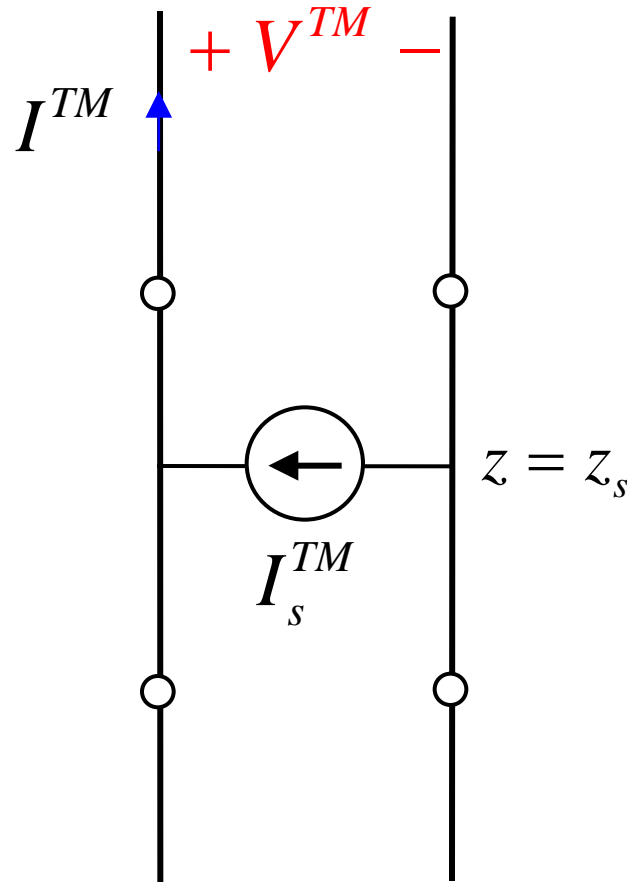
Hence

$$V^{TM}(z_s^+) = V^{TM}(z_s^-)$$

# Source Model (cont.)

TM<sub>z</sub> Model:

$$I_s^{TM} = -\underline{J}_{s0}^p \cdot \hat{u}$$

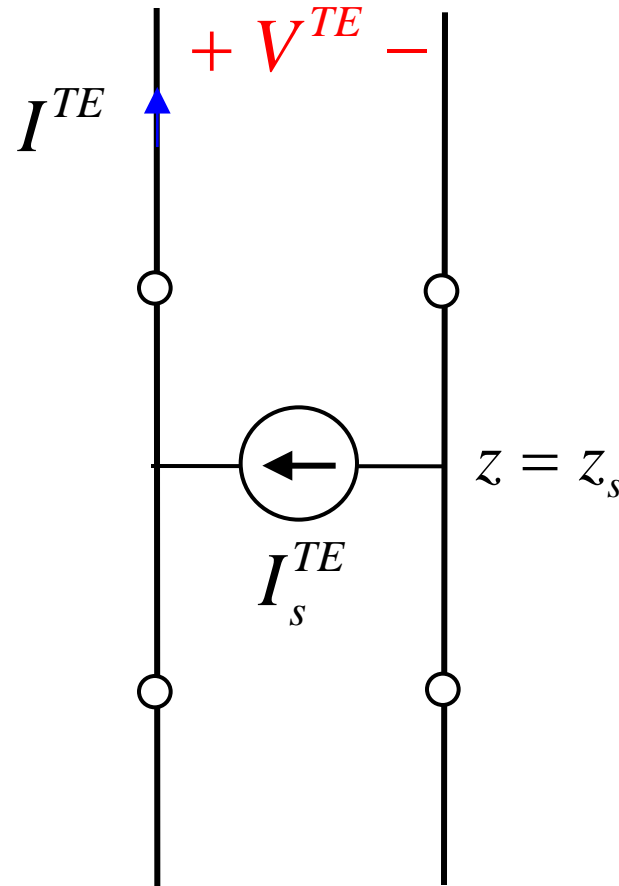


# Source Model (cont.)

TE<sub>z</sub> Model:

$$I_s^{TE} = \underline{J}_{s0}^p \cdot \underline{\hat{v}}$$

(derivation omitted)



# Source Model (cont.)

The transverse fields can then be found from

$$E_u(x, y, z) = V^{TM}(z) e^{-j(k_x x + k_y y)}$$

$$H_v(x, y, z) = I^{TM}(z) e^{-j(k_x x + k_y y)}$$

$$-E_v(x, y, z) = V^{TE}(z) e^{-j(k_x x + k_y y)}$$

$$H_u(x, y, z) = I^{TE}(z) e^{-j(k_x x + k_y y)}$$

# Source Model (cont.)

Introduce **normalized** voltage and current functions:  
(following the notation of K. A. Michalski)

$$V_i^{TM/TE}(z) = V^{TM/TE}(z) \quad \text{when} \quad I_s^{TM/TE} = 1 \text{ [A]}$$

$$I_i^{TM/TE}(z) = I^{TM/TE}(z) \quad \text{when} \quad I_s^{TM/TE} = 1 \text{ [A]}$$

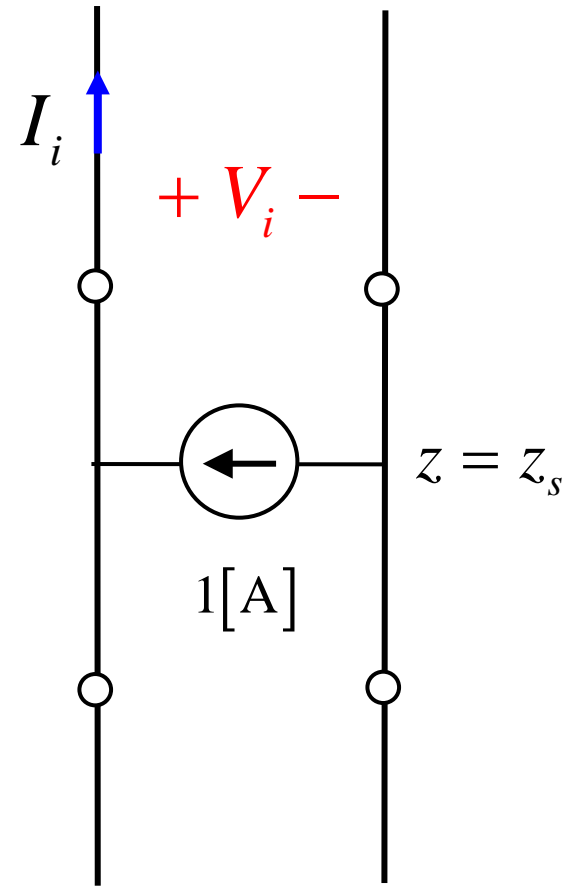
Then we can write

$$V^{TM}(z) = V_i^{TM}(z) \left( -\underline{J}_{s0}^p \cdot \underline{\hat{u}} \right)$$

$$I^{TM}(z) = I_i^{TM}(z) \left( -\underline{J}_{s0}^p \cdot \underline{\hat{u}} \right)$$

$$V^{TE}(z) = V_i^{TE}(z) \left( \underline{J}_{s0}^p \cdot \underline{\hat{v}} \right)$$

$$I^{TE}(z) = I_i^{TE}(z) \left( \underline{J}_{s0}^p \cdot \underline{\hat{v}} \right)$$





# Source Model (cont.)

Hence

$$E_u(x, y, z) = V_i^{TM}(z) \left( -\underline{J}_{s0}^p \cdot \underline{\hat{u}} \right) e^{-j(k_x x + k_y y)}$$

$$H_v(x, y, z) = I_i^{TM}(z) \left( -\underline{J}_{s0}^p \cdot \underline{\hat{u}} \right) e^{-j(k_x x + k_y y)}$$

$$-E_v(x, y, z) = V_i^{TE}(z) \left( +\underline{J}_{s0}^p \cdot \underline{\hat{v}} \right) e^{-j(k_x x + k_y y)}$$

$$H_u(x, y, z) = I_i^{TE}(z) \left( +\underline{J}_{s0}^p \cdot \underline{\hat{v}} \right) e^{-j(k_x x + k_y y)}$$

# Example

Find  $E_x(x, y, z)$  for  $z \geq 0$  due to a surface current at  $z = 0$

$$\underline{J}_s^P = \hat{x} e^{-j(k_x x + k_y y)}$$

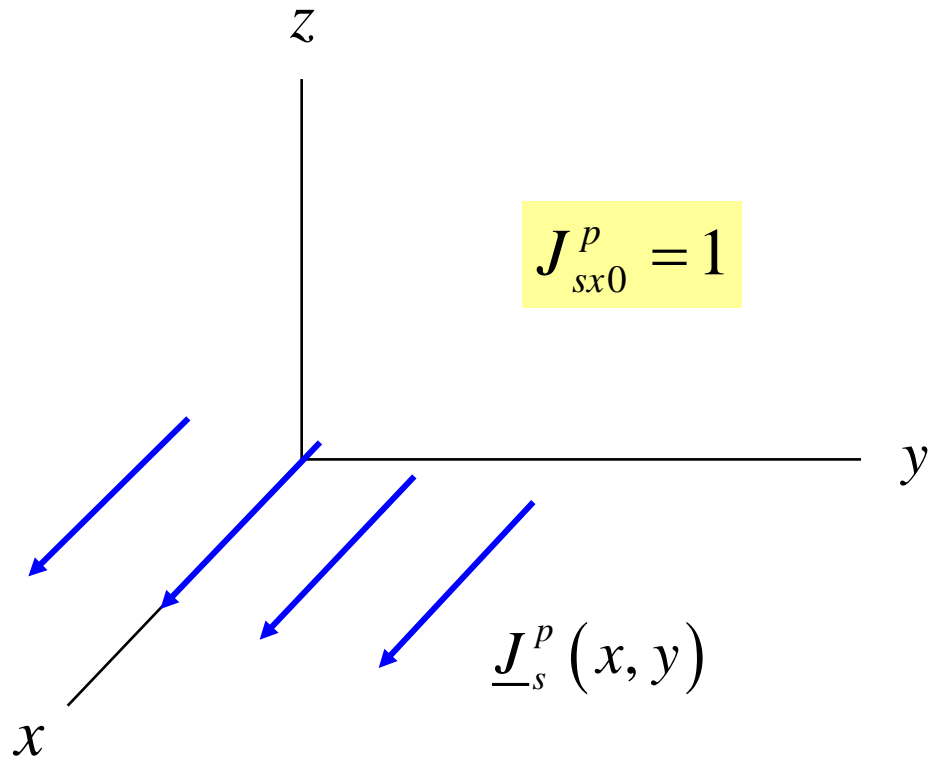
The current is radiating in free space.

with

$$k_x = 2k_0$$

$$k_y = k_0$$

$$k_t = \sqrt{5}k_0$$



# Example

Decompose current into two parts:

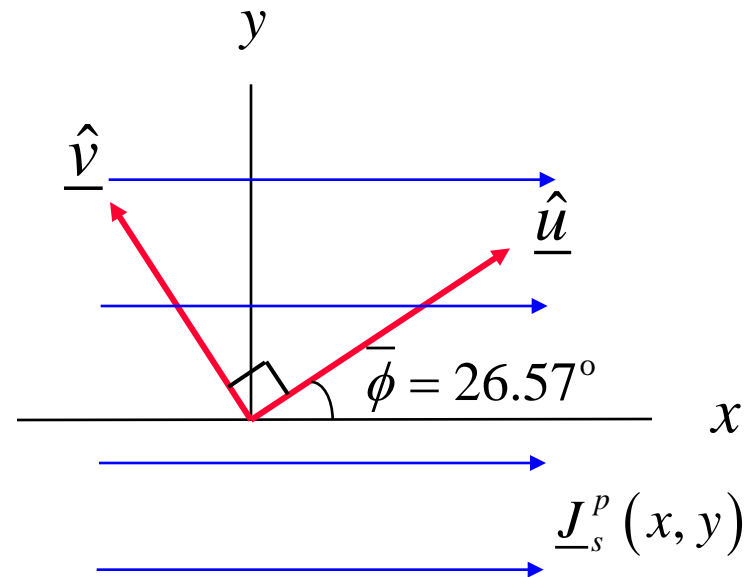
$$E_x = E_u (\underline{\hat{u}} \cdot \underline{\hat{x}}) + E_v (\underline{\hat{v}} \cdot \underline{\hat{x}})$$

$$\tan \bar{\phi} = \frac{k_y}{k_x} = 0.5$$

$$\bar{\phi} = 26.57^\circ$$

$$\underline{\hat{u}} \cdot \underline{\hat{x}} = \cos \bar{\phi} = \frac{k_x}{k_t} = \frac{2}{\sqrt{5}}$$

$$\underline{\hat{v}} \cdot \underline{\hat{x}} = -\sin \bar{\phi} = -\frac{k_y}{k_t} = -\frac{1}{\sqrt{5}}$$



# Example (cont.)

$$\begin{aligned} E_x &= E_u (\cos \bar{\phi}) + E_v (-\sin \bar{\phi}) \\ &= E_u \left( \frac{k_x}{k_t} \right) + E_v \left( -\frac{k_y}{k_t} \right) \\ &= \frac{1}{k_t} \left[ k_x E_{u0} - k_y E_{v0} \right] e^{-j(k_x x + k_y y)} \\ &= \frac{1}{k_t} \left[ k_x V^{TM} (z) + k_y V^{TE} (z) \right] e^{-j(k_x x + k_y y)} \\ &= \frac{1}{k_t} \left[ k_x V_i^{TM} (z) (I_s^{TM}) + k_y V_i^{TE} (z) (I_s^{TE}) \right] e^{-j(k_x x + k_y y)} \\ &= \frac{1}{k_t} \left[ k_x V_i^{TM} (z) (-\underline{J}_{s0}^p \cdot \underline{\hat{u}}) + k_y V_i^{TE} (z) (+\underline{J}_{s0}^p \cdot \underline{\hat{v}}) \right] e^{-j(k_x x + k_y y)} \end{aligned}$$

# Example (cont.)

$$\begin{aligned}
 E_x &= \frac{1}{k_t} \left[ k_x V_i^{TM} (z) \left( -\underline{J}_{s0}^p \cdot \underline{\hat{u}} \right) + k_y V_i^{TE} (z) \left( +\underline{J}_{s0}^p \cdot \underline{\hat{v}} \right) \right] e^{-j(k_x x + k_y y)} \\
 &= \frac{1}{k_t} \left[ k_x V_i^{TM} (z) \left( -J_{sx0}^p \right) (\underline{\hat{x}} \cdot \underline{\hat{u}}) + k_y V_i^{TE} (z) \left( +J_{sx0}^p \right) (\underline{\hat{x}} \cdot \underline{\hat{v}}) \right] e^{-j(k_x x + k_y y)} \\
 &= \frac{1}{k_t} \left[ k_x V_i^{TM} (z) \left( -J_{sx0}^p \right) (\cos \bar{\phi}) + k_y V_i^{TE} (z) \left( +J_{sx0}^p \right) (-\sin \bar{\phi}) \right] e^{-j(k_x x + k_y y)} \\
 &= \frac{1}{k_t} \left[ k_x V_i^{TM} (z) \left( -J_{sx0}^p \right) \left( \frac{k_x}{k_t} \right) + k_y V_i^{TE} (z) \left( +J_{sx0}^p \right) \left( -\frac{k_y}{k_t} \right) \right] e^{-j(k_x x + k_y y)}
 \end{aligned}$$

# Example (cont.)

Hence

$$E_x(x, y, z) = \frac{-1}{k_t^2} \left[ k_x^2 V_i^{TM}(z) + k_y^2 V_i^{TE}(z) \right] J_{sx0}^p e^{-j(k_x x + k_y y)}$$

$$J_{sx0}^p = 1 \quad k_x = 2k_0 \quad k_t = \sqrt{5}k_0$$
$$k_y = k_0$$

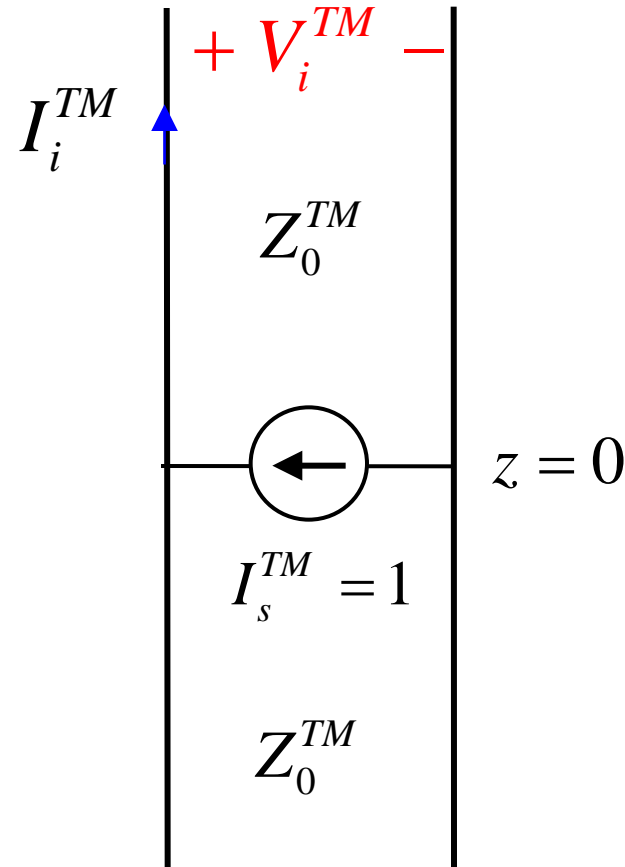
# Example (cont.)

## TM<sub>z</sub> Model

For  $z > 0$ :

$$V_i^{TM}(z) = \frac{Z_0^{TM}}{2} e^{-jk_{z0}z}$$

$$I_i^{TM}(z) = \frac{1}{2} e^{-jk_{z0}z}$$



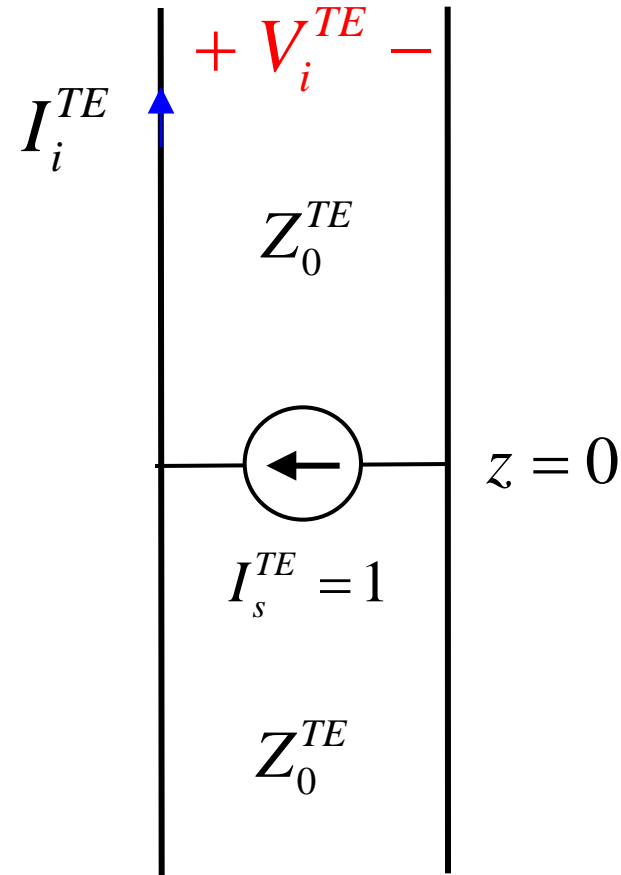
# Example (cont.)

## TE<sub>z</sub> Model

For  $z > 0$ :

$$V_i^{TE}(z) = \frac{Z_0^{TE}}{2} e^{-jk_{z0}z}$$

$$I_i^{TE}(z) = \frac{1}{2} e^{-jk_{z0}z}$$





# Example (cont.)

Hence

$$E_x(x, y, z) = \frac{-1}{k_t^2} \left[ k_x^2 V_i^{TM}(z) + k_y^2 V_i^{TE}(z) \right] J_{sx0}^p e^{-j(k_x x + k_y y)}$$



$$E_x(x, y, z) = \frac{-1}{k_t^2} \left[ k_x^2 \left( \frac{Z_0^{TM}}{2} \right) + k_y^2 \left( \frac{Z_0^{TE}}{2} \right) \right] J_{sx0}^p e^{-j(k_x x + k_y y)} e^{-jk_{z0} z}$$

where

$$Z_0^{TM} = \frac{k_{z0}}{\omega \epsilon_0} \quad Z_0^{TE} = \frac{\omega \mu_0}{k_{z0}}$$

$$k_{z0} = \left( k_0^2 - k_x^2 - k_y^2 \right)^{1/2}$$

# Example (cont.)

Substituting in values, we have:  $k_x = 2k_0$     $k_y = k_0$     $k_t^2 = 5k_0^2$

$$k_{z0} = -j2k_0 \quad Z_0^{TM} = -j2\eta_0 \quad Z_0^{TE} = j\frac{\eta_0}{2} \quad J_{sx0}^P = 1$$

Hence

$$E_x(x, y, z) = \frac{-1}{5k_0^2} \left[ 4k_0^2 (-j\eta_0) + k_0^2 \left( \frac{j\eta_0}{4} \right) \right] e^{-j(2k_0x+k_0y)} e^{-2k_0z}$$

or

$$E_x(x, y, z) = \frac{j\eta_0}{5} \left[ \frac{15}{16} \right] e^{-jk_0(2x+y)} e^{-2k_0z}$$

or

$$E_x(x, y, z) = \frac{j3}{16} \eta_0 e^{-jk_0(2x+y)} e^{-2k_0z} \quad (z \geq 0)$$