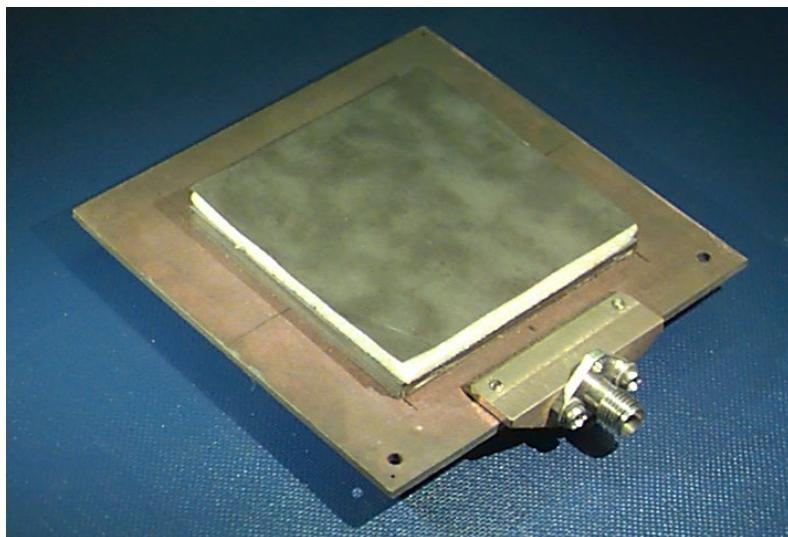


# ECE 6345

## Fall 2024

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## Notes 12

# Overview

- ❖ In this set of notes we calculate the power radiated into space by a current source sitting on top on an infinite grounded substrate.
  - First, we calculate the power radiated by a horizontal electric dipole.
  - We develop a CAD formula for the radiated power of the dipole.
  - Then we extend this to a finite-size patch current.

**Note:**

The power radiated into space is the key ingredient for developing the CAD formula for the space-wave  $Q$  factor ( $Q_{sp}$ ) of the patch. This leads to the CAD formulas for bandwidth, radiation efficiency, and input resistance.

# Radiated Power of Dipole

Horizontal electric dipole in the  $x$  direction on an infinite substrate (from Notes 8):

$$E_\theta = (Il) E_0 \cos \phi G(\theta)$$

$$E_\phi = (Il) E_0 (-\sin \phi) F(\theta)$$

$$F(\theta) = 1 + \Gamma^{\text{TE}}(\theta)$$

$$G(\theta) = \cos \theta (1 + \Gamma^{\text{TM}}(\theta))$$

$$E_0 = \frac{-j\omega\mu_0}{4\pi r} e^{-jk_0 r}$$

$$G(\theta) = \cos \theta (1 + \Gamma^{\text{TM}}(\theta)) = \frac{2 \cos \theta}{1 - j \left( \frac{\varepsilon_r \cos(\theta)}{N_1(\theta)} \right) \cot(k_0 h N_1(\theta))}$$

$$N_1(\theta) \equiv \sqrt{n_1^2 - \sin^2 \theta}$$

$$F(\theta) = 1 + \Gamma^{\text{TE}}(\theta) = \frac{2}{1 - j \left( \frac{N_1(\theta) \sec \theta}{\mu_r} \right) \cot(k_0 h N_1(\theta))}$$

$$n_1 = \sqrt{\varepsilon_r \mu_r}$$

# Radiated Power of Dipole (cont.)

Poynting vector in far field:

$$S_r^{\text{dip}} = \frac{1}{2\eta_0} \left[ |E_\theta|^2 + |E_\phi|^2 \right]$$

Total power radiated into space:

$$\begin{aligned} P_{\text{sp}}^{\text{dip}} &= \int_0^{2\pi} \int_0^{\pi/2} S_r^{\text{dip}}(r, \theta, \phi) r^2 \sin \theta d\theta d\phi \\ &= \frac{1}{2\eta_0} (Il)^2 |E_0|^2 r^2 \left[ \int_0^{2\pi} \cos^2 \phi \int_0^{\pi/2} |G(\theta)|^2 \sin^2 \theta d\theta d\phi + \int_0^{2\pi} \sin^2 \phi \int_0^{\pi/2} |F(\theta)|^2 \sin \theta d\theta d\phi \right] \end{aligned}$$

# Radiated Power of Dipole (cont.)

Performing the  $\phi$  integrals, we have:

$$P_{\text{sp}}^{\text{dip}} = \frac{\pi}{2\eta_0} (Il)^2 |E_0|^2 r^2 \int_0^{\pi/2} (|F(\theta)|^2 + |G(\theta)|^2) \sin \theta d\theta$$

Note that

$$E_0 r = \frac{-j\omega\mu_0}{4\pi} e^{-jk_0 r}$$

so

$$|E_0 r|^2 = \left( \frac{\omega\mu_0}{4\pi} \right)^2 = \left( \frac{k_0 \eta_0}{4\pi} \right)^2$$

and thus

$$P_{\text{sp}}^{\text{dip}} = (Il)^2 k_0^2 \left( \frac{\eta_0}{32\pi} \right) \int_0^{\pi/2} (|F(\theta)|^2 + |G(\theta)|^2) \sin \theta d\theta$$

# CAD Formula for Dipole Radiated Power

Assume  $\frac{h}{\lambda_0} \rightarrow 0$

We wish to approximate these functions:

$$F(\theta) = 1 + \Gamma^{\text{TE}}(\theta)$$

$$G(\theta) = \cos \theta (1 + \Gamma^{\text{TM}}(\theta))$$

## CAD Formula for Dipole Radiated Power (cont.)

$$\frac{h}{\lambda_0} \rightarrow 0$$

$$N_1(\theta) \equiv \sqrt{n_1^2 - \sin^2 \theta}$$

$$n_1 = \sqrt{\epsilon_r \mu_r}$$

Use  $\cot(k_0 h N_1(\theta)) \approx \frac{1}{k_0 h N_1(\theta)} = \frac{1}{k_0 h \sqrt{n_1^2 - \sin^2 \theta}}$

$$G(\theta) = \cos \theta (1 + \Gamma^{\text{TM}}(\theta)) = \frac{2 \cos \theta}{1 - j \left( \frac{\epsilon_r \cos(\theta)}{N_1(\theta)} \right) \cot(k_0 h N_1(\theta))} \approx \frac{2 \cos \theta}{-j \left( \frac{\epsilon_r \cos(\theta)}{N_1(\theta)} \right) \frac{1}{k_0 h N_1(\theta)}} = \left( \frac{2j(n_1^2 - \sin^2 \theta)}{\epsilon_r} \right) k_0 h$$

$$F(\theta) = 1 + \Gamma^{\text{TE}}(\theta) = \frac{2}{1 - j \left( \frac{N_1(\theta) \sec \theta}{\mu_r} \right) \cot(k_0 h N_1(\theta))} \approx \frac{2}{-j \left( \frac{N_1(\theta) \sec \theta}{\mu_r} \right) \frac{1}{k_0 h N_1(\theta)}} = (2j\mu_r \cos \theta) k_0 h$$

Note: The “1” term in the denominator of the  $F$  and  $G$  functions can be neglected for a thin substrate.

## CAD Formula for Dipole Radiated Power (cont.)

The result is then:

$$G(\theta) \sim \left( \frac{2j(n_1^2 - \sin^2 \theta)}{\epsilon_r} \right) k_0 h$$
$$F(\theta) \sim (2j\mu_r \cos \theta) k_0 h$$

where  $n_1 = \sqrt{\epsilon_r \mu_r}$

## CAD Formula for Dipole Radiated Power (cont.)

Recall:

$$P_{\text{sp}}^{\text{dip}} = (Il)^2 \left( \frac{k_0^2 \eta_0}{32\pi} \right) \int_0^{\pi/2} \left[ |F(\theta)|^2 + |G(\theta)|^2 \right] \sin \theta d\theta$$

We need the following integrals:

$$\int_0^{\pi/2} \cos^2 \theta \sin \theta d\theta = \frac{1}{3}$$

$$\int_0^{\frac{\pi}{2}} \sin \theta d\theta = 1$$

$$\int_0^{\frac{\pi}{2}} \sin^3 \theta d\theta = \frac{2}{3}$$

$$\int_0^{\frac{\pi}{2}} \sin^5 \theta d\theta = \frac{8}{15}$$

$$G(\theta) \sim \left( \frac{2j(n_1^2 - \sin^2 \theta)}{\epsilon_r} \right) k_0 h$$
$$F(\theta) \sim (2j\mu_r \cos \theta) k_0 h$$

$$|G(\theta)|^2 \sim \left( \frac{4(n_1^2 - \sin^2 \theta)^2}{\epsilon_r^2} \right) (k_0 h)^2$$
$$|F(\theta)|^2 \sim (4\mu_r^2 \cos^2 \theta) (k_0 h)^2$$

## CAD Formula for Dipole Radiated Power (cont.)

We then have, accounting for all of the constants in front of the integrals:

$$P_{\text{sp}}^{\text{dip}} = (Il)^2 \left( \frac{k_0^2 \eta_0}{32\pi} \right) (k_0 h)^2 4 \left[ \mu_r^2 \left( \frac{1}{3} \right) + \frac{1}{\varepsilon_r^2} \left( n_1^4(1) - 2n_1^2 \left( \frac{2}{3} \right) + \frac{8}{15} \right) \right]$$

Substituting for the index of refraction, we have:

$$P_{\text{sp}}^{\text{dip}} = (Il)^2 (k_0 h)^2 k_0^2 \left( \frac{\eta_0}{8\pi} \right) \left[ \mu_r^2 \left( \frac{1}{3} \right) + \mu_r^2 (1) - 2 \frac{\mu_r}{\varepsilon_r} \left( \frac{2}{3} \right) + \frac{1}{\varepsilon_r^2} \left( \frac{8}{15} \right) \right]$$

$$\text{Recall: } n_1 = \sqrt{\varepsilon_r \mu_r}$$

## CAD Formula for Dipole Radiated Power (cont.)

$$P_s^{\text{dip}} = (Il)^2 (k_0 h)^2 k_0^2 \left( \frac{\eta_0}{8\pi} \right) \left[ \mu_r^2 \left( \frac{1}{3} \right) + \mu_r^2 (1) - 2 \frac{\mu_r}{\epsilon_r} \left( \frac{2}{3} \right) + \frac{1}{\epsilon_r^2} \left( \frac{8}{15} \right) \right]$$

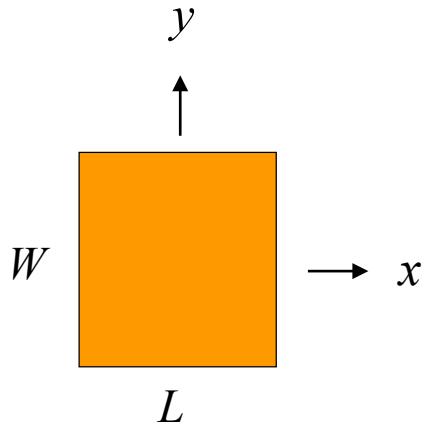
Note that  $\left[ \dots \right] = \mu_r^2 \left( \frac{4}{3} - \frac{4}{3} \frac{1}{\epsilon_r \mu_r} + \frac{8}{15} \frac{1}{\mu_r^2 \epsilon_r^2} \right)$

$$= \mu_r^2 \left( \frac{4}{3} \right) \left( 1 - \frac{1}{n_1^2} + \frac{2/5}{n_1^4} \right)$$

Define  $c_1 \equiv 1 - \frac{1}{n_1^2} + \frac{2/5}{n_1^4}$

Then  $P_s^{\text{dip}} \approx (Il)^2 (k_0 h)^2 k_0^2 \left( \frac{\eta_0}{6\pi} \right) \mu_r^2 c_1$

# Radiated Power of Patch



Assume that

$$J_{sx}^{1,0} = \cos\left(\frac{\pi x}{L}\right)$$

We find the equivalent dipole moment of the patch:

$$\begin{aligned}(Il)_{\text{patch}} &= \int_{-\frac{L}{2}}^{\frac{L}{2}} \int_{-\frac{W}{2}}^{\frac{W}{2}} J_{sx}^{1,0}(x, y) dy dx \\ &= W \int_{-\frac{L}{2}}^{\frac{L}{2}} \cos\left(\frac{\pi x}{L}\right) dx \\ &= W \left( \frac{2L}{\pi} \right)\end{aligned}$$

# Radiated Power of Patch (cont.)

$$(Il)_{\text{patch}} = \left( \frac{2}{\pi} WL \right)$$

Neglecting the space factor,  $P_{\text{sp}}^{\text{patch}} \approx P_{\text{sp}}^{\text{dip}}$

where

$$P_{\text{sp}}^{\text{dip}} = \left( \frac{2}{\pi} WL \right)^2 (k_0 h)^2 k_0^2 \left( \frac{\eta_0}{6\pi} \right) \mu_r^2 c_1$$

This formula may be improved by accounting for the patch space factor, which leads to the introduction of the “ $p$  factor” that is discussed in the next set of notes.