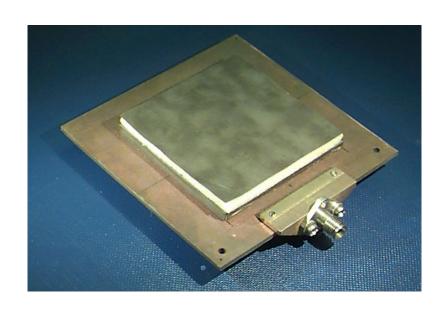
## ECE 6345

Spring 2024

Prof. David R. Jackson ECE Dept.

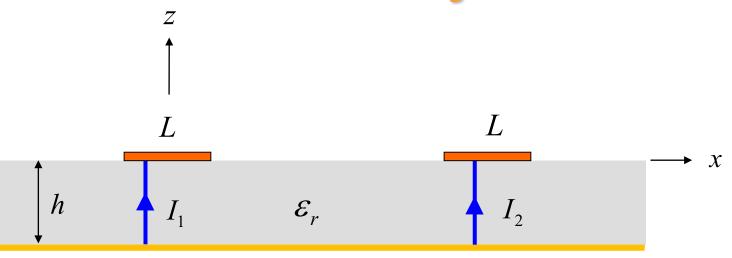


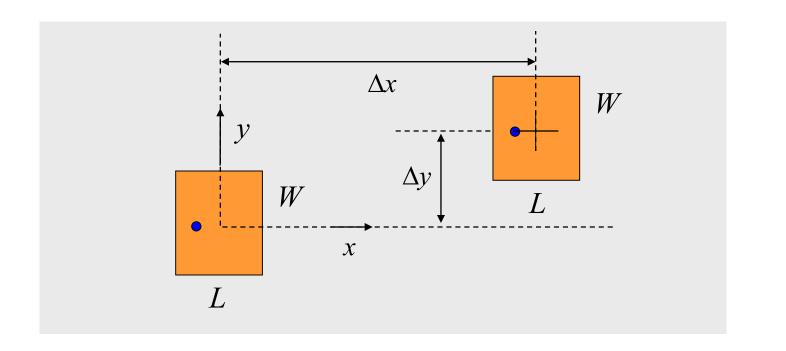
Notes 27

### Overview

❖ In this set of notes we use the spectral-domain method to find the mutual impedance between two rectangular patch antennas.

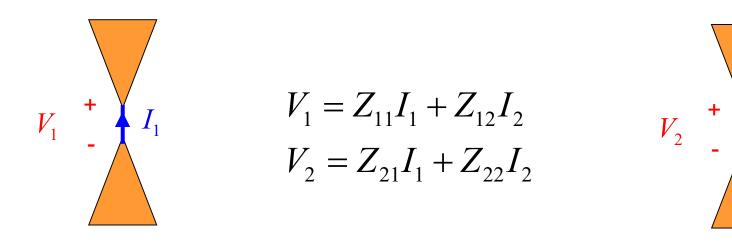
# Geometry





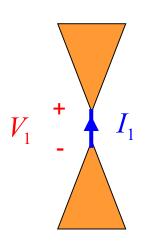
## **Mutual Impedance Formulation**

Assume two arbitrary antennas, to be general.



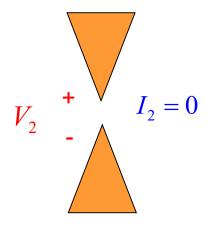
The two-port system is described by a  $2\times2$  impedance (Z) matrix.

The self impedance  $Z_{11}$  is calculated.



$$V_1 = Z_{11}I_1 + Z_{12}I_2$$
$$V_2 = Z_{21}I_1 + Z_{22}I_2$$

$$Z_{11} = \frac{V_1}{I_1} \bigg|_{I_2 = 0}$$

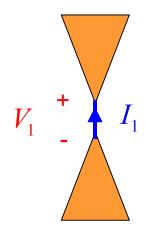


$$Z_{11} \approx Z_{\rm in}$$

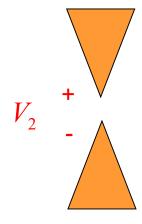
(The presence of open-circuited antenna 2 does not significantly affect the input impedance of antenna 1.)

The mutual impedance  $Z_{21}$  is calculated.

$$V_1 = Z_{11}I_1 + Z_{12}I_2$$
$$V_2 = Z_{21}I_1 + Z_{22}I_2$$

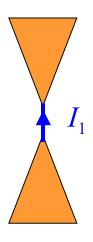


$$Z_{21} = \frac{V_2}{I_1} \bigg|_{I_2 = 0}$$



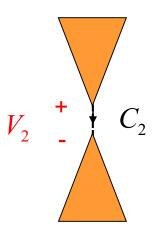
Note:  $Z_{21} = Z_{12}$ 

The open-circuit voltage  $V_2$  is obtained by integrating the electric field produced from current  $I_1$  over the path  $C_2$ .

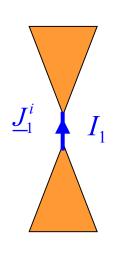


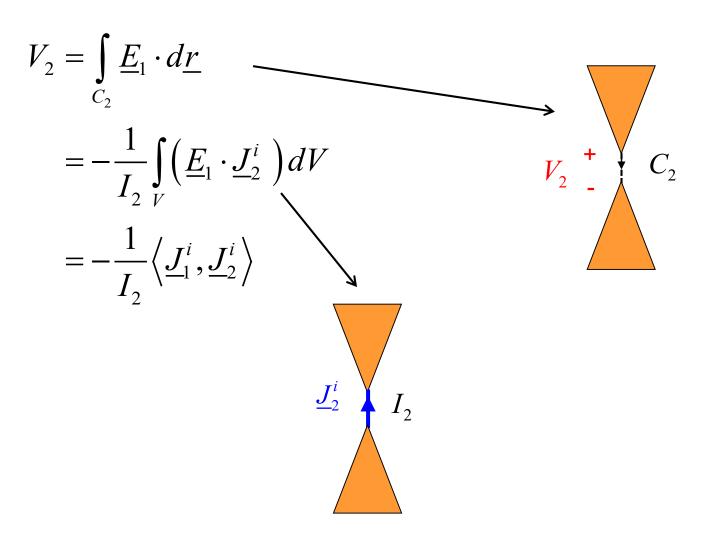
$$V_2 = \int_{C_2} \underline{E}_1 \cdot d\underline{r}$$

 $\underline{E}_1$  = electric field produced by the feed current  $I_1$ , in the presence of antenna 1 and antenna 2.

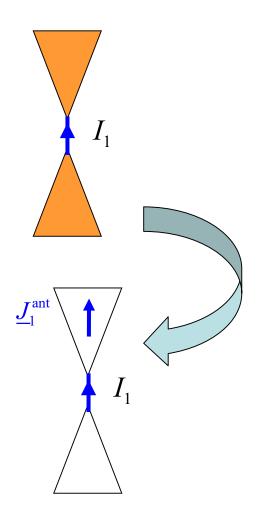


The open-circuit voltage  $V_2$  is put in the form of a reaction.

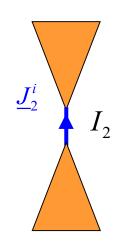




The equivalence principle is used to replace antenna 1 with its surface current.



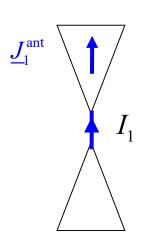
$$\begin{split} V_2 &= -\frac{1}{I_2} \left\langle \underline{J}_1^i, \underline{J}_2^i \right\rangle \\ &= -\frac{1}{I_2} \left\langle \underline{J}_1^{\text{ant}}, \underline{J}_2^i \right\rangle \end{split}$$



The field produced by current  $I_1$  exciting antenna 1 is the same as that produced by the current on antenna 1 in free space.

The antenna current  $\underline{J}_1^{\text{ant}}$  is that excited on antenna 1 when it is in the <u>presence</u> of open-circuited antenna 2.

Reciprocity is invoked, and then the equivalence principle.

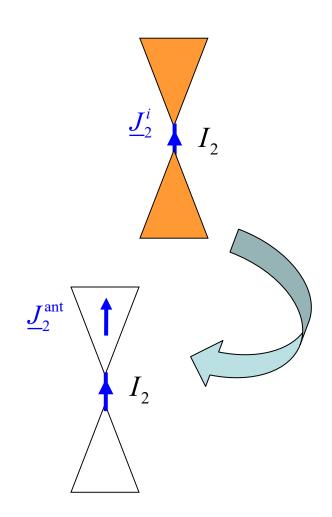


$$V_{2} = -\frac{1}{I_{2}} \left\langle \underline{J}_{1}^{\text{ant}}, \underline{J}_{2}^{i} \right\rangle$$

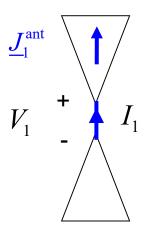
$$= -\frac{1}{I_{2}} \left\langle \underline{J}_{2}^{i}, \underline{J}_{1}^{\text{ant}} \right\rangle$$

$$= -\frac{1}{I_{2}} \left\langle \underline{J}_{2}^{\text{ant}}, \underline{J}_{1}^{\text{ant}} \right\rangle$$

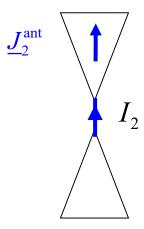
The antenna current  $\underline{J_2}^{\text{ant}}$  is that excited on antenna 2 when it is in the <u>absence</u> of open-circuited antenna 1.



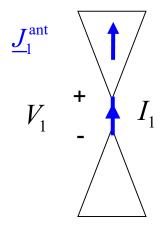
Reciprocity is invoked one more time.



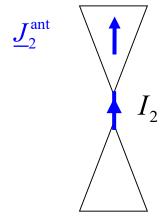
$$V_{2} = -\frac{1}{I_{2}} \left\langle \underline{J}_{2}^{\text{ant}}, \underline{J}_{1}^{\text{ant}} \right\rangle$$
$$= -\frac{1}{I_{2}} \left\langle \underline{J}_{1}^{\text{ant}}, \underline{J}_{2}^{\text{ant}} \right\rangle$$



$$V_2 = -\frac{1}{I_2} \left\langle \underline{J}_1^{\text{ant}}, \underline{J}_2^{\text{ant}} \right\rangle$$



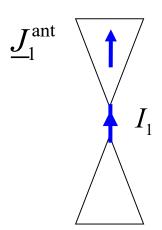
$$Z_{21} = \frac{V_2}{I_1} \bigg|_{I_2 = 0}$$



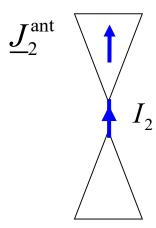
The mutual impedance is then:

$$Z_{21} = -\frac{1}{I_1 I_2} \left\langle \underline{J}_1^{\text{ant}}, \underline{J}_2^{\text{ant}} \right\rangle$$

#### **Summary**



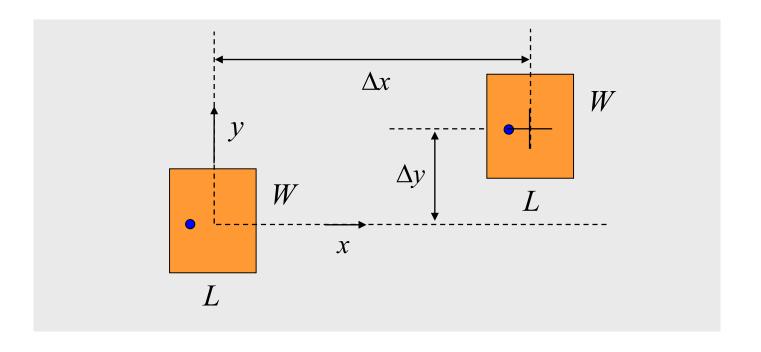
$$Z_{12} = -\frac{1}{I_1 I_2} \left\langle \underline{J}_1^{\text{ant}}, \underline{J}_2^{\text{ant}} \right\rangle$$



 $J_1^{\text{ant}}$  = current on antenna 1, when excited by current  $I_1$  in the <u>presence</u> of open-circuited antenna 2.

 $J_2^{\text{ant}}$  = current on antenna 2, when excited by current  $I_2$  in the <u>absence</u> of antenna 1.

## Mutual Impedance Between two Patch Antennas



$$Z_{12} = -\frac{1}{I_1 I_2} \left\langle J_{sx}^{(1)}, J_{sx}^{(2)} \right\rangle$$

The two patches are assumed to be identical here.

Assume 
$$I_1 = I_2 = 1$$
 [A]

$$Z_{12} = -\left\langle J_{sx}^{(1)}, J_{sx}^{(2)} \right\rangle = -A_{x}^{(1)} A_{x}^{(2)} \left\langle B_{x}^{(1)}, B_{x}^{(2)} \right\rangle = -A_{x}^{2} \left\langle B_{x}^{(1)}, B_{x}^{(2)} \right\rangle$$

Denote 
$$Z_{xx}^{1,2} = -\langle B_x^{(1)}, B_x^{(2)} \rangle$$

Then we have  $Z_{12} = A_r^2 Z_{rr}^{1,2}$ 

From Notes 9:

$$\frac{A_{10}^{J}}{I_{0}} = -\frac{1}{j\omega\mu} \left(\frac{\pi}{L}\right) \left[\frac{Z_{\text{in}}}{h\sin\left(\frac{\pi x_{0}}{L}\right)}\right] \qquad \Box \qquad A_{x} = -\frac{1}{j\omega\mu} \left(\frac{\pi}{L}\right) \left[\frac{Z_{\text{in}}}{h\sin\left(\frac{\pi x_{0}}{L}\right)}\right]$$

$$A_{x} = -\frac{1}{j\omega\mu} \left(\frac{\pi}{L}\right) \left| \frac{Z_{\text{in}}}{h\sin\left(\frac{\pi x_{0}}{L}\right)} \right|$$

Note:  $A_r^{(1)} = A_r^{(2)} = A_r$ 

 $A_r$  is the amplitude of the patch current when the patch is fed by a 1 A probe current.

$$B_x^{(1)} = \cos\left(\frac{\pi x}{L}\right)$$

$$B_x^{(2)} = \cos\left(\frac{\pi(x - \Delta x)}{L}\right)$$

"basis functions"

New notation:  $(A_x = A_{10}^J, I_0 = 1 \text{ A})$ 

Calculation of reaction  $Z_{xx}^{1,2}$  between patch basis functions:

$$\tilde{E}_{x}\left[B_{x}^{(1)}\right] = \tilde{G}_{xx}\tilde{B}_{x}^{(1)}$$

$$E_{x}\left[B_{x}^{(1)}\right] = \frac{1}{(2\pi)^{2}} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{G}_{xx} \tilde{B}_{x}^{(1)} e^{-j(k_{x}x+k_{y}y)} dk_{x} dk_{y}$$

Hence, integrating over the surface of patch 2, we have:

$$Z_{xx}^{1,2} = -\frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{G}_{xx} (k_x, k_y) \tilde{B}_x^{(1)} (k_x, k_y) \tilde{B}_x^{(2)} (-k_x, -k_y) dk_x dk_y$$

$$\left( \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} B_{x2} (x, y) e^{-j(k_x x + k_y y)} dx dy = \tilde{B}_2 (-k_x, -k_y) \right)$$

$$Z_{xx}^{1,2} = -\frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{G}_{xx} \left( k_x, k_y \right) \tilde{B}_x^{(1)} \left( k_x, k_y \right) \tilde{B}_x^{(2)} \left( -k_x, -k_y \right) dk_x dk_y$$

From the Fourier "shifting" theorem, we have:

$$\tilde{B}_{x}^{(2)}\left(k_{x},k_{y}\right) = \tilde{B}_{x}^{(1)}\left(k_{x},k_{y}\right)e^{j\left(k_{x}\Delta x + k_{y}\Delta y\right)} \implies \tilde{B}_{x}^{(2)}\left(-k_{x},-k_{y}\right) = \tilde{B}_{x}^{(1)}\left(-k_{x},-k_{y}\right)e^{-j\left(k_{x}\Delta x + k_{y}\Delta y\right)}$$

Hence, we have:

$$Z_{xx}^{1,2} = -\left\langle B_{x}^{(1)}, B_{x}^{(2)} \right\rangle = -\frac{1}{\left(2\pi\right)^{2}} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{G}_{xx} \left(k_{x}, k_{y}\right) \left(\tilde{B}_{x}^{(1)} \left(k_{x}, k_{y}\right)\right)^{2} e^{-j\left(k_{x}\Delta x + k_{y}\Delta y\right)} dk_{x} dk_{y}$$

Note: 
$$\tilde{B}_{x}^{(1)}(k_{x},k_{y}) = \left(\frac{\pi}{2}LW\right)\operatorname{sinc}\left(k_{y}\frac{W}{2}\right)\left|\frac{\cos\left(k_{x}\frac{L}{2}\right)}{\left(\frac{\pi}{2}\right)^{2}-\left(k_{x}\frac{L}{2}\right)^{2}}\right|$$
  $\left(\tilde{B}_{x}^{(1)}\left(-k_{x},-k_{y}\right)=\tilde{B}_{x}^{(1)}\left(k_{x},k_{y}\right)\right)$ 

Converting to polar coordinates, we have: Note: The "1" superscript is dropped henceforth.

$$Z_{xx}^{1,2} = -\left\langle B_{x}^{(1)}, B_{x}^{(2)} \right\rangle = -\frac{1}{\left(2\pi\right)^{2}} \int_{0}^{2\pi} \int_{0}^{\infty} \tilde{G}_{xx} \left(k_{x}, k_{y}\right) \tilde{B}_{x}^{2} \left(k_{x}, k_{y}\right) e^{-j\left(k_{x}\Delta x + k_{y}\Delta y\right)} k_{t} dk_{t} d\overline{\phi}$$

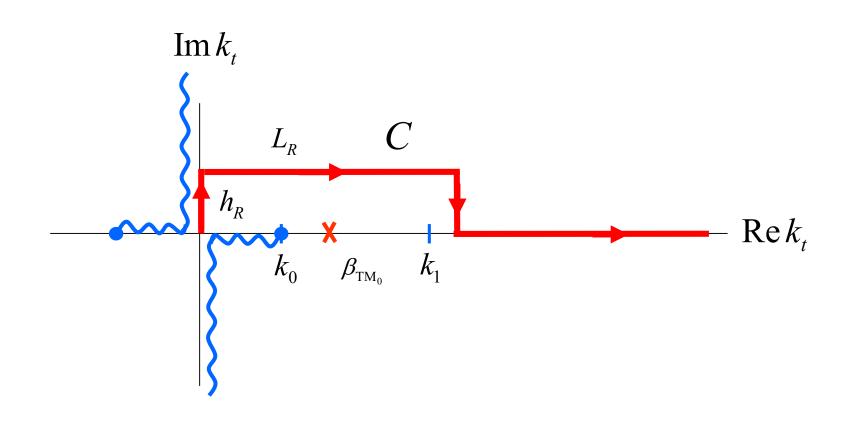
Since the integrand is an even function of  $k_x$  and  $k_y$ , we can write:

$$Z_{xx}^{1,2} = -\left\langle B_{x}^{(1)}, B_{x}^{(2)} \right\rangle = -\frac{1}{\pi^{2}} \int_{0}^{\pi/2} \int_{0}^{\infty} \tilde{G}_{xx} \left( k_{x}, k_{y} \right) \tilde{B}_{x}^{2} \left( k_{x}, k_{y} \right) \cos \left( k_{x} \Delta x \right) \cos \left( k_{y} \Delta y \right) k_{t} dk_{t} d\overline{\phi}$$

Note: Quadrant 1 Quadrant 2 Quadrant 3 Quadrant 4 
$$e^{-j(k_x\Delta x)}e^{-j(k_y\Delta y)} + e^{+j(k_x\Delta x)}e^{-j(k_y\Delta y)} + e^{+j(k_x\Delta x)}e^{+j(k_y\Delta y)} + e^{-j(k_x\Delta x)}e^{+j(k_y\Delta y)}$$
$$= 2\cos(k_x\Delta x)e^{-j(k_y\Delta y)} + 2\cos(k_x\Delta x)e^{+j(k_y\Delta y)}$$
$$= 2\cos(k_x\Delta x)\left[e^{-j(k_y\Delta y)} + e^{+j(k_y\Delta y)}\right]$$
$$= 4\cos(k_x\Delta x)\cos(k_y\Delta y)$$

#### Final form of mutual reaction:

$$Z_{xx}^{1,2} = -\left\langle B_{x}^{(1)}, B_{x}^{(2)} \right\rangle = -\frac{1}{\pi^{2}} \int_{0}^{\pi/2} \int_{C} \tilde{G}_{xx} \left( k_{x}, k_{y} \right) \tilde{B}_{x}^{2} \left( k_{x}, k_{y} \right) \cos \left( k_{x} \Delta x \right) \cos \left( k_{y} \Delta y \right) k_{t} dk_{t} d\overline{\phi}$$



### **Summary**

$$Z_{12} = A_x^2 Z_{xx}^{1,2}$$

$$Z_{xx}^{1,2} = -\frac{1}{\pi^2} \int_0^{\pi/2} \int_C \tilde{G}_{xx} \left( k_x, k_y \right) \tilde{B}_x^2 \left( k_x, k_y \right) \cos \left( k_x \Delta x \right) \cos \left( k_y \Delta y \right) k_t dk_t d\overline{\phi}$$

$$A_{x} = -\frac{1}{j\omega\mu} \left(\frac{\pi}{L}\right) \left[\frac{Z_{\text{in}}}{h\sin\left(\frac{\pi x_{0}}{L}\right)}\right]$$

## Results

D. M. Pozar, "Input Impedance and mutual coupling of rectangular microstrip antennas," *IEEE Trans. Antennas Propagat.*, vol. AP-30. pp. 1191-1196, Nov. 1982.

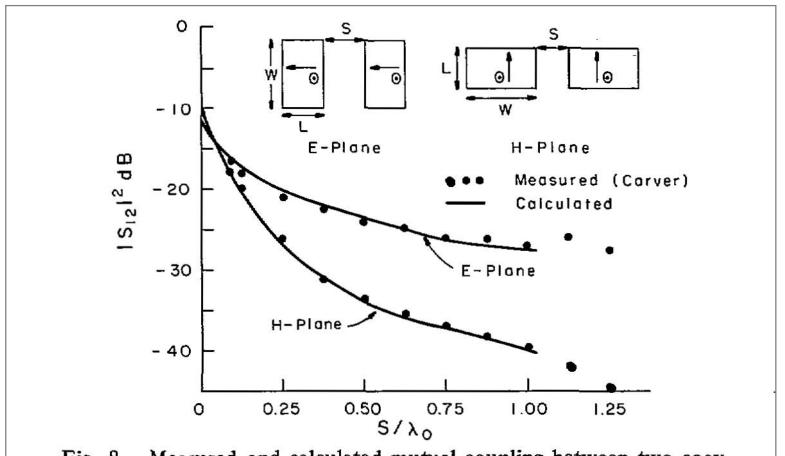
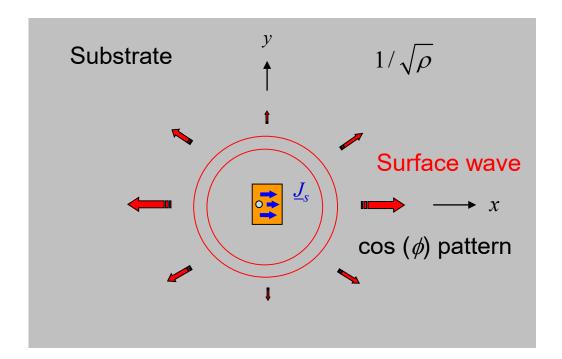


Fig. 8. Measured and calculated mutual coupling between two coaxfed microstrip antennas, for both  $\overline{E}$ -plane and  $\overline{H}$ -plane coupling. W = 10.57 cm, L = 6.55 cm, d = 0.1588 cm,  $\epsilon_r = 2.55$ , f = 1410. MHz.

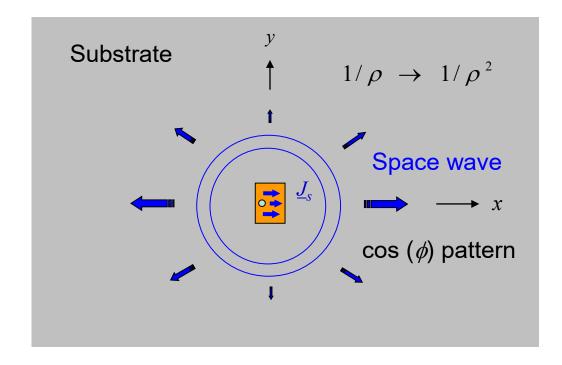
## **Components of Mutual Impedance**

#### We can also consider the various components of $Z_{12}$ :

- Surface-wave contribution
- Space-wave contribution ("lateral wave")
- The space wave decays as  $1/\sqrt{\rho}$



• The space wave initially decays as  $1/\rho$  (but eventually transitions to a behavior of  $1/\rho^2$ )



## **Components of Mutual Impedance (cont.)**

#### Results for typical patches

Circular patches

$$\varepsilon_r = 2.94, \ h/\lambda_0 = 0.01, \ f = 2.0 \,\text{GHz}$$
 (h = 1.5 mm)

