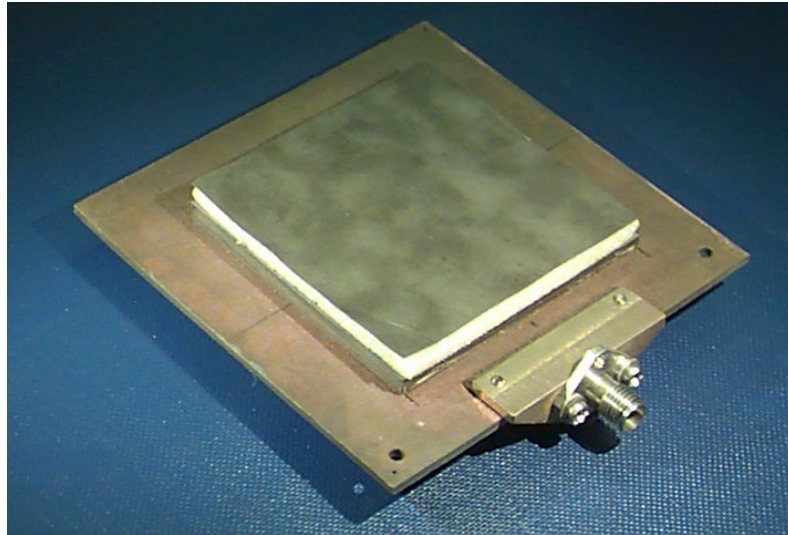


ECE 6345

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Notes 1

Overview

This set of notes discusses the Q (quality factor) of a patch and its different components, as well as the radiation efficiency of the patch based on the Q components.

- Define Q and its components: Q_d , Q_c , Q_{sp} , Q_{sw}
- Calculate Q_d , Q_c , Q_{sp} , Q_{sw}
- Calculate the radiation efficiency based on the Q components.

Q of a Resonator

$$Q \equiv 2\pi \left(\frac{U_S}{U_D^T} \right)$$

U_S = energy stored inside resonator

U_D^T = energy dissipated per cycle (period T)

$$Q \equiv \frac{2\pi}{T} \left(\frac{U_S}{U_D^T / T} \right)$$

$T = 1 / f_0 =$ period

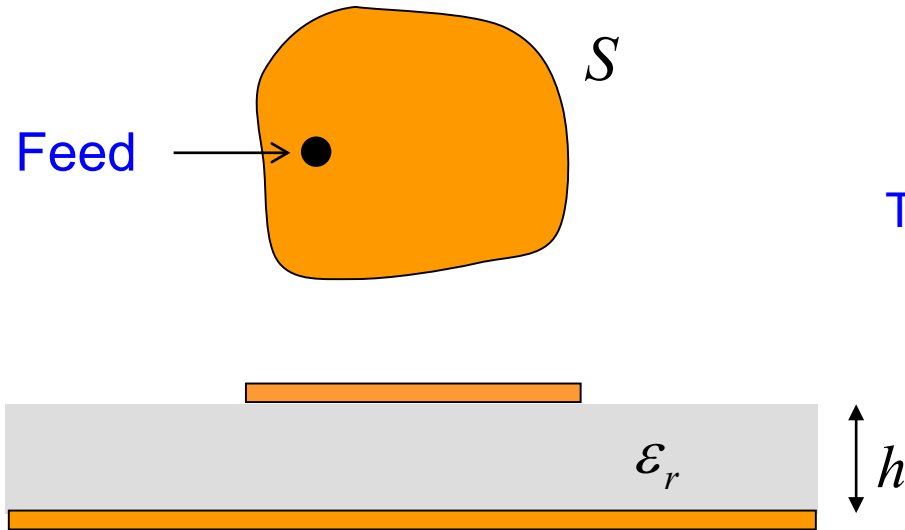
or

$$Q \equiv \omega_0 \left(\frac{U_S}{P_D^{\text{ave}}} \right)$$

P_D^{ave} = average power "dissipated"

(This includes radiation loss)

Q of the Patch



The patch is allowed to have an arbitrary shape here.

$$Q = \omega_0 \frac{U_S}{P_D^{\text{ave}}} \quad \text{so} \quad \frac{1}{Q} = \frac{P_D^{\text{ave}}}{\omega_0 U_S}$$

$$P_D^{\text{ave}} = P_D^{\text{sp}} + P_D^{\text{sw}} + P_D^c + P_D^d$$

Note: ω_0 denotes the resonance frequency (radians/second).

Q of the Patch (cont.)

Hence, we have:

$$\frac{1}{Q} = \frac{P_D^{\text{sp}}}{\omega_0 U_S} + \frac{P_D^{\text{sw}}}{\omega_0 U_S} + \frac{P_D^c}{\omega_0 U_S} + \frac{P_D^d}{\omega_0 U_S}$$

or

$$\frac{1}{Q} = \frac{1}{Q_{\text{sp}}} + \frac{1}{Q_{\text{sw}}} + \frac{1}{Q_c} + \frac{1}{Q_d}$$

Note: Combining Q terms is like combining resistors in parallel.

Note: A smaller Q is a more dominant one!

Calculation of Q_d

$$U_S = \langle U_S \rangle = \langle U_E \rangle + \langle U_H \rangle = 2 \langle U_E \rangle \quad (\text{We have equal time-average stored energies at resonance.})$$

$$= 2 \int_V \frac{1}{4} \epsilon' |\underline{E}|^2 dV$$

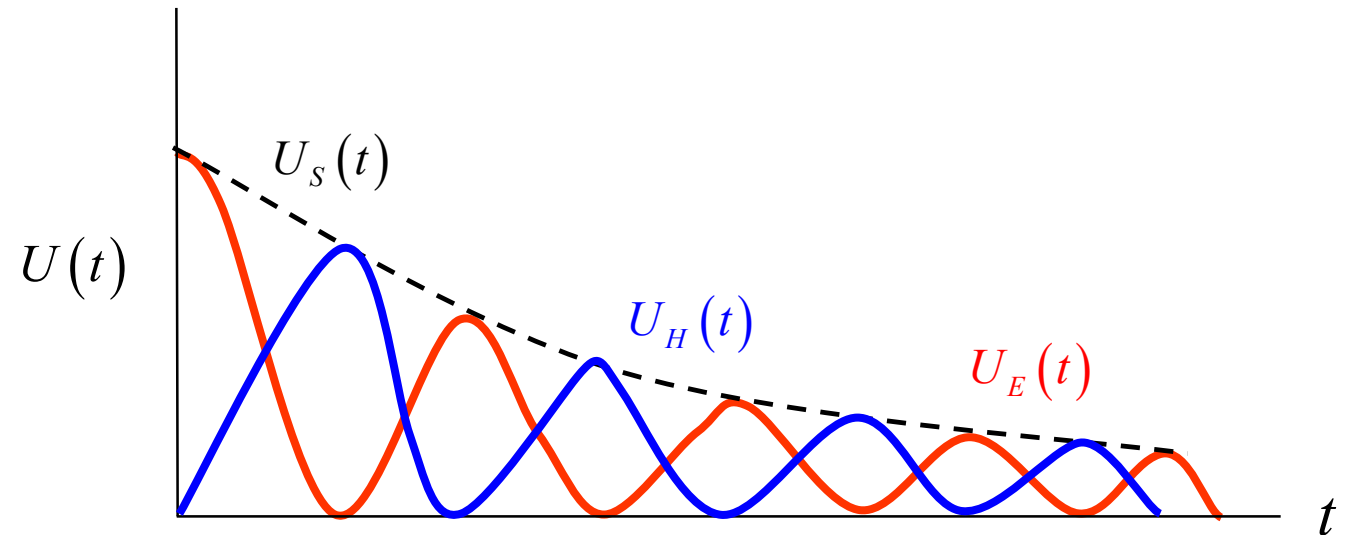
$$= \frac{1}{2} \epsilon' h \int_S |\underline{E}|^2 dS$$

Note:

The total stored energy U_S is a slowly decaying function of time (approximately constant over a cycle).

From ECE 6340:

$$P_D^d = \int_V \frac{1}{2} (\omega_0 \epsilon'') |\underline{E}|^2 dV$$
$$= \frac{1}{2} \omega_0 \epsilon'' h \int_S |\underline{E}|^2 dS$$



Calculation of Q_d (cont.)

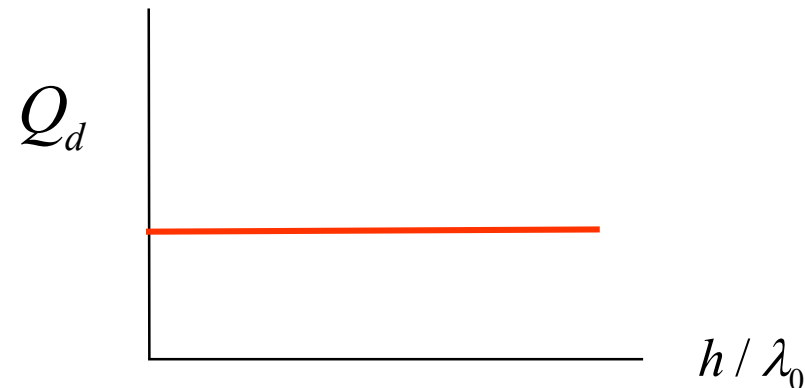
Hence

$$Q^d = \omega_0 \left[\frac{\frac{1}{2} \varepsilon' h \int_S |\underline{E}|^2 dS}{\frac{1}{2} \omega_0 \varepsilon'' h \int_S |\underline{E}|^2 dS} \right] = \frac{\varepsilon'}{\varepsilon''}$$

Therefore, we have:

$$Q^d = \frac{1}{\tan \delta}$$

The dielectric Q factor is independent of the substrate thickness.



Calculation of Q_c

$$\langle P_D^c \rangle = \int_{S_P} \frac{1}{2} R_s^{\text{patch}} |\underline{H}|^2 dS + \int_{S_G} \frac{1}{2} R_s^{\text{ground}} |\underline{H}|^2 dS$$

S_P denotes patch

S_G denotes ground plane

Hence, we have:

$$R_s^{\text{ave}} = (R_s^{\text{patch}} + R_s^{\text{ground}}) / 2$$

$$\begin{aligned} \langle P_D^c \rangle &= \frac{1}{2} (R_s^{\text{patch}} + R_s^{\text{ground}}) \int_S |\underline{H}|^2 dS \\ &= R_s^{\text{ave}} \int_S |\underline{H}|^2 dS \end{aligned}$$

$$R_s = \frac{1}{\sigma \delta}$$

$$\delta = \sqrt{\frac{2}{\omega \mu \sigma}}$$

Calculation of Q_c (cont.)

For the stored energy,

$$U_S = \langle U_S \rangle = \langle U_E \rangle + \langle U_H \rangle = 2 \langle U_H \rangle$$

where

$$\begin{aligned} \langle U_H \rangle &= \int_V \frac{1}{4} \mu |\underline{H}|^2 dV \\ &= \frac{1}{4} \mu_0 \mu_r h \int_S |\underline{H}|^2 dS \end{aligned}$$

Calculation of Q_c (cont.)

Hence,

$$Q_c = \omega_0 \frac{2 \left(\frac{1}{4} \mu_0 \mu_r h \int_S |\underline{H}|^2 dS \right)}{R_s^{\text{ave}} \int_S |\underline{H}|^2 dS}$$

Use $\omega_0 = \frac{k_0}{\sqrt{\mu_0 \epsilon_0}}$

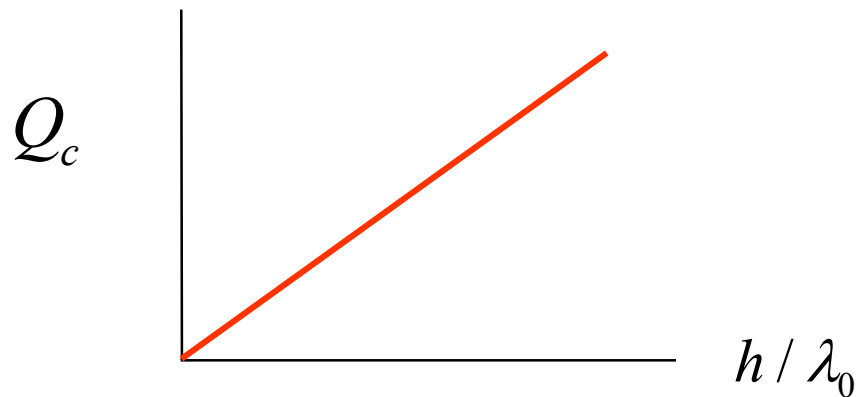
We then have:

$$Q_c = \frac{\frac{1}{2} \mu_0 \mu_r (k_0 h)}{R_s^{\text{ave}} \sqrt{\mu_0 \epsilon_0}} = \frac{\frac{1}{2} \mu_r (k_0 h)}{R_s^{\text{ave}}} \sqrt{\frac{\mu_0}{\epsilon_0}}$$

Calculation of Q_c (cont.)

Hence, we have:

$$Q_c = \left(\frac{\eta_0}{2} \right) \mu_r \left[\frac{(k_0 h)}{R_s^{\text{ave}}} \right]$$



The conducting Q factor becomes more important (smaller) as the substrate gets thinner.

Calculation of Q_{sp}

Rectangular Patch: (The derivation is given later.)

$$Q_{sp} \approx \frac{3}{16} \left(\frac{\epsilon_r}{pc_1} \right) \left(\frac{L_e}{W_e} \right) \left(\frac{1}{h / \lambda_0} \right)$$

$$c_1 = 1 - \frac{1}{n_1^2} + \frac{2/5}{n_1^4} \quad \left(n_1 = \sqrt{\epsilon_r \mu_r} \right)$$

$$p = 1 + \frac{a_2}{10} (k_0 W_e)^2 + (a_2^2 + 2a_4) \left(\frac{3}{560} \right) (k_0 W_e)^4 \\ + c_2 \left(\frac{1}{5} \right) (k_0 L_e)^2 + a_2 c_2 \left(\frac{1}{70} \right) (k_0 W_e)^2 (k_0 L_e)^2$$

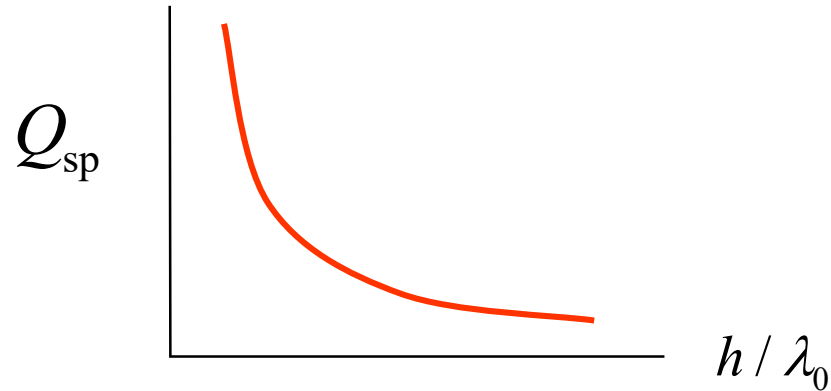
where

$$a_2 = -0.16605$$

$$a_4 = 0.00761$$

$$c_2 = -0.0914153$$

Calculation of Q_{sp} (cont.)



The radiation Q factor becomes more important (smaller) as the substrate gets thicker.

$$Q_{sp} \approx \frac{3}{16} \left(\frac{\epsilon_r}{pc_1} \right) \left(\frac{L_e}{W_e} \right) \left(\frac{1}{h / \lambda_0} \right)$$

Calculation of Q_{SW}

Surface-wave radiation efficiency:

$$e_r^{sw} \equiv \frac{P_{sp}}{P_{sp} + P_{sw}}$$

so

$$\frac{1}{e_r^{sw}} = \frac{P_{sp} + P_{sw}}{P_{sp}} = 1 + \frac{P_{sw}}{P_{sp}}$$

Hence

$$P_{sw} = P_{sp} \left(\frac{1}{e_r^{sw}} - 1 \right)$$

Calculation of Q_{sw} (cont.)

Now look at the Q 's :

$$Q_{sw} = \omega_0 \frac{U_s}{P_{sw}}$$

$$Q_{sp} = \omega_0 \frac{U_s}{P_{sp}}$$

Hence, we have

$$\begin{aligned} \frac{Q_{sw}}{Q_{sp}} &= \frac{P_{sp}}{P_{sw}} \\ &= \frac{1}{\frac{1}{e_r^{sw}} - 1} \\ &= \frac{e_r^{sw}}{1 - e_r^{sw}} \end{aligned}$$

Calculation of Q_{sw} (cont.)

Hence, we have:

$$Q_{sw} = Q_{sp} \left(\frac{e_r^{sw}}{1 - e_r^{sw}} \right)$$

For the radiation efficiency, the patch can be approximated by a horizontal electric dipole (HED) at the center of the patch.

$$e_r^{sw} \approx e_r^{hed}$$

(This is approximately true for any shape of patch.)

Calculation of Q_{SW} (cont.)

$$e_r^{\text{hed}} = \frac{P_{\text{sp}}^{\text{hed}}}{P_{\text{sp}}^{\text{hed}} + P_{\text{sw}}^{\text{hed}}} = \frac{1}{1 + \left(P_{\text{sw}}^{\text{hed}} / P_{\text{sp}}^{\text{hed}} \right)}$$

$$P_{\text{sp}}^{\text{hed}} \approx \frac{1}{\lambda_0^2} (k_0 h)^2 \left(80\pi^2 \mu_r^2 c_1 \right)$$

$$P_{\text{sw}}^{\text{hed}} \approx \frac{1}{\lambda_0^2} (k_0 h)^3 \left(60\pi^3 \mu_r^3 \left(1 - \frac{1}{n_1^2} \right)^3 \right)$$

where

$$c_1 = 1 - \frac{1}{n_1^2} + \frac{2/5}{n_1^4}$$

$$n_1 = \sqrt{\varepsilon_r \mu_r}$$

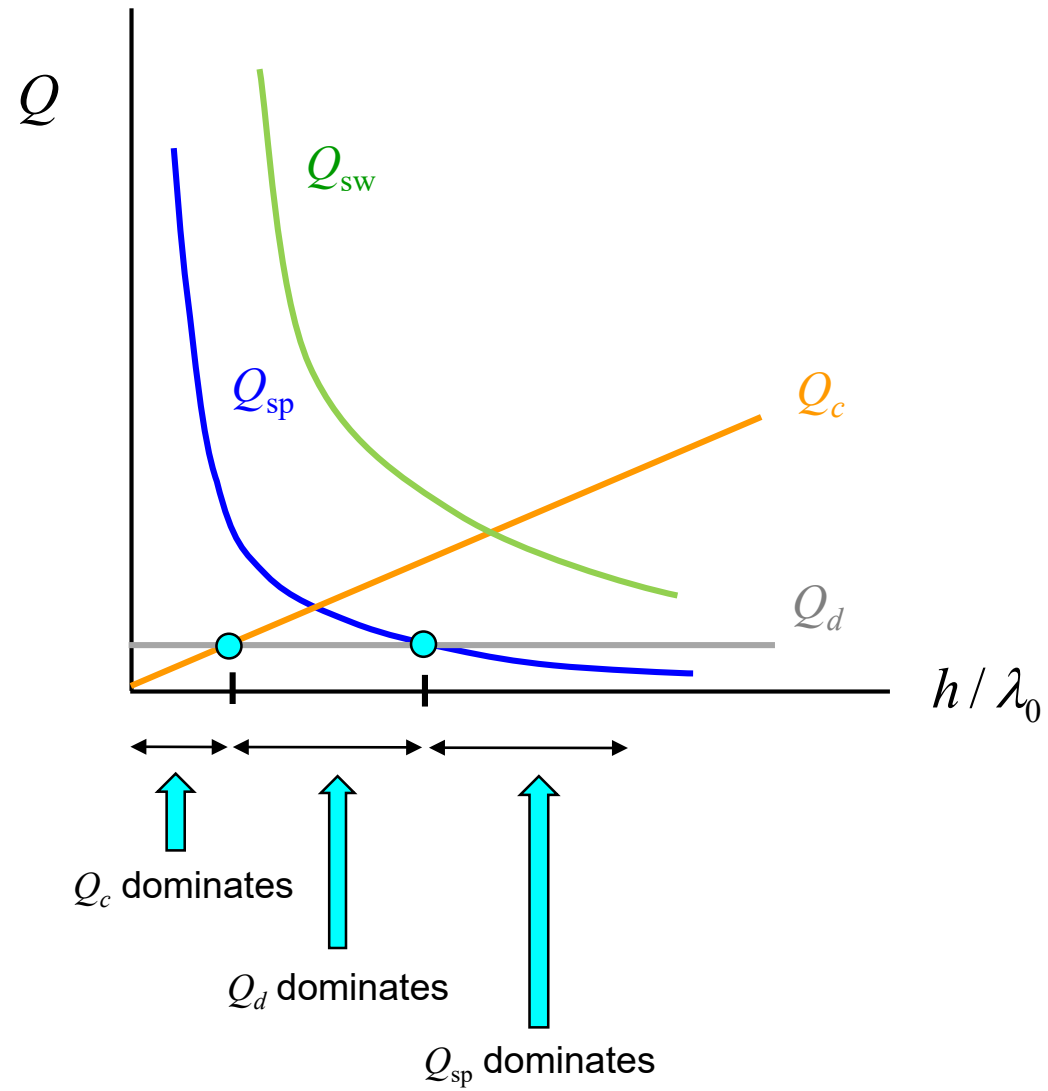
Calculation of Q_{SW} (cont.)

Hence, we have

$$e_r^{\text{sw}} \approx e_r^{\text{hed}} = \frac{1}{1 + (k_0 h) \left(\frac{3\pi}{4} \right) \mu_r \frac{1}{c_1} \left(1 - \frac{1}{n_1^2} \right)^3}$$

This holds for any shape patch
(assuming the HED approximation is accurate).

Comparison of Q_s



Radiation Efficiency

$$e_r \equiv \frac{P_{\text{sp}}}{P_{\text{tot}}} = \frac{P_{\text{sp}}}{P_{\text{sp}} + P_{\text{sw}} + P_c + P_d}$$

Note that

$$Q_i = \omega_0 \frac{U_s}{P_i}$$

Hence

$$P_i \propto \frac{1}{Q_i}$$

Radiation Efficiency (cont.)

Hence

$$e_r = \frac{\frac{1}{Q_{sp}}}{\frac{1}{Q_{sp}} + \frac{1}{Q_{sp}} + \frac{1}{Q_c} + \frac{1}{Q_d}}$$

or $e_r = \frac{1}{\frac{Q_{sp}}{Q}}$

or

$$e_r = \frac{Q}{Q_{sp}}$$

Radiation Efficiency (cont.)

Also, we can write

$$e_r = \frac{P_{\text{sp}}}{P_{\text{tot}}} = \left(\frac{P_{\text{sp}}}{P_{\text{spw}}} \right) \left(\frac{P_{\text{spw}}}{P_{\text{tot}}} \right)$$

where $P_{\text{spw}} = P_{\text{sp}} + P_{\text{sw}}$

Define:

$$e_r^{\text{sw}} = \frac{P_{\text{sp}}}{P_{\text{spw}}}$$

(efficiency due to surface wave loss only)

$$e_r^{\text{diss}} = \frac{P_{\text{spw}}}{P_{\text{tot}}}$$

(efficiency due to material (dissipation) loss only)

Radiation Efficiency (cont.)

Then $e_r = e_r^{\text{sw}} e_r^{\text{diss}}$

where

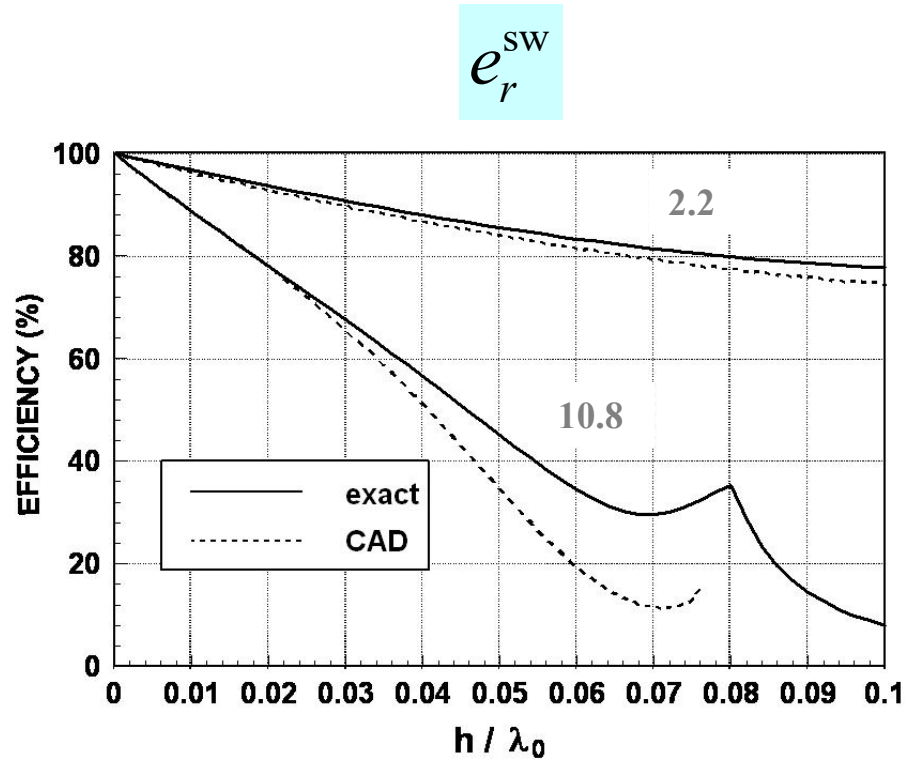
$$e_r^{\text{sw}} = \frac{Q_{\text{spw}}}{Q_{\text{sp}}}$$

$$e_r^{\text{diss}} = \frac{Q}{Q_{\text{spw}}}$$

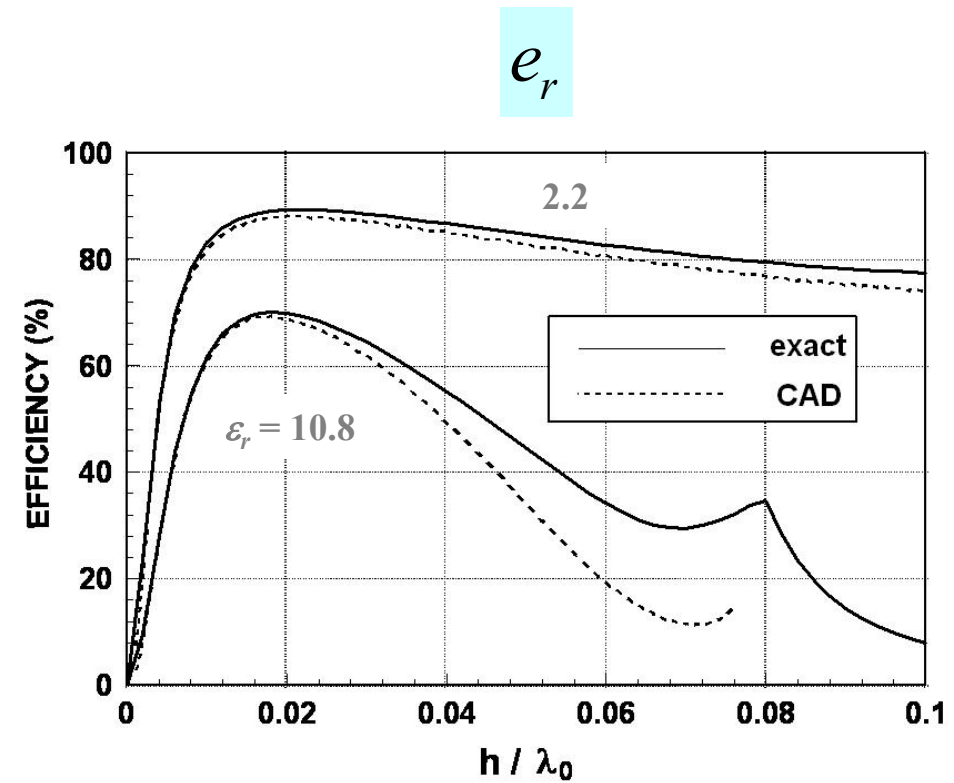
and

$$\frac{1}{Q_{\text{spw}}} = \frac{1}{Q_{\text{sp}}} + \frac{1}{Q_{\text{sw}}}$$

Radiation Efficiency (cont.)



$\epsilon_r = 2.2$ or 10.8
 $W / L = 1.5$



$\tan \delta = 0.001$
 $\sigma = 3.0 \times 10^7$ [S/m]